

Analysis of triangularity effects on edge turbulence with the GBS code

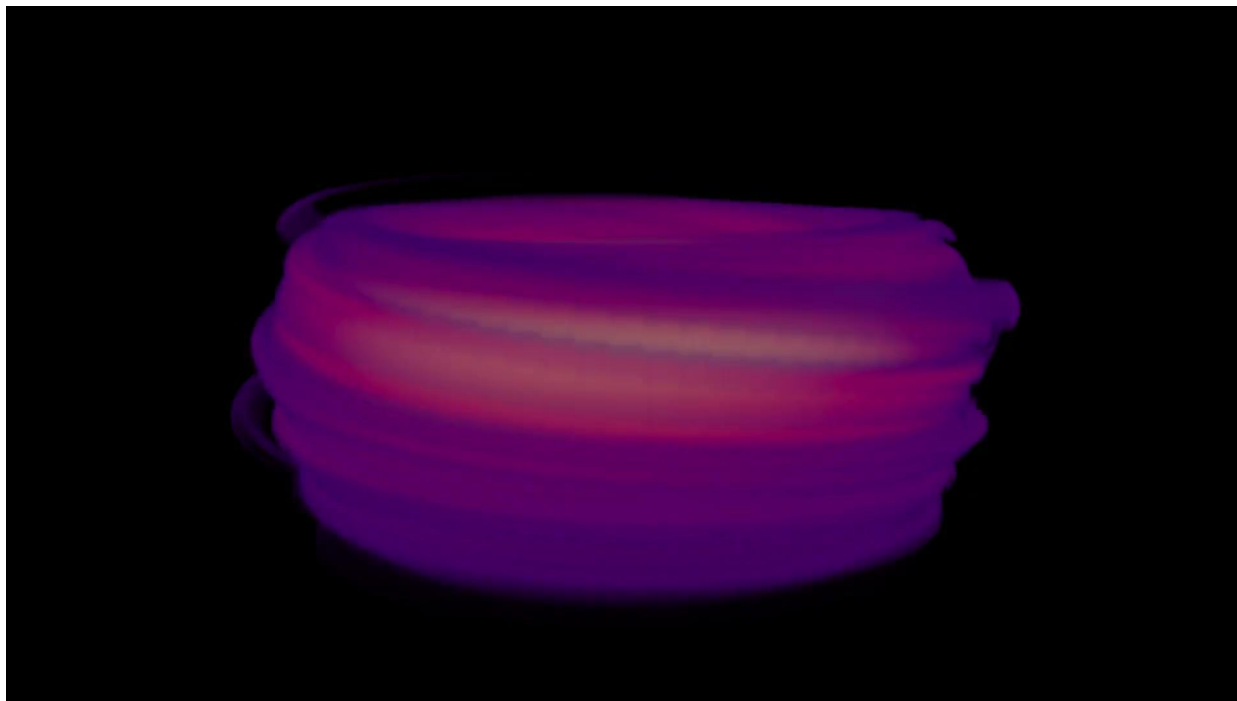
Kyungtak Lim and team GBS

École Polytechnique Fédérale de Lausanne (EPFL), Swiss Plasma Center (SPC), Switzerland

