



Investigation of edge velocity shear generation with NBI for QH-mode in DEMO

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DEMO QH-mode scenario 2019

- DEMO parameters (scenario 2017): R = 8.94 m a = 2.94 m $B_T = 4.89 T$ Ip = 19.07 MA $n_{avg} \sim 8 * 10^{19} m^{-3}$ k = 1.7triang = 0.33
- $P_{aux} \sim$ to be calculated MW
- $P_{fus} \sim 2 \text{ GW}$
- P_{rad} , core ~ 300 MW
- $P_{sep}/P_{LH} \sim 1.5$

Physics to be investigated

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- QH mode requires a certain velocity shear to be triggered [A. M. Garofalo et al., NF 2011]
- Basically, ExB shear > (value), linked to edge MHD (i.e. Alfvén speed)
- The dimensionless criterion chosen here is (0.16 is arbitrary):

$$- \frac{a}{V_{A}}a\frac{d\Omega}{dr} \approx 0.16;$$

$$V_{A} = \frac{B}{\sqrt{(\mu_{0}nM)}}; \qquad E_{r} = B_{\varphi}(V_{dia} - V_{\theta}) + B_{\theta}V_{\varphi}$$

$$\Omega = \frac{E_{r}}{RB_{\theta}} = \frac{B_{\varphi}}{RB_{\theta}}(V_{dia} - V_{\theta}) + \frac{V_{\varphi}}{R} = \frac{q}{r}(V_{dia} - V_{\theta}) + \frac{V_{\varphi}}{R};$$

- where a is the minor radius, r is the local minor radius

 \bullet Note that $V_{_{dia}}$ is large and negative, i.e. it is much more convenient to inject counter-current toroidal rotation rather than co-current

Value for DEMO



• Applying the criterion for DEMO we get ($w_{ped} = 15$ cm):

$$\frac{a}{V_A} a \frac{d\Omega}{dr} \approx 0.16; \quad \frac{d\Omega}{dr} \approx \frac{\Omega}{w_{ped}}$$
$$\Rightarrow \Omega \approx 2.55 \cdot 10^4 [rad/s] \Rightarrow V_E \approx -19 \, km/s$$

- First estimate of "natural" (i.e. without rotation) edge shear is $V_{_E} \thicksim$ 8 km/s
- Missing ~ -10 km/s of perpendicular rotation, that is ~ 120 km/s of toroidal rotation which have to come from NBI counter-current injection (or ~ + 360 km/s from co-current torque)
- So... how much torque is required to drive \sim -120 km/s of pedestal top rotation?
- Assuming that the angular momentum confinement time in the edge is the same as the energy confinement time, this would mean a torque of:

- So... how much torque is required to drive \sim -100 km/s of pedestal top rotation?
- Assuming that the angular momentum confinement time in the edge is the same as the energy confinement time, this would mean a torque of:

$$S \chi_{\varphi} n R M \frac{V_{\varphi}}{w_{ped}} = T_{\varphi}$$

$$S = 1320 [m^{2}]; \quad \chi_{\varphi} \approx 0.25; \quad n = 4.2$$

$$T_{\varphi} [Nm] \approx 400 [Nm]$$

- very rough calculation, to be done with ASTRA properly.
- Result: confirmed by ASTRA

Results from P. Vincenzi @ 76 MW



lbb

Operational space @ 76 MW

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- very narrow operational space
- expect linearity in power, which would make e.g. 300 keV available @ 140 MW



Discussion

• If a dimensionless parameter for the QH mode entrance is assumed, for DEMO this leads to a certain requirements in edge radial electric field shearing

 \rightarrow as already mentioned by Pietro, needs large torque

• Since DEMO naturally has already a rather large counter-current ExB rotation, to reach the desired value it is better to inject counter-current torque to add the remaining rotation on top of the natural rotation

• This remaining counter-current rotation/torque is estimated and is the ultimate result of the study. The relation by torque and power is provided by the work done by P. Vincenzi

• Regarding pedestal rotation vs torque, the model assumes a pedestal confinement time which is the same in angular momentum as well as in ion energy, and given by the local transport coefficients

 \rightarrow to check against experimental evidence

Conclusions & outlook

- The chosen criterion is just the DIII-D one times a machine size to make it dimensionless \rightarrow absolutely no first principles here
- It could be that the reality is more favourable (more unfavourable means no QH-mode)
- Present results show that with the assumptions used here the required torque is at the limit of the lowest energy, highest tangency radius cases done by Pietro.
- Main things to improve:
 - QH criterion
 - pedestal transport model for toroidal rotation