



#### Recent Advancements in the Gyrokinetic Moment-Based Approach for Boundary Plasmas

B. J. Frei<sup>1</sup>, P. Ricci<sup>1</sup>, J. Ball<sup>1</sup>, A. C. D. Hoffmann<sup>1</sup>, R. Jorge<sup>2</sup>, and L. Stenger<sup>1</sup>

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Swiss Plasma Center  <sup>1</sup> Ecole Polytechnique Fédérale de Lausanne (EPFL), Swiss Plasma Center, CH-1015 Lausanne, Switzerland
 <sup>2</sup> Institute for Research in Electronics and Applied Physics, University of Maryland, College Park MD 20742, United States of America

- Motivations and The GyroKinetic (GK) Moment-Based Approach
- Numerical studies and benchmarks with GENE code
- Conclusions



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### EPFL Challenges of Simulating the Turbulent Boundary Plasmas

- Boundary region (edge and scrape-off-layer) controls the performance of fusion devices (H-L transition, pedestal, ELMs, ...)
- Boundary region is characterised by different plasma collisionality regimes:

TER: 
$$T_e \sim 10 - 10^4 \text{ eV}$$
 and  $n \sim 10^{18} - 10^{20} \text{ m}^{-3} \Rightarrow \lambda_{mpf} / R_0 \sim \frac{T_e^2}{n_e R_0} \sim 10^{-1} - 10^3$ 

- Two currently-used turbulent modelling approaches:
  - Drift-Kinetic (DK) fluid modelling (lowest-order moments, less expensive,  $k_{\perp}\rho_i\ll 1$  and  $\lambda_{mfp}k_{\parallel}\ll 1$ , no kinetic effects, Full-F)
  - GyroKinetic (GK) modelling (expensive,  $k_{\perp}\rho_i \sim 1$ , kinetic effects, also suitable for  $\lambda_{mfp}k_{\parallel}\gtrsim 1$ )

**GK Moment Approach**  $k_{\parallel}\lambda_{mfp} \ll 1$  &  $k_{\parallel}\lambda_{mfp} \gtrsim 1$ 



Giacomin M. et al. JPP, 2020

Chang C. S. et al. Nucl. Fusion, 2017

## EPFL The GK Moment Approach to the GK Boundary Model

- Expansion of  $F_a$  (Full-F) on a Hermite-Laguerre polynomials basis: Gyro-Moment of  $F_a$  $F_a = \sum_p \sum_j N_a^{pj} (\mathbf{R}, t) \frac{H_p(v_{\parallel}) L_j(\mu)}{\sqrt{2^p p!}} F_{Ma}$
- Equation for  $N_a^{pj}$  from the projection onto the Hermite-Laguerre basis of GK Equ.

$$||\ldots||^{pj} = \int d\theta \int d\mu dv_{\parallel} H_p(v_{\parallel}) L_j(\mu) \ldots \qquad || (\text{GK Equ.}) ||^{pj}$$

Gyro-Moment Hierarchy Equation and GK Field Equations

Projection of GK collision operator

$$\frac{\partial}{\partial t}N_{a}^{pj} + \nabla \cdot ||\dot{\mathbf{R}}||^{pj} - \frac{\sqrt{2l}}{v_{th\parallel a}}||\dot{v}_{\parallel}||^{p-1j} + \mathcal{F}_{a}^{pj} = \sum_{b} C_{ab}^{pj} \qquad C_{ab}^{pj} = ||\langle C_{ab}\rangle||^{pj}$$
B. J. Frei *et al.*, JPP **86**, 905860205 (2020)

## **EPFL** Nonlinear GK Coulomb in the Gyro-Moment Approach

• In (x, v) phase-space, Coulomb ("Landau") collision operator is defined by

$$C_{ab}[f_a, f_b] = C_{ab}(\boldsymbol{x}, \boldsymbol{v}) = \frac{\partial}{\partial \boldsymbol{v}} \cdot \left[ \boldsymbol{A}_{ab} f_a + \frac{\partial}{\partial \boldsymbol{v}} \cdot (\boldsymbol{D}_{ab} f_b) \right]$$

