

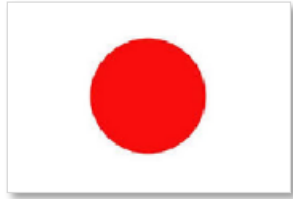


# Status of the PLS and the "Design 100" proposal

P. T. Lang for the PLS Team



This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement number 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.



Go Matsunaga

Satoshi Yamamoto

Sigetoshi Nakamura

Isayama Akihiko



Peter Lang

Bernhard Ploeckl

Jörg Tretter

Carla Piccinni



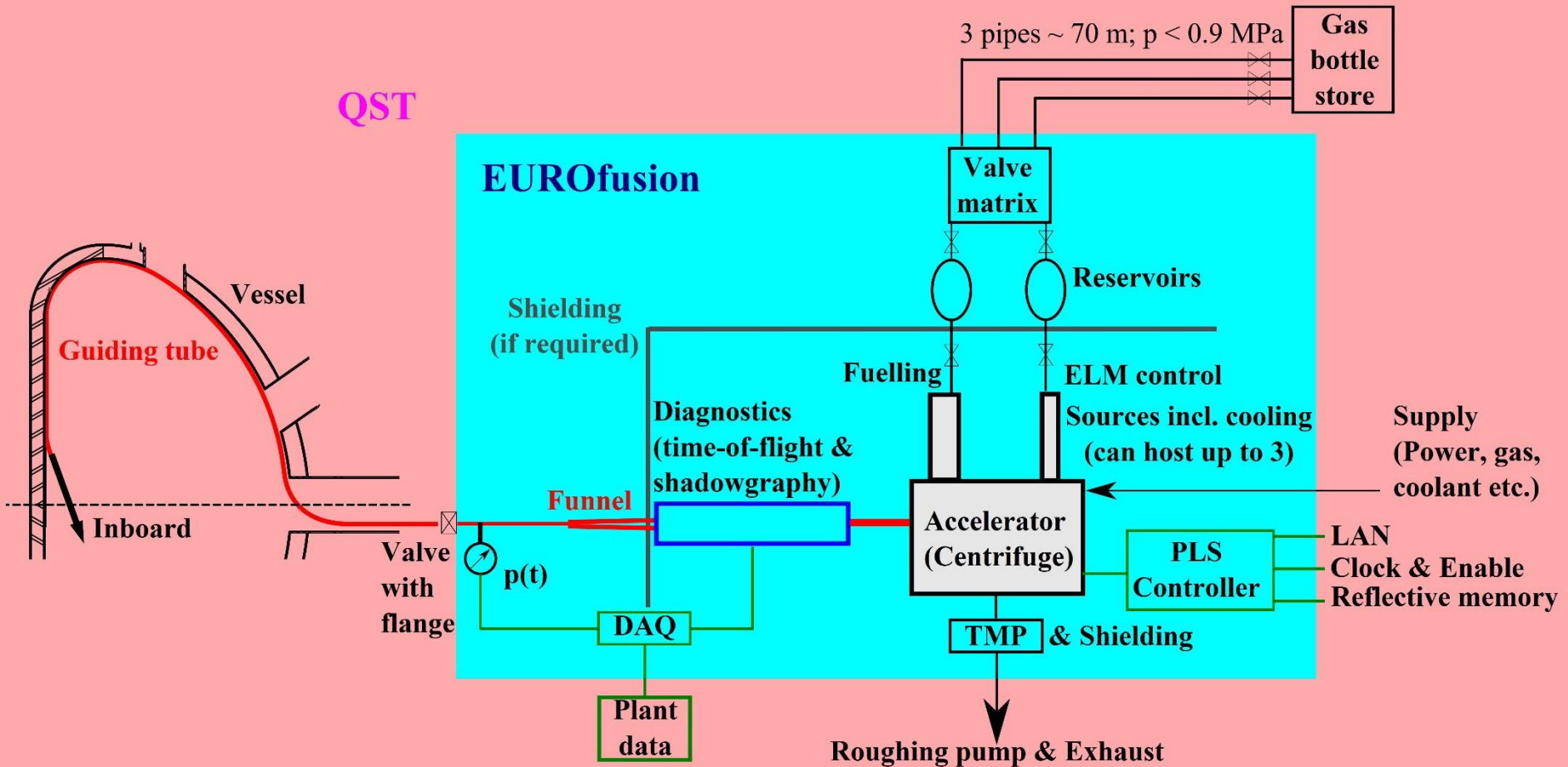
Sam Davis

Manfred Wanner

# PELLET LAUNCHING SYSTEM LAYOUT



PLS scheme with projected responsibility as shared between QST and EUROfusion



Status since first working meeting in Naka (February 2019)



## Achievements since 6<sup>th</sup> WPSA PPM Sevilla

- **Enhancement Project ongoing**

Contracts for both extruders negotiated

Call for tender “Centrifuge” in preparation

Preparation for diagnostics ongoing

- **Team modifications and enhancements**

Cooperation with 3<sup>rd</sup> QST pellet team established

(Satoshi Yamamoto, Shigetoshi Nakamura)