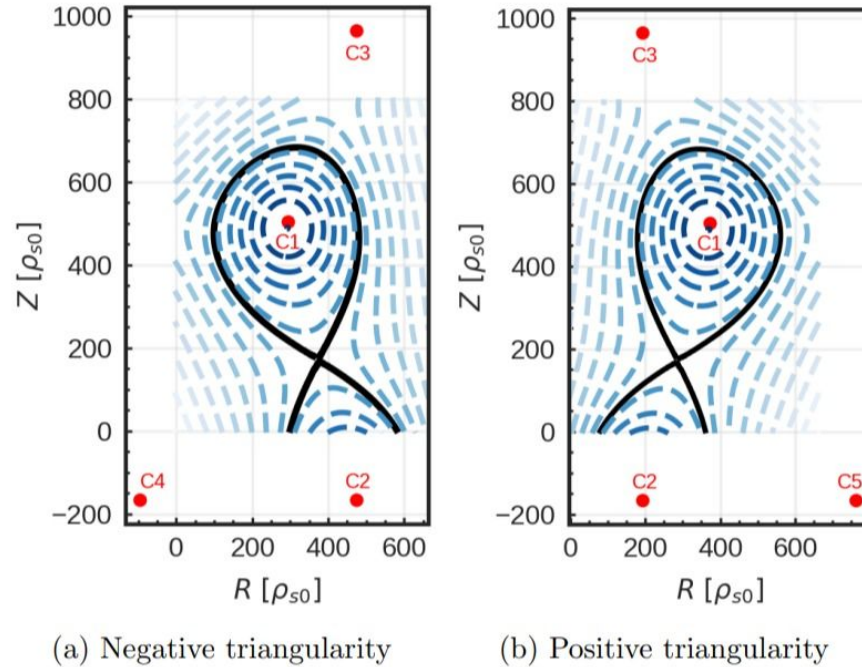
Perform GBS simulations

1. different triangularity (NT and PT)
2. different plasma resistivity and heating power

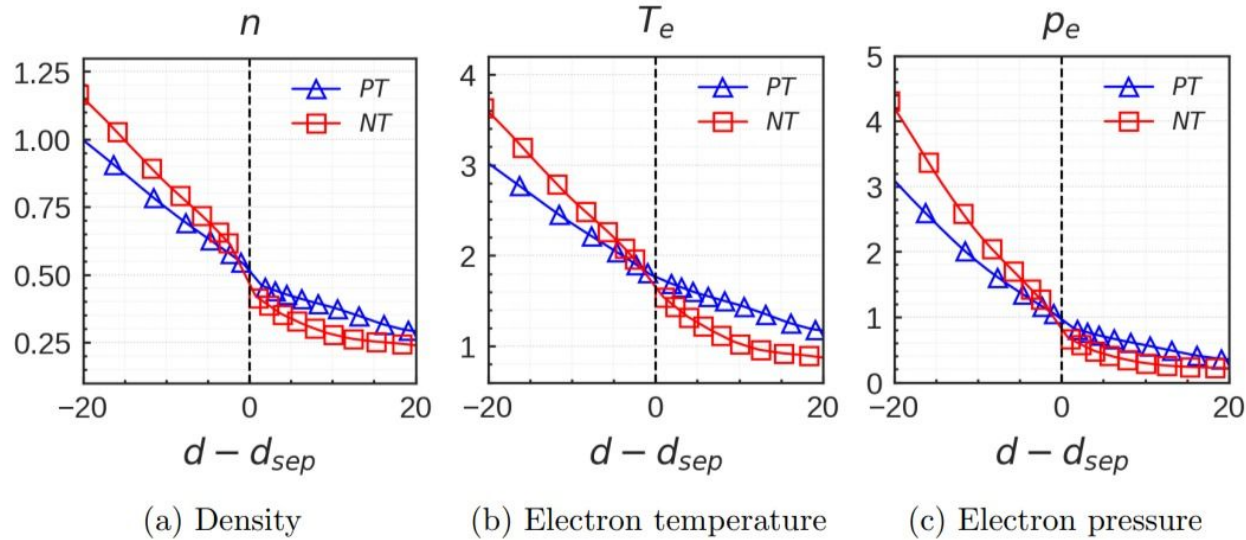
Compared to core plasma, few works have been done for effects of NT on edge plasma turbulence



Two-fluid, self-consistent, global, flux-driven turbulence code



By manipulating external currents, NT/PT ($\delta = \pm 0.3$) configurations obtained
 Adjust current to have $q_{95} \sim 4$ for both cases



Reduced edge plasma turbulence -> enhanced confinement
i.e. steep nT_p gradients in NT, strong shear rate, reduced correlation length

