

Excitation of TAE modes by an electromagnetic antenna using the global gyrokinetic code ORB5

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October 27, 2021

ORB5 eqs. of motion

Consider evolution of reduced velocity distribution function $f(\mathbf{R}, v_{\parallel}, \mu; t)$

$$\frac{\partial \delta f_s}{\partial t} + \dot{\mathbf{R}} \cdot \frac{\partial \delta f_s}{\partial \mathbf{R}} \Big|_{v_{\parallel}} + \dot{v}_{\parallel} \frac{\partial \delta f_s}{\partial v_{\parallel}} = -\dot{\mathbf{R}}^{(1)} \cdot \frac{\partial F_{0s}}{\partial \mathbf{R}} \Big|_{\epsilon} - \dot{\epsilon}^{(1)} \frac{\partial F_{0s}}{\partial \epsilon} . \quad (1.1)$$

The 0th/1st-order gyrocenter characteristics follow

$$\dot{\mathbf{R}}^{(0)} = v_{\parallel} \mathbf{b}^* + \frac{1}{qB_{\parallel}^*} \mathbf{b} \times \mu \nabla B,$$

$$\dot{v}_{\parallel}^{(0)} = -\frac{\mu}{m} \mathbf{b}^* \cdot \nabla B ,$$

$$\dot{\mathbf{R}}^{(1)} = \frac{\mathbf{b}}{B_{\parallel}^*} \times \nabla \langle \phi - v_{\parallel} A_{\parallel}^{(s)} - v_{\parallel} A_{\parallel}^{(h)} \rangle - \frac{q_s}{m_s} \langle A_{\parallel}^{(h)} \rangle \mathbf{b}^*,$$

$$\dot{v}_{\parallel}^{(1)} = -\frac{q_s}{m_s} \left[\mathbf{b}^* \cdot \nabla \langle \phi - v_{\parallel} A_{\parallel}^{(h)} \rangle + \frac{\partial \langle A_{\parallel}^{(s)} \rangle}{\partial t} \right] - \mu \frac{\mathbf{b} \times \nabla B}{B_{\parallel}^*} \cdot \nabla \langle A_{\parallel}^{(s)} \rangle ,$$

and particle energy $\dot{\epsilon}^{(1)} = v_{\parallel} \dot{v}_{\parallel}^{(1)} + \mu \dot{\mathbf{R}}^{(1)} \cdot \nabla B,$

where $\mu = v_{\perp}^2 / (2B)$, $B_{\parallel}^* = \mathbf{b} \cdot \nabla \mathbf{A}^*$, $\mathbf{b}^* = \nabla \times \mathbf{A}^* / B_{\parallel}^*$, and $\mathbf{A}^* = \mathbf{A} + \frac{m_s v_{\parallel}}{q_s} \mathbf{b}$.

ϕ is computed from the quasineutrality equation

$$-\nabla \cdot \left[\left(\sum_{s=i,f} \frac{q_s^2 n_s}{T_s} \rho_s^2 \right) \nabla_{\perp} \phi \right] = \sum_{s=i,e,f} q_s n_{1,s} \quad (1.2)$$

where $n_{1,s} = \int \delta f_s \delta(\mathbf{R} + \boldsymbol{\rho} - \mathbf{x}) d^6 Z$, $\rho_s = \sqrt{m_s T} / (q_s B)$, and $d^6 Z = B_{\parallel}^* d\mathbf{R} dv_{\parallel} d\mu d\alpha$.

Given the decomposition $A_{\parallel} = A_{\parallel}^{(s)} + A_{\parallel}^{(h)}$, symplectic part is computed from Ohm's law

$$\frac{\partial}{\partial t} A_{\parallel}^{(s)} + \mathbf{b} \cdot \nabla \phi = 0, \quad (1.3)$$

and the Hamiltonian part from Ampere's law

$$\left(\sum_{s=i,e,f} \frac{\beta_s}{\rho_s^2} - \nabla_{\perp}^2 \right) A_{\parallel}^{(h)} = \mu_0 \sum_{s=i,e,f} j_{\parallel,1s} + \nabla_{\perp}^2 A_{\parallel}^{(s)}, \quad (1.4)$$

$$\text{and } j_{\parallel,1s} = \int v_{\parallel} \delta f_s \delta(\mathbf{R} + \boldsymbol{\rho} - \mathbf{x}) d^6 Z. \quad (1.5)$$