-> In-vessel guiding tube, QST –EUROfusion Interfaces

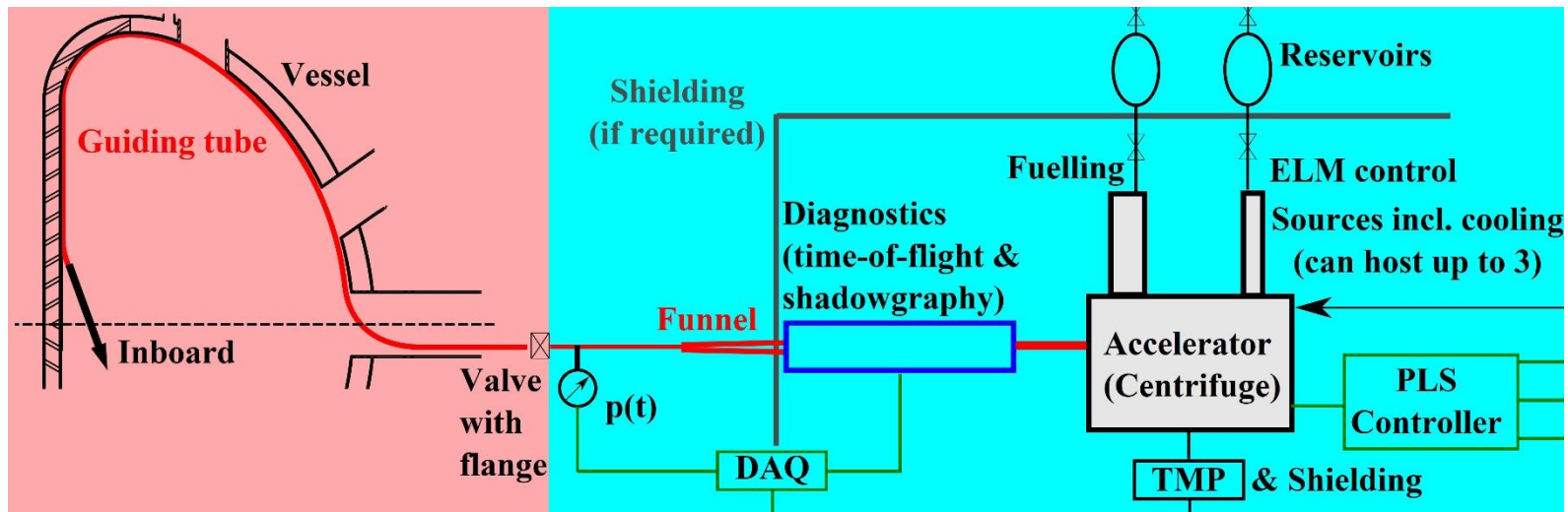
IPP pellet team reinforced by Carla Piccinni (EE Grant)

- Contribution to EPS submitted (after triple clearance)

# Overview



- Guiding tube
- Extruders
- Interface Extruders-Centrifuge
- Centrifuge design
- Diagnosing during R&D phase
- The “Design 100” proposal



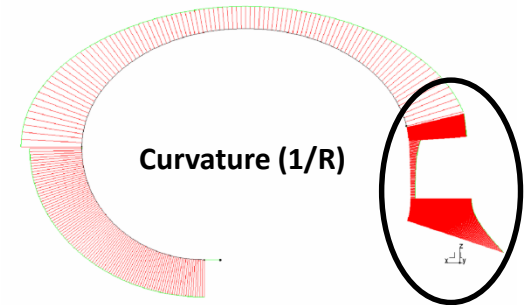
# GUIDING TUBE DESIGN



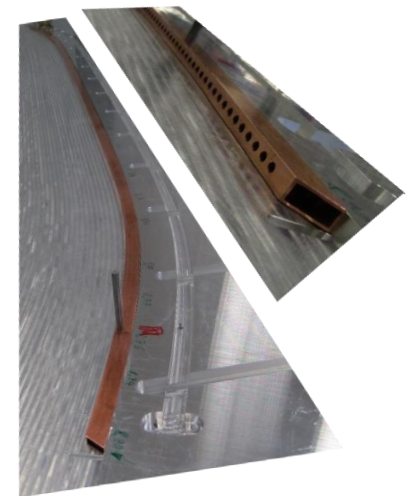
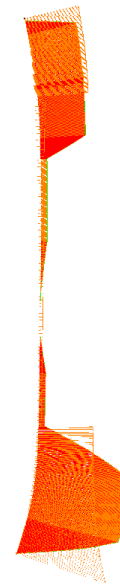
AUG had to replace in-vessel guiding tube due to corrosion after steam leak damage



Old track:  
Steps in curvature  
Lowest R in final part



New track:  
Avoid steps in curvature  
Applying clothoid shape  
(Cornu spiral:  $L \sim 1/R$ )  
Improved maintainability  
Revised system commissioned and showed sound behaviour



# GUIDING TUBE DESIGN



Replacement of in-vessel guiding tube on AUG  
QST team visited and watched...

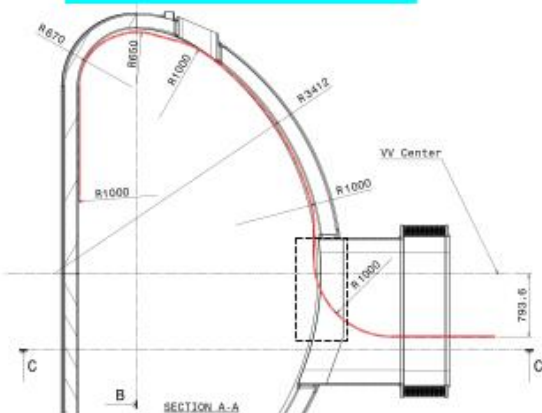


... and decided to follow the AUG approach

# GUIDING TUBE DESIGN (Yamamoto, TCM34)



## Current routing



✓ Optimization of guiding tube (GT) is ongoing.