• Gyroaveraged of  $C_{ab}$  performed in  $(\mathbf{R}, \mu, v_{\parallel}, t)$  phase-space and project on Hermite-Laguerre, i.e.

$$C_{ab}^{pj} = \int d\boldsymbol{v} H_p(v_{\parallel}) L_j(\mu) \left\langle C_{ab} \right\rangle$$

#### Full-F Nonlinear GK Coulomb Collision Operator

$$C_{ab}^{pj} = \nu_{ab} \sum_{\mathbf{k}, \mathbf{k}'} \sum_{l=0}^{\infty} \sum_{m=-l}^{m=l} \sum_{r, s, p, q, \dots} \nu_{ab, \dots}^{lpj, \dots} (T^{-1})_{pq}^{rsm} \cdot K_s(b_a) K_q(b_b') N_a^{rs}(\mathbf{k}) N_b^{pq}(\mathbf{k}'),$$

$$Numerical coefficients \quad FLR Kernels \quad Gyro-Moments$$

$$\bullet \text{ Arbitrary } k_{\perp}, \text{ and } m_a/m_b, T_a/T_b \text{ ratios}$$

$$Jorge \text{ R., B. J. Frei and P. Ricci, JPP 85, 905850604 (2019)$$

B. J. Frei, TSVV3 2021

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### EPFL Linearized GK Coulomb in the Gyro-Moment Approach

• Assuming 
$$F_a = F_{aM} + f_a$$
  $(f_a \ll F_{aM})$   
 $C_{ab} \simeq C_{ab}^T + C_{ab}^F$   $C_{ab}^T \stackrel{\text{Test}}{=} C_{ab}[f_a, f_{bM}]$   $C_{ab}^F = C_{ab}[f_{aM}, f_b]$   
• Linearized **GK Coulomb Collision Operator** in the gyro-moment approach FLR Kernels  
 $C_{ab}^{Tpj} = \sum_{l=0}^{\infty} \sum_{m=-l}^{m=l} \sum_{r,s,p,q,\dots} \nu_{ab\dots}^{Tlpj} \dots (T^{-1})_{pq}^{rsm} K_s(b_a) N_a^{rs}$   
Numerical coefficients Gyro-Moments

 Gyro-moment approach applied to different simplified/ad hoc linearized collision operators (e.g. GK/DK Sugama, GK/DK pitch-angle, GK/DK Dougherty)

B. J. Frei et al., JPP 87, 905870501 (2021)

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### EPFL Linearized Gyro-Moment Hierarchy in a Flux-Tube Code

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- Assuming 
$$F_a = F_{aM} + f_a$$
  $(f_a \ll F_{aM})$ 

With

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$$\begin{split} & \frac{\partial}{\partial t} \mathbf{N}_{a} + \mathbf{H}_{a} \cdot \nabla_{\parallel} \mathbf{N}_{a} + (\mathbf{M}_{a} \cdot \mathbf{N}_{a}) \nabla_{\parallel} \ln B + \mathbf{D}_{a} \cdot \mathbf{N}_{a} \\ &= \mathbf{S}_{\phi} \phi + \mathbf{S}_{\psi} \psi + \sum_{b} \left( \mathbf{C}_{ab}^{T} \cdot \mathbf{N}_{a} + \mathbf{C}_{ab}^{F} \cdot \mathbf{N}_{b} \right) \\ & \text{Background Gradient drive} & \text{Linearized GK Collision Operators} \\ & \delta \mathbf{E}_{es} = -\nabla \phi, \, \delta \mathbf{B}_{\perp} \simeq - \mathbf{b} \times \nabla \psi \text{ and } \mathbf{N}_{a} = [N_{a}^{00}, N_{a}^{01}, \dots N_{a}^{10}, N_{a}^{11} \dots N_{a}^{PJ}]^{T} \end{split}$$