Pullback scheme

Initialize markers in the phase space;

while $t < t_{\text{final}}$ **do**

for $k = 1, \dots, 4$ *step of Runge-Kutta scheme* **do**

- Compute ϕ , $A_{\parallel}^{(s)}$ and $A_{\parallel}^{(h)}$;
- Push particles according to equations of motion;
- Apply boundary conditions;

end

- Update mixed-variable δf with $\delta f_s^{(m)} \leftarrow \delta f_s^{(m)} + \frac{q_s \langle A_{\parallel}^{(h)} \rangle}{m_s} \frac{\partial F_{0s}}{\partial v_{\parallel}}$;
- Update A_{\parallel} decomposition, i.e., $A_{\parallel}^{(s)} \leftarrow A_{\parallel}^{(s)} + A_{\parallel}^{(h)}$ and $A_{\parallel}^{(h)} \leftarrow 0$;
- $t = t + \Delta t$;

end

Algorithm 1: The δf solution algorithm used in ORB5 within the pull-back scheme framework in linear setting

We devise antenna as an electrostatic potential with profile

$$\phi_{\text{ant}}(\mathbf{s}, \theta, \varphi; t) = \text{Re} \left[\sum_{I \in \mathcal{T}} h_I(\mathbf{s}) A_I e^{\hat{i}(l_1 \theta + l_2 \varphi + \Phi_I)} (c_1 + c_2 e^{\hat{i} w_{\text{ant}} t}) \right] \quad (1.6)$$

where the set $\mathcal{T} = \{(m_1, n_1), \dots\}$ includes the target mode numbers. Electromagnetic potential of antenna from Ohm's law is computed

$$\frac{\partial}{\partial t} A_{\text{ant},||}^{(s)} + \mathbf{b} \cdot \nabla \phi_{\text{ant}} = 0. \quad (1.7)$$

Eqs. of motion are adapted by setting $\phi_{\text{plasma}} \rightarrow \phi_{\text{plasma}} + \phi_{\text{ant}}$.

Integrating electrostatic antenna in the eqs. of motion

$$\dot{\mathbf{R}}^{(1)} = \dot{\mathbf{R}}_{\text{plasma}}^{(1)} + \frac{\mathbf{b}}{B_{\parallel}^*} \times \nabla \langle \phi_{\text{ant}} \rangle, \quad (1.8)$$

$$\dot{v}_{\parallel}^{(1)} = \dot{v}_{\parallel, \text{plasma}}^{(1)} - \frac{q_s}{m_s} \mathbf{b}^* \cdot \nabla \langle \phi_{\text{ant}} \rangle, \quad (1.9)$$

$$\dot{\epsilon}^{(1)} = \dot{\epsilon}_{\text{plasma}}^{(1)} - \frac{q_s}{m_s} \left[\frac{v_{\parallel} \mathbf{B}}{B_{\parallel}^*} + m_s \mu \frac{\mathbf{b} \times \nabla B}{q_s B_{\parallel}^*} + \frac{m_s v_{\parallel}^2}{q_s B_{\parallel}^*} \nabla \times \mathbf{b} \right] \cdot \nabla \langle \phi_{\text{ant}} \rangle. \quad (1.10)$$

Integrating electromagnetic antenna in the eqs. of motion

$$\dot{\mathbf{R}}^{(1)} = \dot{\mathbf{R}}_{\text{plasma}}^{(1)} + \frac{\mathbf{b}}{B_{\parallel}^*} \times \nabla \langle \phi_{\text{ant}} \rangle - \frac{\mathbf{b}}{B_{\parallel}^*} \times \nabla \langle v_{\parallel} A_{\parallel, \text{ant}}^{(s)} \rangle, \quad (1.11)$$

$$\dot{v}_{\parallel}^{(1)} = \dot{v}_{\parallel, \text{plasma}}^{(1)} - \frac{q_s}{m_s} (\mathbf{b}^* - \mathbf{b}) \cdot \nabla \langle \phi_{\text{ant}} \rangle - \frac{\mu}{B_{\parallel}^*} \mathbf{b} \times \nabla B \cdot \nabla \langle A_{\parallel, \text{ant}}^{(s)} \rangle, \quad (1.12)$$

and

$$\dot{\epsilon}^{(1)} = \dot{\epsilon}_{\text{plasma}}^{(1)} - \frac{q_s}{m_s} \left[m_s \mu \frac{\mathbf{b} \times \nabla B}{q_s B_{\parallel}^*} + \frac{m_s v_{\parallel}^2}{q_s B_{\parallel}^*} \nabla \times \mathbf{b} \right] \cdot \nabla \langle \phi_{\text{ant}} \rangle. \quad (1.13)$$