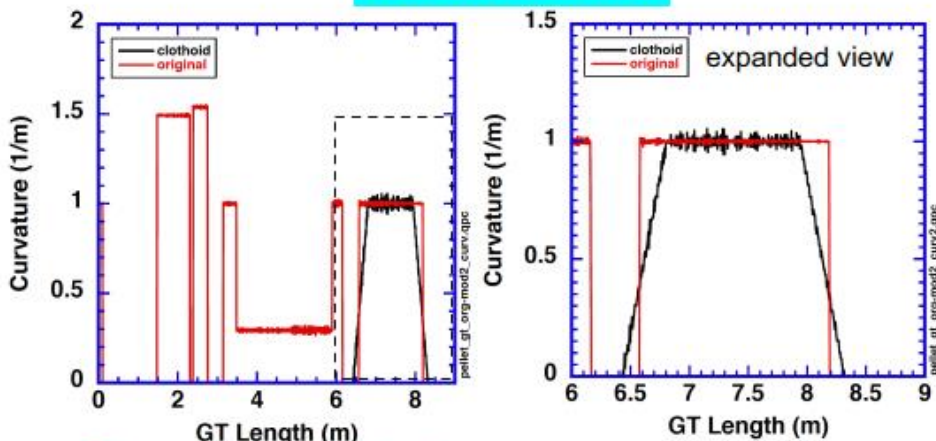
- Find better routing of GT
- Apply clothoid curve to have gentle change of curvature
- Pellet speed depends upon effective radius  $R_{eff}$

➔  $R_{eff} \sim 343$  (m) [current route]

➔ critical trans.  $v_c \sim 435$  (m/s)

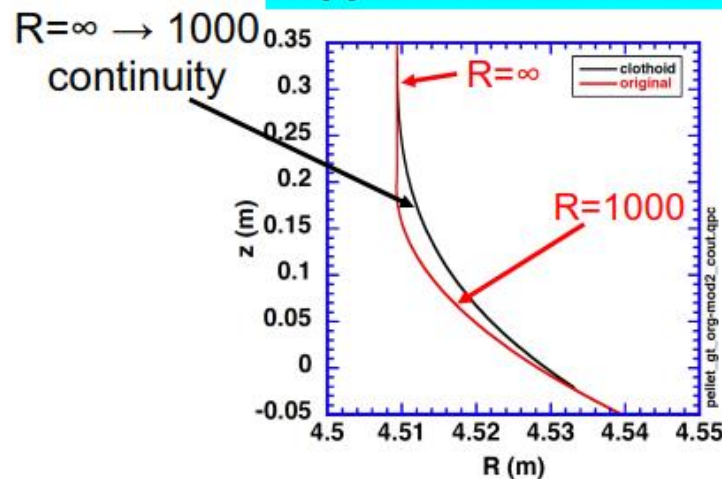


## Curvature 1/R



Discontinuity (original) & Continuity (clothoid) 1/R

## Application of clothoid



Optimisation still under way – Tests envisaged to determine  $v_c$





Procurement contracts in preparation

## **Fuelling extruder:**

$D = L = 2.4 \text{ mm}$  ( $10.8 \times 10^{20} \text{ e}$ ) at 20 Hz →  $2.2 \times 10^{22} / \text{s}$  flux

Throughput  $350 \text{ mm}^3/\text{s}$  but priority sound pellets at 20 Hz

Operation with D, H, HD mixture, doping (e.g. N, Ne) up to 2%

## **Pacing extruder:**

$D = L = 1.2 \text{ mm}$  at 50 Hz

Throughput  $100 \text{ mm}^3/\text{s}$  but priority sound pellets at 50 Hz

Operation with D, H, HD mixture

Size flexibility (D/L optional 1.2, 1.5, 2.4 mm)

→ 9 possible pellet sizes possible (only 5 useful)

# INTERFACE EXTRUDERS-CENTRIFUGE



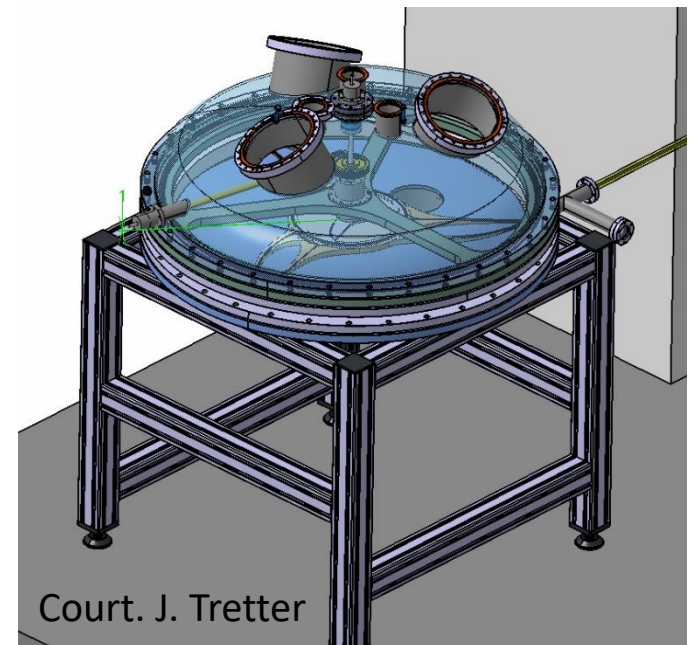
The feed-in from the extruders to the stop cylinder is considered as the technical key issue of the PLS