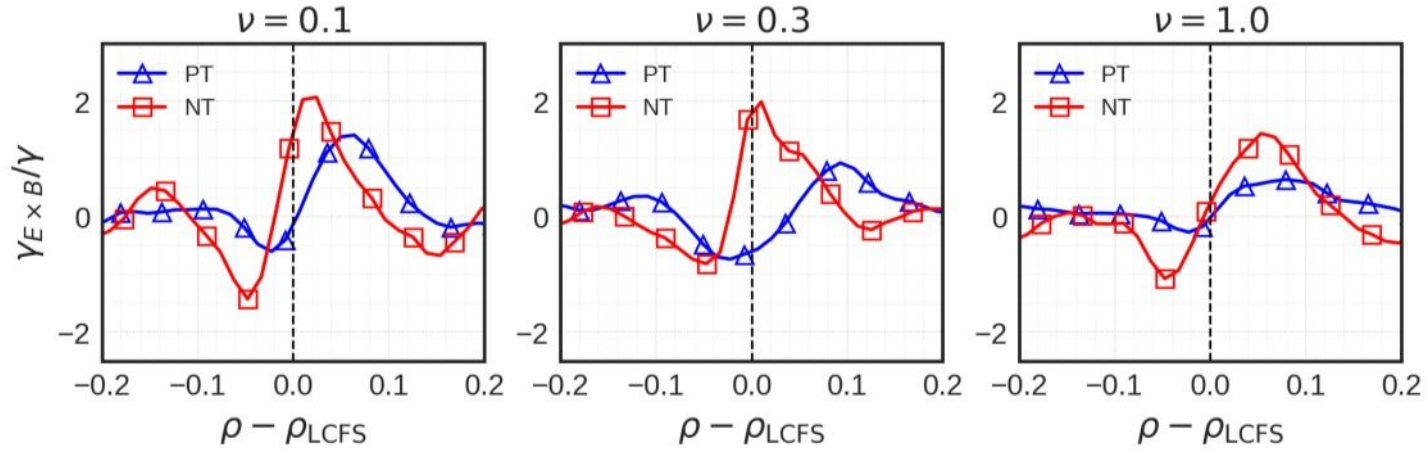


Figure 5: $E \times B$ shear rate normalized by background turbulence growth rate for NT and PT plasma near the separatrix.

Reduced edge plasma turbulence -> enhanced confinement
 i.e. steep nT_p gradients in NT, strong shear rate, reduced correlation length

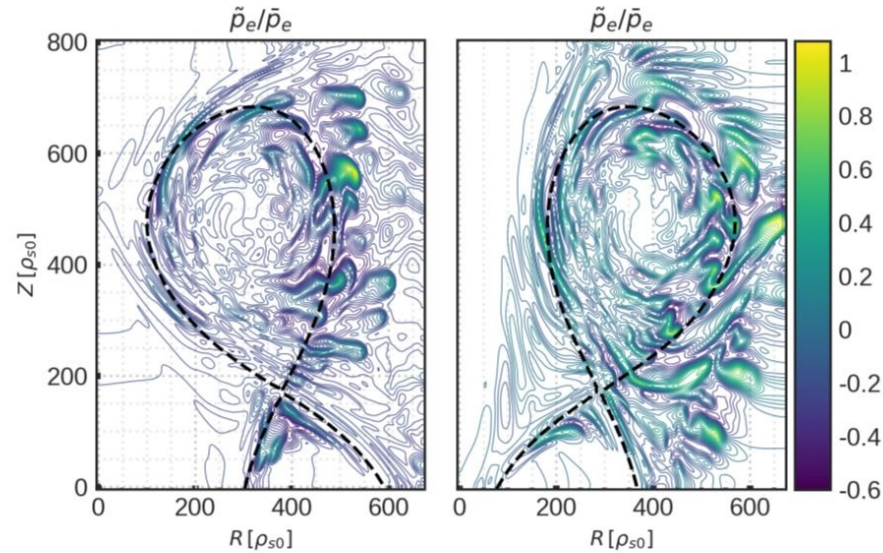


Figure 6: Snapshot of the normalized electron pressure fluctuation for NT/PT plasma with $s_{T0} = 0.025$ and $\nu = 1.0$.