ITPA-TAE test case

Uniform profile of density/temperature for ion and electron.

Ad hoc magnetic field.

$q \in [1.71, 1.87]$, and $\beta = 0.000448$.

kinetic ion/electron.

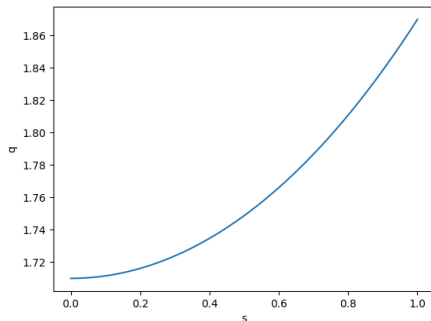
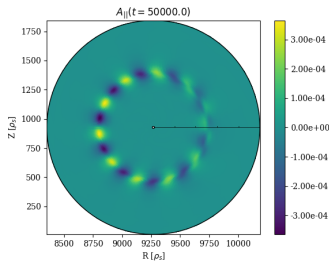
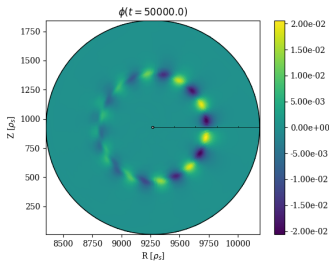
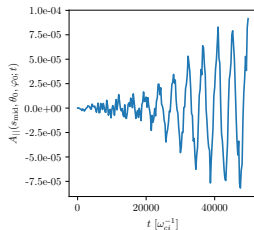
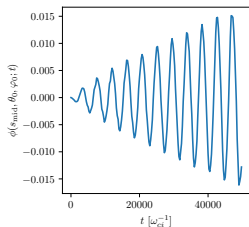
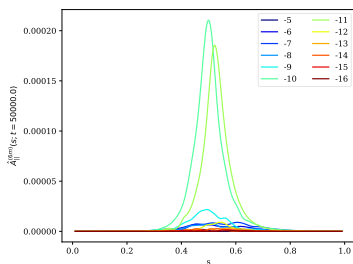
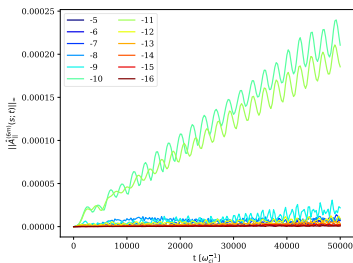
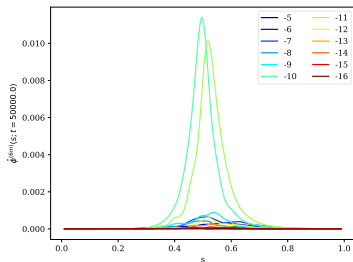
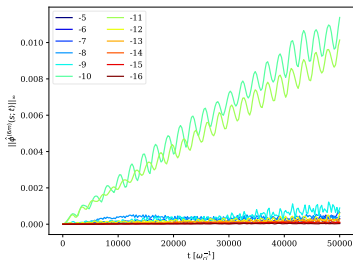