Feed-in from up to three sources

Steady state extrusion requires “high” ice temperature

➔ High repulsion force from ablating gas

IPP- engineer dedicated to this task



Court. J. Tretter

# DESIGN CENTRIFUGE



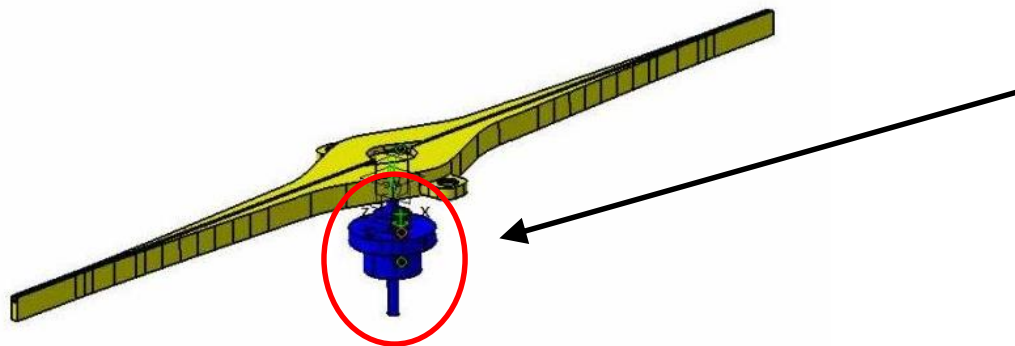
Call for tender in preparation

Centrifuge design, in particular stop cylinder design, must be compatible with extruder design

Layout, in particular launch speed, must be compatible with guiding tube design ( $v_c$ )

Modernized approach with magnetic fluid sealed rotary feedthrough:

Tests up to 85 mT without problems





Several tasks assigned to diagnostics & ...:

- Monitoring ice extrusion/pellet production
- Monitoring pellet behavior in stop cylinder
- Measure pellet speed and mass/size at PLS exit (later @ torus valve)

For first extruder tests:

Analysis of ice quality and extrusion speed

Suggestion: take solution chosen for IPP-ORNL project

Project aim: investigate  $> 10$  s extrusion for

H, D, D with up to 2% Ne ice,  $D = 1.9$  or  $2.4$  mm

Straight or  $90^\circ$  bend extrusion geometry

*Double extrusion die*

Video observation, analysis by “Optical flow” tool



## Video:

- Original overview
- Zimmermann part full speed
- Zimmermann part 5x slowmo

# “DESIGN 100” Proposal



In a centrifuge accelerator, there is a correlation between

Revolution frequency - Pellet speed – Pellet rate – Pellet flux

Set by the design parameters:

Driving potential (-> minimum and maximum revolution frequency)

Number of acceleration arms

Stop cylinder diameter

Outer acceleration arm diameter

There are many combinations possible

Initial design had potential to achieve pellet rate up to 600 Hz

Advantage: high temporal resolution for pellet investigations (1.7 ms)

Disadvantage: high technical effort for centrifuge and local controller

With designed extruders (20 Hz fuelling and 50 Hz pacing):

Max pellet rate of 70 Hz

# “DESIGN 100” Proposal



During PLS working meeting 2/2019 it became clear:

The SCSDAS density and heating controller has a response time of 10ms

Regarded sufficient for proper parameter adjustment

Energy and particle confinement times are significantly longer

→ Same response time regarded sufficient for the PLS control system

Assume PLS controller has  $dt = 10 \text{ ms}$ :

Can select any available pellet per SCSDAS cycle

→ Simple and straightforward control approach

In order to get PLS controller capable for  $f_p > 100 \text{ Hz}$ :

Needs to launch “pellet bursts” within one SCSDAS cycle

→ Needs internal sequence handling – Complicated! → Disregarded

# “DESIGN 100” Proposal



New approach for centrifuge drive:

Use of a magnetic fluid sealed rotary feedthrough

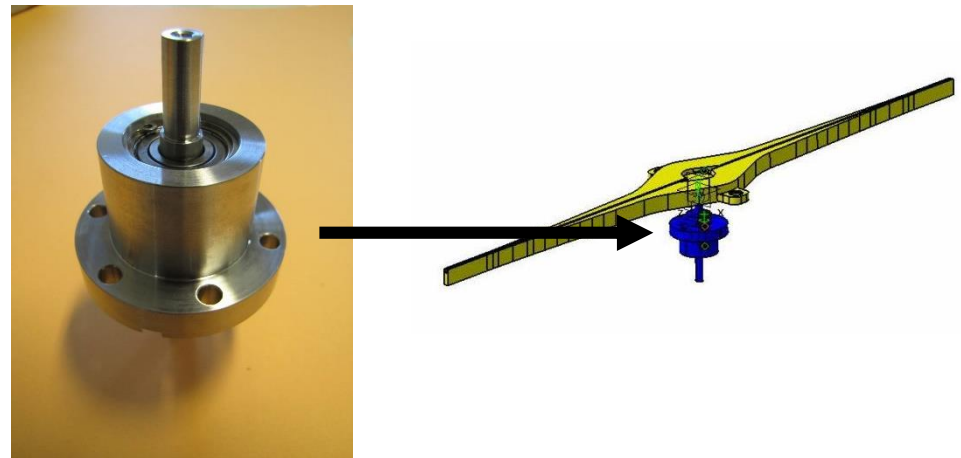
➔ Installation of the motor on atmosphere

Expected possible up to

166 Hz revolution rate

Expected simple up to

100 Hz revolution rate



Initial design proposed multi arm acceleration scheme

Possible, but requires high temporal and spatial accuracy

Single inner arm scheme relaxes these requirements



# “DESIGN 100” Proposal



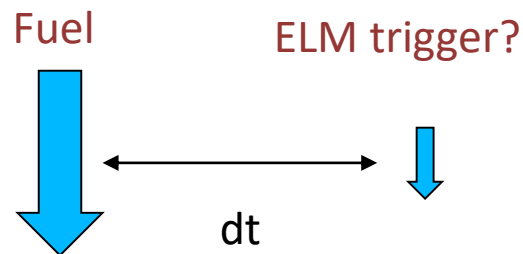
Adjust PLS layout to SCSDAS density controller response time of 10 ms:

PLS “Design 100”

- ▶ Centrifuge revolution frequency 100 Hz
- ▶ Single inner arm scheme (keep at least double outer arm)
- ➔  $dt = 10$  ms (upgrade to 5 ms if required adding second inner arm)

Maximum averaged pellet rate of 70 Hz not limited

Small caveat: Fast “probing” experiments restricted to  $dt = 10$  ms as well



# “DESIGN 100” Proposal

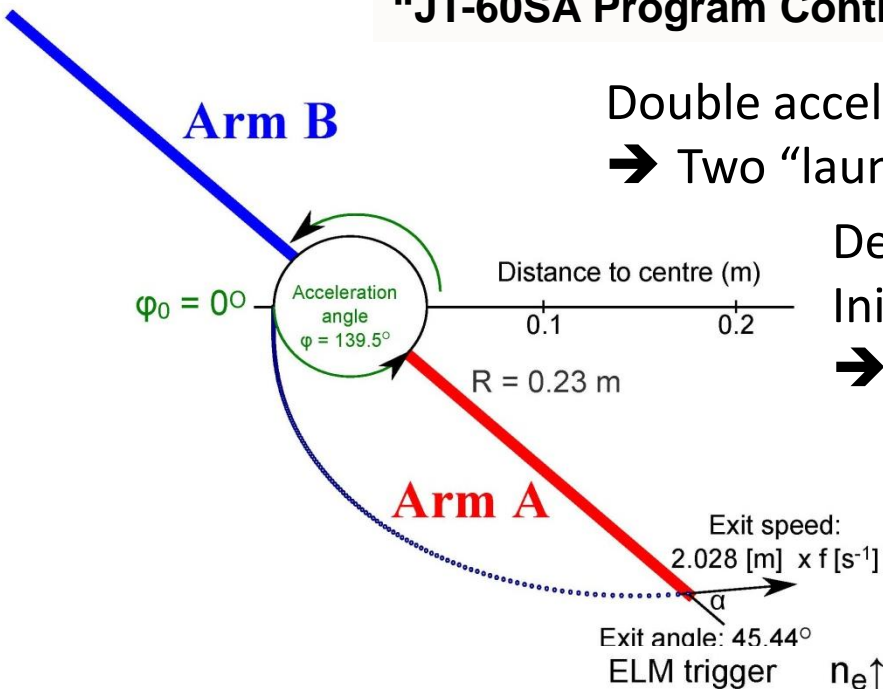


Y. Kamada, Invited talk, SOFT 2018  
 “JT-60SA Program Contribution to Fusion Energy”

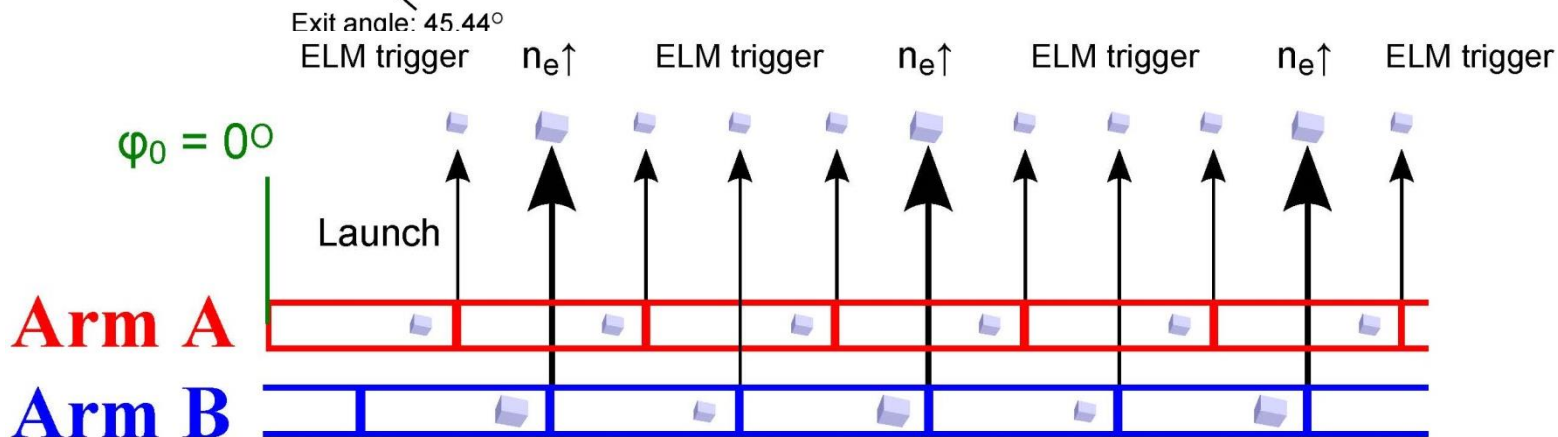
Double accelerator arm approach:

➔ Two “launching slots” per revolution

Design can host up to 3 different extruders  
 Initial configuration employing 2 extruders  
 ➔ Variability during experiment, e.g.



