

Simulations for GyM and AUG

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General framework of PoliMi modelling activities





Outline



- 1. SOLPS-ITER modelling in GyM
- 2. Global ERO2.0 simulations in GyM
- 3. ERO2.0 erosion/deposition in AUG
- 4. ERO2.0 morphology evolution modelling

GyM linear plasma device

Vacuum vessel:	Stainless steel (SS): L = 2.11 m, Ø = 25 cm	
vacuum vessei.	(optional: SS liner with W coating)	
Pumping system:	2 turbopumps:	
	p _{base} = 1E-8 mbar, p _{work} < 1E-3 mbar	
Working gas:	H_2 , D_2 , N_2 , He , Ar , $He+NH_3$ and mixtures	





Helium databases and atomic reaction set



Objective: studying He plasma properties in GyM in order to provide a plasma background for ERO2.0 simulations

- $\sqrt{}$ Ionization (IZ) reaction rates from different databases (HYDHEL, ADAS and AMJUEL) can produce differences up to 20% in T_e and n_e
- \checkmark Including electron neutral excitation (EHL_{rad}) of He atoms (without resolving metastable states) leads to global increase in n_e
- ✓ Including charge exchange (CX) reactions between He-He⁺ and He-He⁺⁺ leads to increase in n_e , consistent with the collisional drag, and a reduction of T_e . Important effect in GyM due to high neutral density
- \checkmark New default set of reactions and database for He plasma modelling with SOLPS-ITER

SOLPS-ITER modelling in GyM

Investigation of He metastable states (MS) in low-temperature plasmas

- Implementation of MS resolved model (ADAS rate coefficients, left figures) in the 0D model [Tonello E. et al, NF 2021], already benchmarked with SOLPS-ITER.
- Results show small difference between metastable resolved and un-resolved models in GyM conditions (right figures)



Fig. Reaction rate coefficients (ADAS) for He with metastables resolved (left). Results of OD model resolved vs. un-resolved (right).

SOLPS-ITER modelling in GyM



Benchmark of SOLPS-ITER simulations with experimental LP data from GyM

 Optimisation of simulation input (recycling coefficients, D_n, P_{ext}) to obtain good agreement with GyM experimental Langmuir probes (LP) data in the full machine configuration



SOLPS-ITER modelling in GyM







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Global ERO2.0 simulations in GyM



Objective: Exploiting the coupling between SOLPS-ITER and ERO2.0 in a linear plasma device to study erosion of internal walls and impurity migration in GyM helium plasma



(a) 3D plasma background for ERO2.0

- 2D SOLPS-ITER plasma background interpolated on the (x, y) plane of 3D ERO2.0 mesh
- Axial symmetry is assumed

(b) 2D ERO2.0 domain boundary

- 2D SOLPS-ITER plasma background is extrapolated up to this boundary
- Axial symmetry is assumed



(c) 3D GyM wall structures

- Used by ERO2.0 to assess erosion/deposition of walls (bases and lateral wall of vacuum chamber and bushings)
- Drawn in CAD: no axial symmetry required

Global ERO2.0 simulations in GyM



Varied parameters:

GyM vacuum chamber material

Bias voltage applied to the walls





Main results:

Erosion rate (atoms/s)

- Lowest erosion for **W** (not eroded for $V_{\text{bias}} < 110 \text{ V}$), highest for **Fe**
- Bases and bushings are main erosion sources, lateral wall main deposition zone
- Deposition on lateral wall generally increases at high V_{bias}



Gross erosion



Deposition

0 20

100 200

Bases and bushings biasing voltage (V)

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20 100 200

0

20 110 200

0

Global ERO2.0 simulations in GyM

Angular distribution of erosion is studied on lateral surfaces of bushings:

- *a.* \vec{B} impinges on lateral side of GyM bushings: full distribution for He plasma ions incidence angle (no sheath-tracing model is used)
- b. poloidal plot shows erosion normalised to the peak values for each material

The angular position of the peak depends on two opposite effects: Y increases towards grazing incidence (higher erosion); the flux decreases towards grazing incidence (lower erosion)

The variation of $Y(\theta)$ **depends on the material:** e.g. for W mild $Y(\theta)$ dependence = maximum erosion at normal incidence $(\theta = 90^{\circ})$ Normalised erosion





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Previous AUG erosion/deposition experiments

- Eight L-mode D-plasma discharges (#35609-35617)
- Measured erosion of Mo and Au markers close to outer strike point (OSP)
- ERO1.0 modelling to simulate markers erosion/deposition in small volume around markers
- W, C, B and N impurities considered in plasma for ERO modelling

Objective of our work: Exploiting ERO2.0 extended simulation volume to estimate role of impurities eroded from FW on divertor markers erosion



Simulations setup

- **D plasma** from SOLPS-ITER with C (1.0%) and W (0.01%) impurities
- 80° sector with periodic BC
- **3D full-W** wall divided into 6 parts to distinguish impurity sources
- Inner core boundary at 0.7 r_{sep}
- Single time step of 1s