Figure: q profile

Linear simulations: $n=6, m=-11, -10$



Linear simulations: $n=6$, $m=-10,-11$



Resonance frequency .vs. fast-particle simulation result

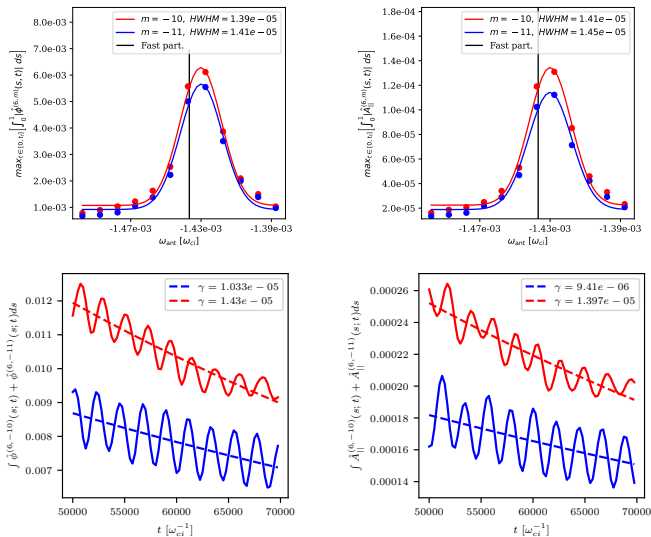
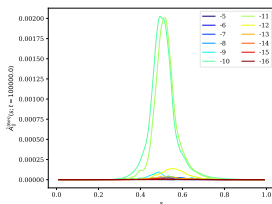
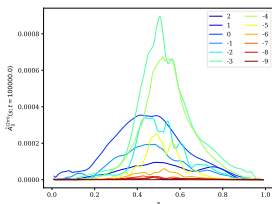
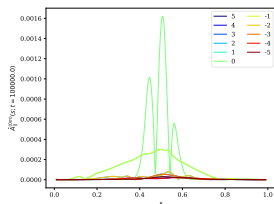
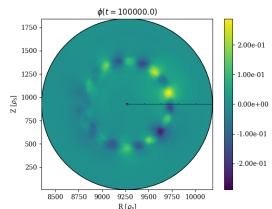
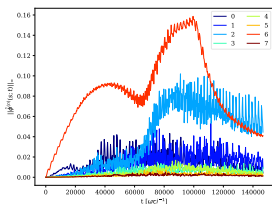
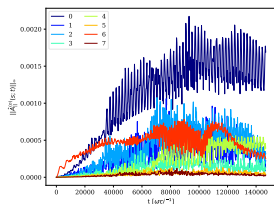
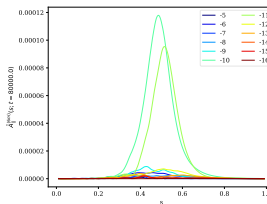
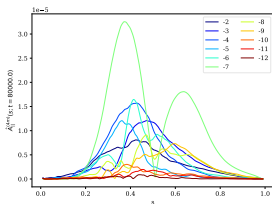
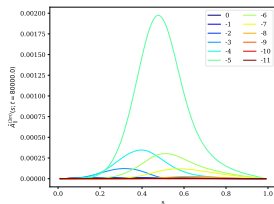
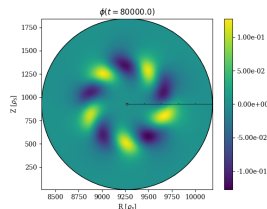
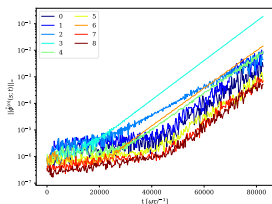
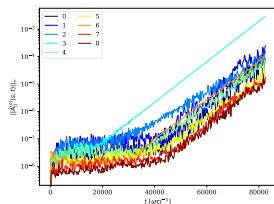


Figure: Damping rates for $\omega_{ant} = -0.00144$ (blue) and 0.00144 (red).

Nonlinear simulation ($n = 0, \dots, 18$), exciting $n = 6, m = -10, -11$ with antenna



Nonlinear simulation ($n = 0, \dots, 18$) with fast particle, no antenna



Conclusion and outlook

- An electromagnetic antenna was devised to excite TAE modes.
- Reasonable agreement with fast particle simulations in linear simulations.
- Damping rate can be measured by switching off antenna.
- First nonlinear simulations are shown.

Acknowledgements

- 1 This work is part of the EUROfusion 'Theory, Simulation, Validation and Verification' (TSVV) Task and has received funding from the European research and training programme 2019-2020 under grant agreement No. 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission. This work is also supported by a grant from the Swiss National Supercomputing Centre (CSCS) under project ID s1067.
- 2 We acknowledge PRACE for awarding us access to Marconi100 at CINECA, Italy.