Combined fuelling & pacing



# “DESIGN 100” Proposal

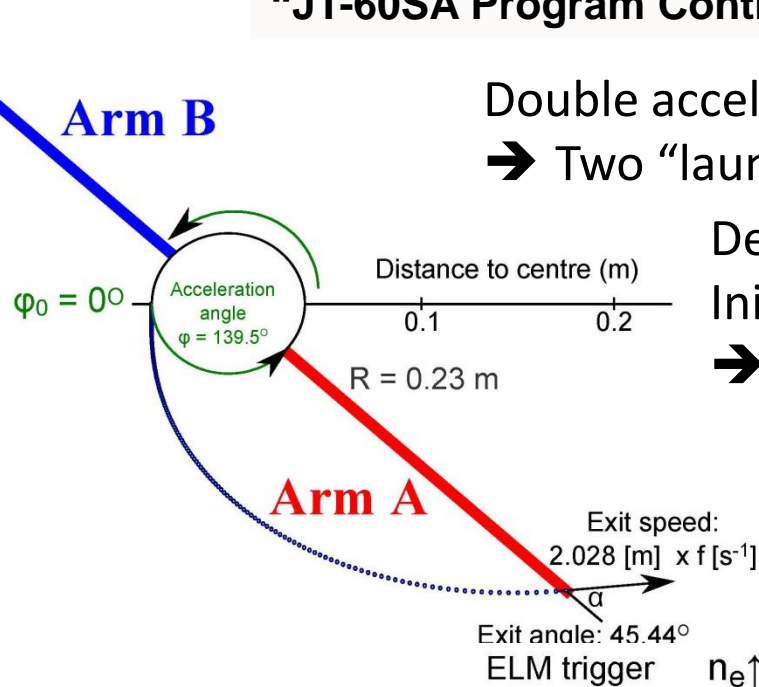


Y. Kamada, Invited talk, SOFT 2018  
“JT-60SA Program Contribution to Fusion Energy”

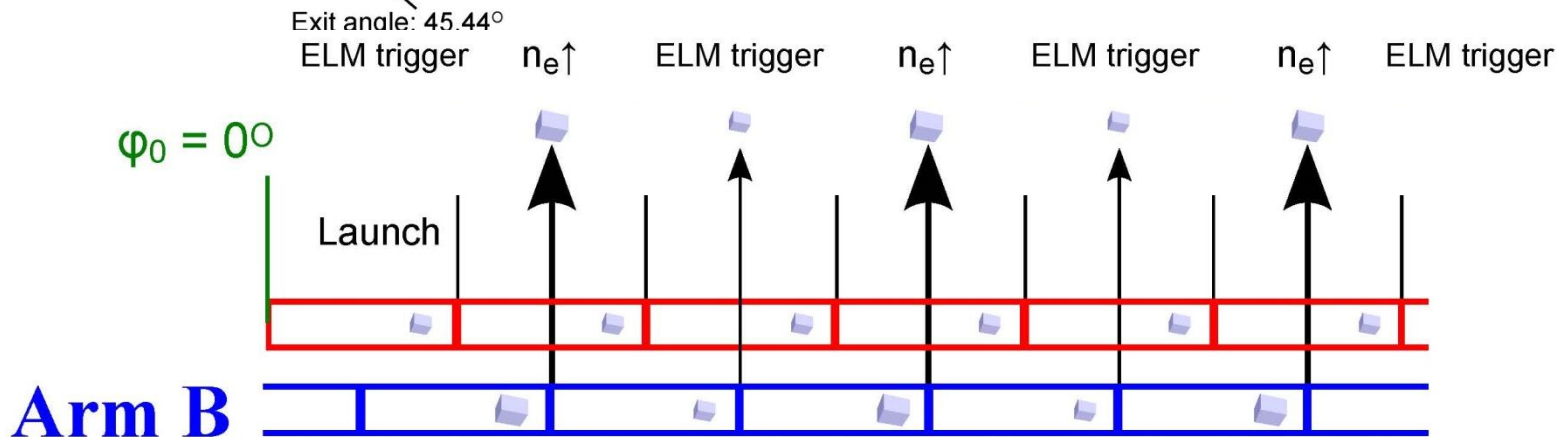
Double accelerator arm approach:

➔ Two “launching slots” per revolution

Design can host up to 3 different extruders  
Initial configuration employing 2 extruders  
➔ Variability during experiment, e.g.