Analyzed parameters

- Plasma shadowing effects (- 50% of erosion)
- Migration studied from each FW component individually
- Extrapolation method of SOLPS-ITER solution to the wall
- Plasma w/o **W** impurities
- Multiple time steps

ERO2.0 erosion/deposition in AUG





Contribution to divertor erosion from different PFCs

3 different simulations: a) Upper wall erosion, b) Inner wall erosion, c) Outer wall erosion

- Highest contribution to **outer divertor** erosion due to plasma, W particles eroded from outer wall contribute to about 6% (only outer wall considered in the following)
- Highest probability of reaching **core** for **inner wall W** impurities



a. Upper wall b. Inner wall c. Outer wall Core 5.7 46.8 reflection [%]



12.7



Effect of particle charge on impurity migration

W particles eroded from outer wall

- Lower ionized W impurities more localized near production areas
- Particles in higher ionization states can migrate towards different PFCs (main contributors to outer divertor erosion)





Effect of extrapolation method of SOLPS-ITER plasma to 3D walls

4 different simulations, varying from constant extrapolation to exponential decay with different characteristic lengths λ (10, 1 and 0.1)

- Outer wall erosion deeply affected by extrapolation method (about factor 200 reduction, compared to < factor 3 for outer divertor)
- As a consequence, contribution of outer wall impurities on divertor erosion decreases at lower λ
- Probability of reaching **core boundary** for outer wall impurities **increases at lower** λ due to lower plasma density and temperature at edge



	Constant	λ = 10	λ = 1	$\lambda = 0.1$
Divertor erosion rate [10 ¹⁶ /m ² s]	3.46	3.28	2.55	1.40
Outer wall erosion rate [10 ¹⁶ /m ² s]	26.4	23.2	7.90	0.14
Core reflection [%]	12.7	14.8	32.8	215



Effect of W impurities in the plasma

- Removing W impurities (0.01%) in D plasma deeply affects divertor erosion (> factor 10 reduction, compared to < factor 2 for outer wall)
- As a consequence, the contribution of W particles eroded from outer wall to divertor erosion increases (14.4% against previous 6.0%)

	w/o W in plasma	with W in plasma
Divertor erosion rate [10 ¹⁶ /m ² s]	0.24	3.46
Outer wall erosion rate [10 ¹⁶ /m ² s]	16.3	26.4
W from FW contribution [%]	14.4	6.0

Effect of multiple time steps

Up to 10 time-steps for a total of **10s discharge** simulated

• No significant differences observed for the reported global results (local effects observed, especially regarding erosion of plasma shadowed areas)



Molybdenum (Mo) as outer divertor material

- Mo presents 30 times higher erosion wrt W, especially due to D-plasma
- Almost doubled erosion due to W from FW for Mo
- Erosion % due to FW W decreases for Mo

	W divertor	Mo divertor
Divertor erosion rate [10 ¹⁶ /m ² s]	0.24	8.27
W from FW contribution [%]	14.4	0.8



Further developments:

- Comparison with experimental data and ERO1.0 modelling
- Consider also erosion from CX neutrals



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ERO2.0 morphology evolution modelling: experimental results



Motivation : Previous work showed the dependence of ERO2.0 morphology evolution on few numerical parameters, e.g. time step and mesh resolution

Samples production and exposure

- pyramidal surfaces produced by chemical etching of Si wafers (@ ISTP-CNR) with different average surface roughnesses (300-600-900 nm)
- Deposition of compact W coating by means of HiPIMS technique (@ PoliMi)
- New exposure @ 350 eV to enhance samples erosion

Before and after exposures

- weighing to evaluate erosion using balance @ CNR-Mi
- AFM for topography evolution @ ISTP
- SEM morphology evolution @ PoliMi
- SEM statistical analysis of coating thickness variation in cross section @ PoliMi





ERO2.0 morphology evolution modelling: experimental results



Net erosion statistical analysis

- $\Delta s_{flat} > \Delta s_{pyra}$ as expected in literature
- Δs_{faces} > Δs_{valleys}: possible deposition of sputtered particles from faces to valleys
- Further work needed to reduce uncertainty

350 eV	Flat	Pyr. Ra = 900 nm		
		Faces	Valleys	
$\overline{\Delta s}[nm]$	60.7	49.4	34.6	
$\sigma_{\Delta s}[nm]$	17.0	29.9	35.9	

Less erosion than expected from Y_{sputt}!





ERO2.0 morphology evolution modelling: ERO2.0 modelling



- ERO2.0 overestimates erosion of all samples, in agreement with available sputtering yields
- ERO2.0 predicts more morphology variations than observed in experiments (fig. b)
- Y_{rough}/Y_{flat} well reproduces experimental data for all roughnesses (fig. c)

Strategy: fixing physical parameters for quantitative agreement with flat surface and vary numerical ones to morphology evolution of pyramids





Thank you for your attention!



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