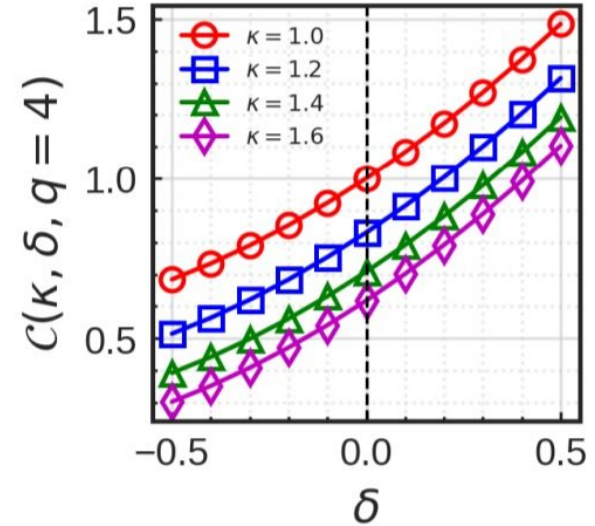
Reduced edge plasma turbulence -> enhanced confinement
i.e. steep nT_p gradients in NT, strong shear rate, reduced correlation length

Reduction of magnetic curvature drive of interchange instabilities

Geometrical operators in GBS

$$\begin{aligned}
 [\phi, f] &= \mathcal{P}_{xy}[\phi, f]_{xy} + \mathcal{P}_{yz}[\phi, f]_{yz} + \mathcal{P}_{zx}[\phi, f]_{zx} \\
 \nabla_{\parallel} f &= \mathcal{D}^x \frac{\partial f}{\partial x} + \mathcal{D}^y \frac{\partial f}{\partial y} + \mathcal{D}^z \frac{\partial f}{\partial z} \\
 \mathcal{C}(f) &= \mathcal{C}^x \frac{\partial f}{\partial x} + \mathcal{C}^y \frac{\partial f}{\partial y} + \mathcal{C}^z \frac{\partial f}{\partial z} \\
 \nabla_{\perp}^2 f &= \mathcal{N}^x \frac{\partial f}{\partial x} + \mathcal{N}^y \frac{\partial f}{\partial y} + \mathcal{N}^z \frac{\partial f}{\partial z} + \mathcal{N}^{xx} \frac{\partial^2 f}{\partial x^2} + \mathcal{N}^{xy} \frac{\partial^2 f}{\partial x \partial y} \\
 &\quad + \mathcal{N}^{yy} \frac{\partial^2 f}{\partial y^2} + \mathcal{N}^{xz} \frac{\partial^2 f}{\partial x \partial z} + \mathcal{N}^{yz} \frac{\partial^2 f}{\partial y \partial z} + \mathcal{N}^{zz} \frac{\partial^2 f}{\partial z^2}
 \end{aligned}$$

Analytical formula of curvature operator at outer mid plane



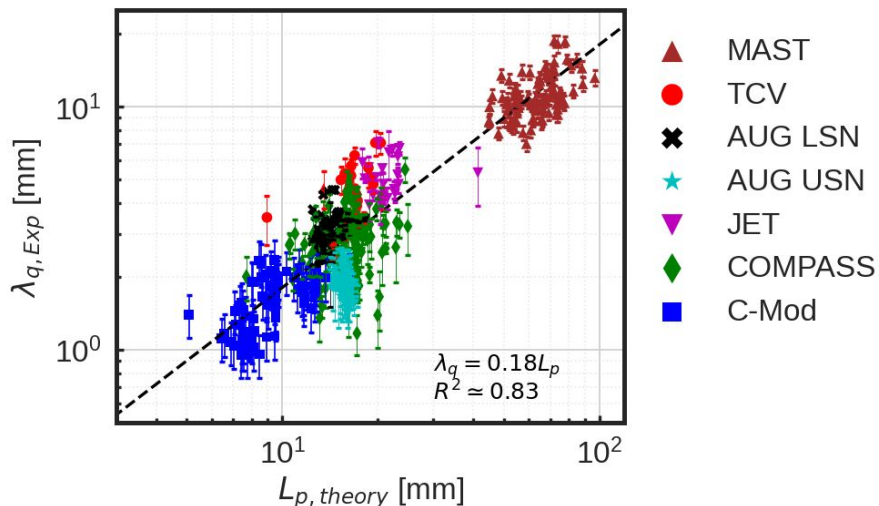
By equating input heating power and outward heat flux (steady state), one can derive analytical expression of SOL width