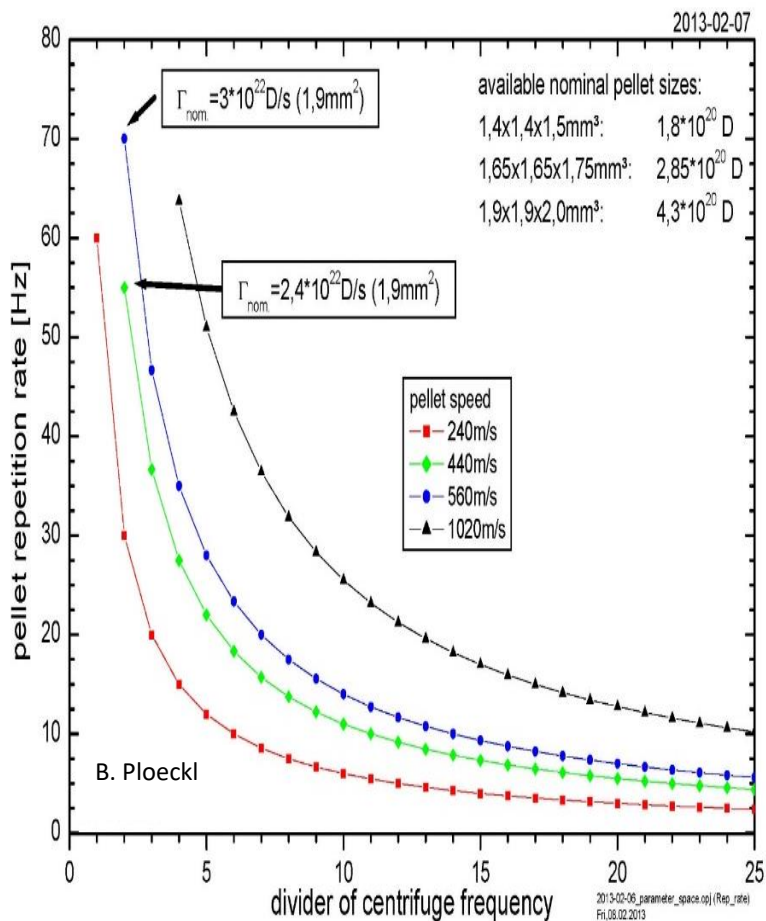
Combined fuelling & pacing



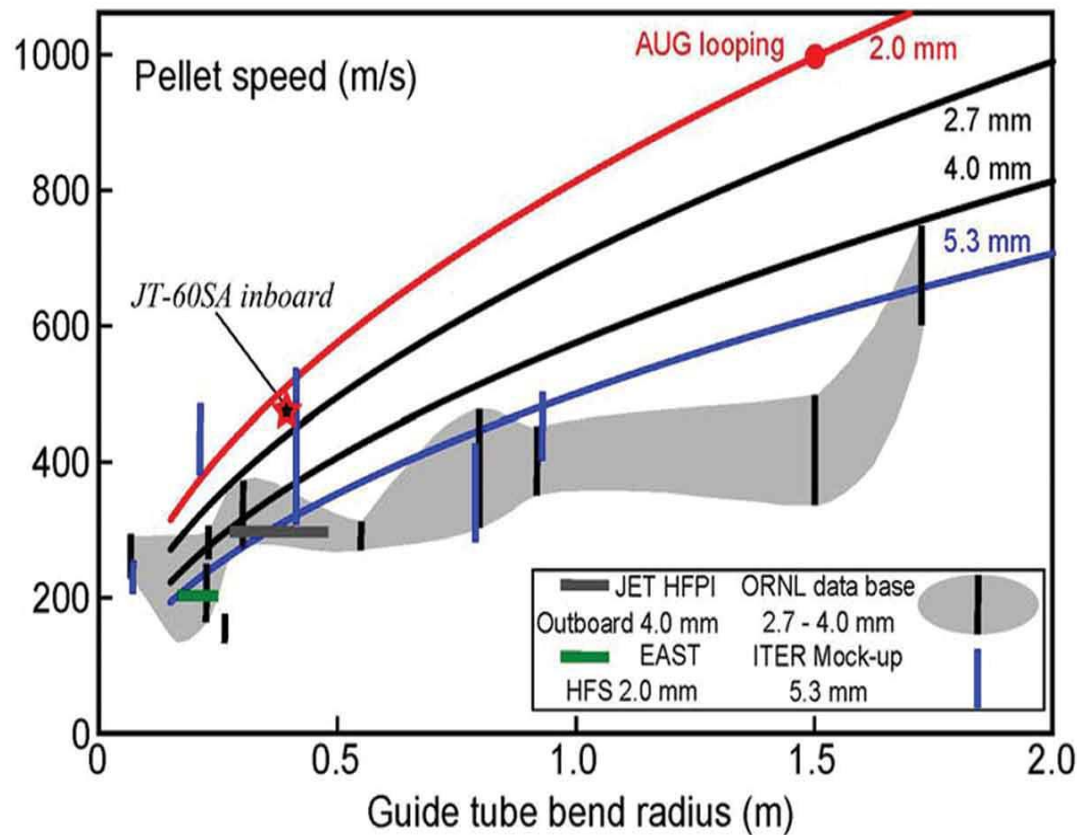
# “DESIGN 100” Proposal



Operational points are correlated to pellet speed (AUG example)



Applicable pellet speed is correlated with guiding tube geometry



# “DESIGN 100” Proposal



Adjust PLS layout to SCSDAS density controller response time of 10 ms:

Assume maximum pellet transfer speed is 500 m/s

Layout of stop cylinder diameter and outer arm length to fulfil

$$v_p \text{ [m/s]} = 5 \times f_c \text{ [Hz]}$$

→ Maximum  $f_p$  (70 Hz) can be provided until  $v_p = 350$  m/s

→ Still  $f_p = 50$  Hz until  $v_p = 250$  m/s

“Granularity” of possible “short term” repetition rates  $f_c/n$  with  $n$  integer

e.g. 100 Hz – 50 Hz – 33.3 Hz – 25 Hz – 20 Hz - 16.6 Hz - 14.3 Hz...

