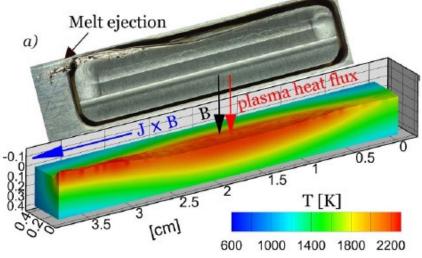
MEMOS-U describes macroscopic metallic melt motion in large-deformation long-displacement regimes, where melts spill onto progressively colder solid surfaces

Treatment of free-surface MHD flows with phase transitions

S. Ratynskaia, E. Thorén, P. Tolias *et al., NF* **60**, 104001 (2020). E. Thorén, S. Ratynskaia, P. Tolias *et al., PPCF* **63**, 035021 (2021). E. Thorén 2020 *PhD Thesis* KTH Royal Institute of Technology



MEMOS-U as per TSVV project application time

"Employs the finite difference method solving coupled Navier-Stokes and heat convection-diffusion equations. The code is already parallelized and runs on IO clusters, but would benefit from further parallelization and optimization"

Retained original MEMOS-3D architecture, lack of documentation and adaptive meshing

Currently is beeing re-written

in AMReX - open source framework for adaptive mesh refinement)

Zhang et al., (2019) Journal of Open Source Software, 4(37), 1370

- Some versions of heat and fluid solvers exist, not coupled yet
- Testing of current heat solver version (with all surface cooling fluxes and phase change) is being carried out
- No attempts of parallelization have been undertaken yet (<u>AMReX does have build-in possibilities</u>)

MEMOS-U model

$$\begin{split} \frac{\partial h}{\partial t} + \nabla_{\mathbf{t}} \cdot (h\boldsymbol{U}) &= \frac{\partial b_{1}}{\partial t} - \dot{x}_{\mathrm{vap}} \,, \\ \rho_{\mathrm{m}} \left[\frac{\partial \boldsymbol{U}}{\partial t} + (\boldsymbol{U} \cdot \nabla_{\mathbf{t}}) \, \boldsymbol{U} \right] &= \langle (\boldsymbol{J} \times \boldsymbol{B})_{\mathbf{t}} \rangle - \nabla_{\mathbf{t}} P - 3 \frac{\mu}{h^{2}} \boldsymbol{U} \\ &+ \mu \nabla_{\mathbf{t}}^{2} \boldsymbol{U} + \frac{3}{2h} \left(\frac{\partial \gamma}{\partial T} \nabla_{\mathbf{t}} T_{\mathbf{s}} + f_{\mathrm{d}} \right) \,, \\ \rho_{\mathrm{m}} c_{\mathrm{p}} \left[\frac{\partial T}{\partial t} + \boldsymbol{U} \cdot \nabla_{\mathbf{t}} T \right] &= \nabla \cdot (k \nabla T) + \rho_{\mathrm{e}} |\boldsymbol{J}|^{2} \\ &- T \frac{\partial S}{\partial T} \boldsymbol{J} \cdot \nabla T \,, \\ \nabla \cdot (\sigma_{\mathrm{e}} \nabla \psi) &= 0 \quad \text{with } \boldsymbol{J} = -\sigma_{\mathrm{e}} \nabla \psi \,, \end{split}$$

Liquid-solid phase transition: heat integration method (the enthalpy budget is kept by an extra set of algorithms)

Boundary conditions:

 $(k\nabla T - STJ) \cdot \hat{n} = q_{\rm inc} - q_{\rm cool}$, q_{inc} is the incident heat flux and and q_{cool} is the surface cooling fluxes $\sigma_{\rm e} \frac{\partial \psi}{\partial n} = J_{\rm surf}$, J_{surf} is the current density on the surface

(U) depth-averaged fluid velocity,

(h,P) melt column height, ambient pressure (J,B) current density, magnetic flux density, (b_1,\dot{x}_{vap}) solidification interface, rate of change of interface position due to vaporization, (T,T_s) bulk and surface temperature (ρ_m,c_p) mass density, heat capacity (k,S) thermal conductivity, thermoelectric power,

 (σ_e,μ_0) electrical conductivity, vacuum permeability

 (μ, γ) dynamic viscosity, surface tension