- Closure by truncation (arbitrary collisionality closure available):  $P = P(\nu, k_{\parallel}), J = J(\nu, k_{\perp})$
- Implemented in a flux-tube code with concentric, circular flux surface:  $\mathbf{B} = B_0 \nabla x \times \nabla y$ ,  $\mathbf{k}_{\perp} = k_x \nabla x + k_y \nabla y$

# EPFL Benchmark ( $\nu \ll 1$ ) with GENE: Cyclone Base Case

• Collisionless ITG with adiabatic electron:

• 
$$\mathbf{B} = B_0 \nabla x \times \nabla y$$
 and  $\mathbf{k}_{\perp} = k_x \nabla x + k_y \nabla y$   
 $R_{T_i} = \frac{R}{L} \simeq -R \partial_x \ln T_i$ 





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B. J. Frei, TSVV3 2021

# EPFL Benchmark ( $\nu \ll 1$ ) with GENE: ITG to TEM mode

• Retrieve collisionless ITG to TEM transition (cyclone base case parameters) with  $(P, J) \simeq (32, 16)$  (GENE velocity-space resolution  $(N_{\nu_{\parallel}}, N_{\mu}) \simeq (64, 24)$ )



- Good agreement with ballooning mode structures
- Strong kinetic physics (e.g. trapped/passing boundary) require larger (P, J)

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# EPFL Benchmark ( $\nu \ll 1$ ) with GENE: ITG to KBM mode

- Retrieve KBM transition (cyclone base case parameters) at finite  $\beta_e$ , with  $(P,J)\simeq(16,8)$ 



- Low number of gyro-moments (w.r.t to ITG) underlies the "fluid-like" properties of KBM

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# EPFL Benchmark ( $\nu \ll 1$ ) with GENE: ITG to TEM modes

- Fine scale structures near passing/trapped boundary
- With sufficient number of gyro-moments, good qualitative agreement with the modulus of  $f_e$  at the outboard mid plane



## **EPFL** ITG mode with GK Coulomb and other GK Collision Models

• Relative deviation of **ITG growth rate peak w.r.t GK Coulomb** as a function of collisionality,  $\nu = \nu_{ii}/[c_s/L_N]$ , and normalized temperature gradient,  $\eta = L_N/L_T$ 



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## EPFL First Nonlinear Simulation using the Gyro-Moment Approach

- **Z-Pinch** geometry ( $k_{\parallel} = 0$ ), kinetic electrons
- Retain  $\mathbf{E} \times \mathbf{B}$  nonlinearity

$$\sim \sum_{\boldsymbol{k},\boldsymbol{k}'} \frac{i\boldsymbol{E}(\boldsymbol{k}) \times \boldsymbol{B}}{B^2} \cdot \boldsymbol{k}' N_a^{pj}(\boldsymbol{k}') e^{i(\boldsymbol{k}+\boldsymbol{k}') \cdot \boldsymbol{R}}$$

- Collisional effects with linearized GK collision operators (GK Coulomb, GK Sugama, GK Dougherty)
- Cyclic, bursting behaviour of fluctuations, transport, and zonal flows



### EPFL Conclusions

- A new GK model for the tokamak boundary based on a Hermite-Laguerre polynomials basis (gyro-moment expansion)
- A nonlinear GK Coulomb collision operator (arbitrary mass and temperature ratios) is derived; a linearized version derived and numerically implemented; gyromoment expansion of different simplified/ad hoc collision operator models (e.g., Sugama operator)
- Recover relevant microinstability linear properties (e.g., TEM, ITG and KBM); in agreement with GENE
- Explore deviations between GK Coulomb and other GK collision operator models (e.g. ITG mode)
- Number of gyro-moment decreases with collisionality (SOL) ⇒ optimal for edge and SOL modelling.
- Extend to flux-tube code to nonlinear and realistic 3D equilibrium and Full-F conditions

#### Thank you for your attention