Can be refined for averaged flux with new suggested AUG control approach

50 Hz: ▲x▲x▲x▲    75 Hz: ▲x▲▲x▲    100 Hz: ▲▲▲▲

# “DESIGN 100” Proposal



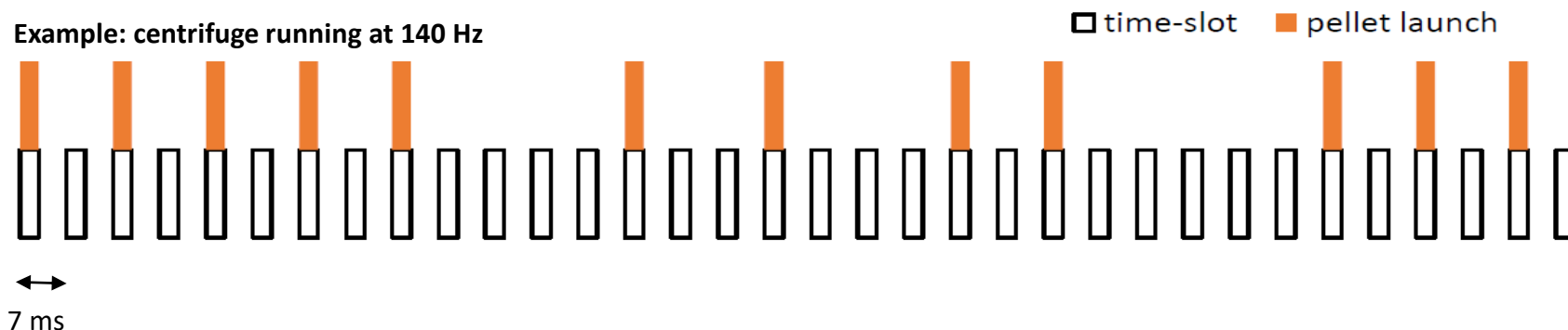
## “Launch slot selection”

Abandon concept of predefined repetition rates

Controller selects next available launching slot

Fastest response, more flexibility

Work is in progress



Concept from IPP suitable for single pellet source only

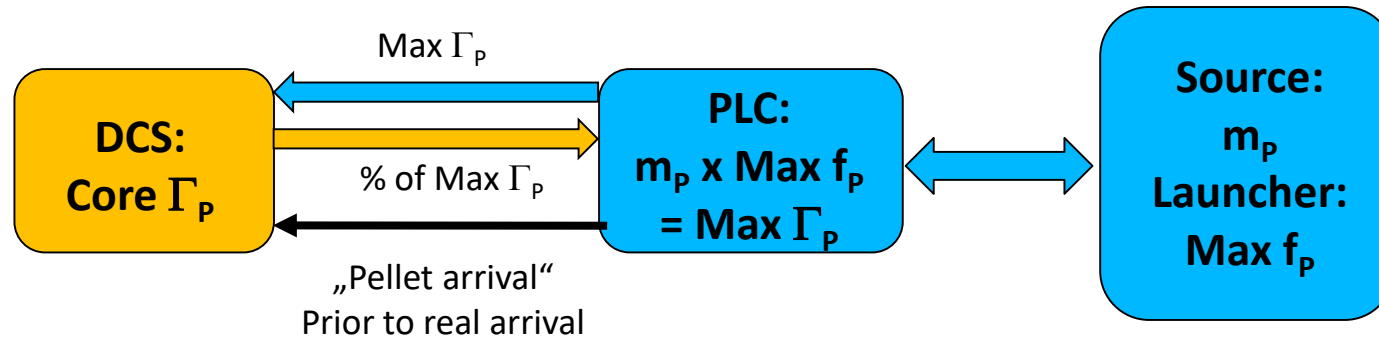
For JT-60SA, upgraded version needed to enable selection from different pellet sources as well

We are going step-by-step!

# “DESIGN 100” Proposal



Revised IPP Discharge Control System (DCS)  
approach for single pellet source:



Suggested approach for fuelling & pacing sources:  
SCSDAS requests independent fuelling flux and pacing rate  
PLC controller takes care for pacing flux balancing  
SCSDAS cares for handling of cases which would require  
Pacing flux > Fuelling flux (PLC could provide “alarm signal”)

# “DESIGN 100” Proposal



How to go on:?

- Discussion at PPM Budapest
- Agree on with QST
- Agree on max pellet speed (and impact on  $v_p$  and  $f_p$  range)
- Fix stop cylinder diameter  $r_0$
- Fix outer acceleration arm length  $R$
- Fix design of centrifuge

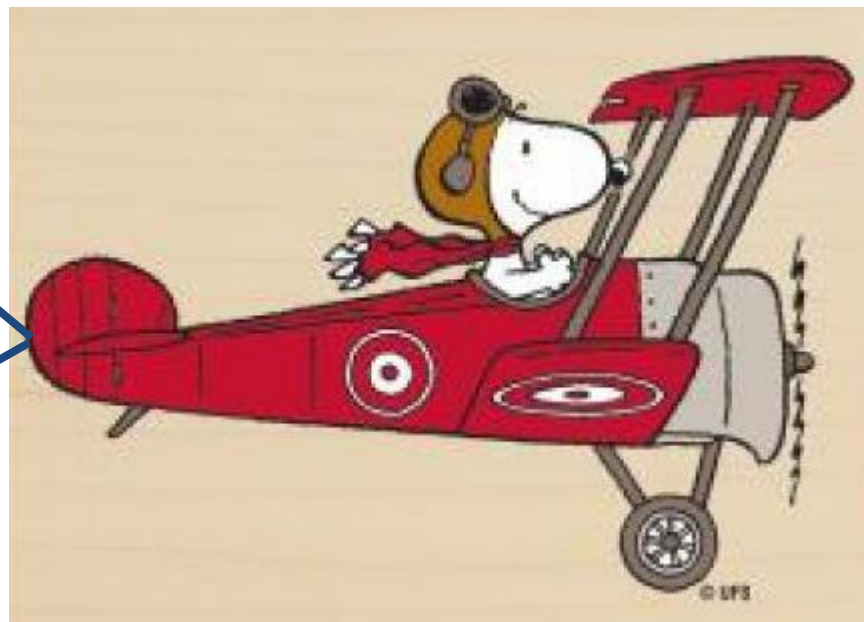
$$R = \frac{1}{\sqrt{2}} \sqrt{\left(\frac{v_P}{2\pi f_C}\right)^2 + r_0^2}$$





# THANK YOU FOR YOUR ATTENTION

Pellets on the move



# “CENTRIFUGE CLOCK”