$$L_{p,theory} \simeq 1.95 C(\kappa, \delta, q)^{9/17} A^{1/17} q^{12/17} R_0^{7/17} P_{SOL}^{-4/17} n_e^{10/17} B_T^{-12/17} L_\chi^{12/17}$$

Extrapolation to larger machines

Parameter	ITER	DTT	SPARC	JT-60SA
R_0 [m]	6.2	2.1	1.85	2.96
a [m]	2	0.6	0.57	1.18
q	2	3	3	3
κ	1.85	1.7	1.97	1.95
δ	0.49	0.3	0.54	0.53
\bar{n}_e [m ⁻³]	4×10^{19}	1.8×10^{20}	3.1×10^{20}	6.3×10^{19}
B_T [T]	5.3	6	12.2	2.3
P_{SOL} [MW]	18	15	29	10
$\lambda_{q,PT}$ [mm]	~3.7	~2.7	~2.3	~7.1
$\lambda_{q,NT}$ [mm]	~2.2	~1.8	~1	~3.3

Table 1: Power fall-off length extrapolation of future tokamaks for NT/PT L-mode plasma. The values of $\lambda_{q,NT}$ are computed using $-\delta$ in the scaling law.



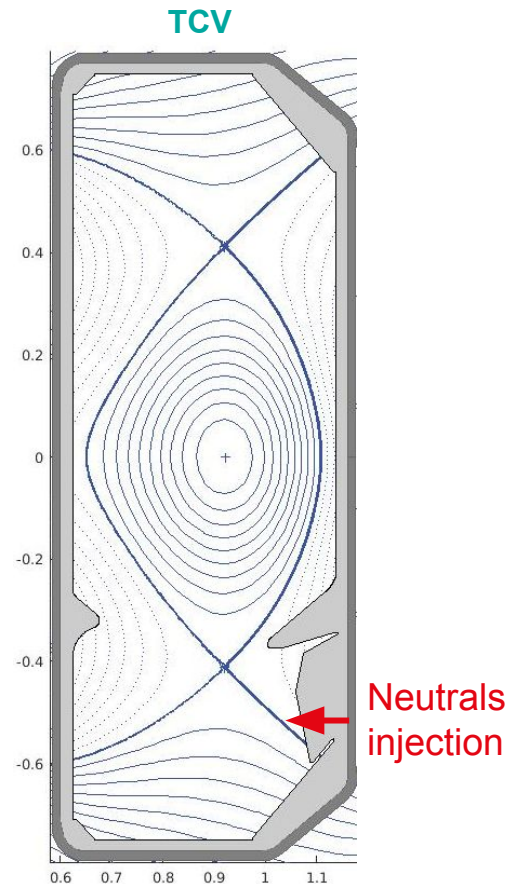
During 6th cycle, NT/PT plasma in SN simulations

During 7th cycle, we plan to

- perform double-null (DN) simulations
- impose triangularity
- add neutrals

focusing on heat mitigation in DN + NT + neutrals

with detached conditions



Simulations of detachment are carried out with GBS in single-null

Detachment achieved with neutral injections

I will explore the transition to detached conditions compatible with high confinement regimes

