



TCV-X21 modelling using updated SolEdge-HDG with self-consistent neutrals and mesh adaptivity

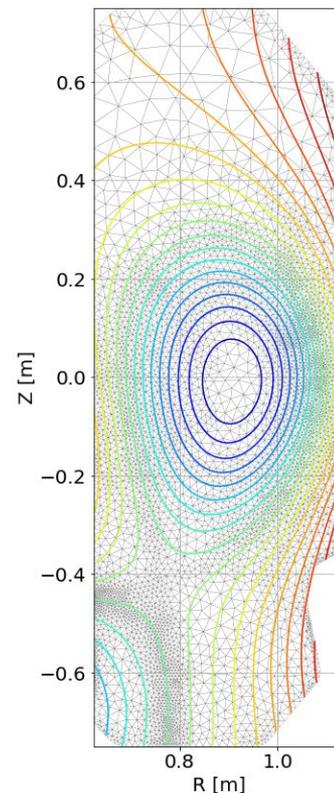
On behalf of SolEdge-HDG team

Regular TSVV3 meeting | 28.05.25



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- Based on finite elements [Giorgiani G., 2018]
Hybridized Discontinuous Galerkin method:
 - Highly parallelizable
 - Straightforward description of complicated boundary geometries
- High-order numerical scheme:
 - Meshes are magnetic equilibrium free
 - X-points and magnetic axis cause no topological issues
- Implicit time scheme: large time steps up to steady-state
- Mesh adaptivity is implemented [Piraccini G., 2022]



TCV-X21 magnetic field lines on computational mesh



- Braginskii fluid closure
- Fluid diffusive neutrals
- Cylindrical geometry with toroidal symmetry
- Single ion deuterium plasma
- Only parallel plasma flow
- Adiabatic electrons with inertia neglected
- No drifts
- No neutrals energy equation

$$\mathbf{B} = B^R \mathbf{e}_R + B^Z \mathbf{e}_Z + B^\phi \mathbf{e}_\phi, \quad \partial_\phi = 0$$

$$n_e = n_i \equiv n$$

$$\mathbf{u} \approx u \mathbf{b}$$

$$enE_{\parallel} = -\nabla_{\parallel}(nk_b T_e)$$
$$m_e/m_i = \mathcal{O}(10^{-3})$$

$$T_i = T_n$$

SolEdge-HDG neutrals model



- Fully diffusive model

$$\partial_t n_n - \underbrace{\nabla \cdot (D_{n_n} \nabla n_n)}_{\text{neutral diffusion}} = S_{n_n}$$

- Neutral-neutral collisions included as in Kotov's PhD

$$D_{n_n} = \frac{eT_i[\text{eV}]}{m_i (n \langle \sigma v \rangle_{cx} + \langle \sigma v \rangle_{iz}) + n_n \langle \sigma v \rangle_{nn}} \quad \langle \sigma v \rangle_{nn} = s_0 T^{0.25}$$

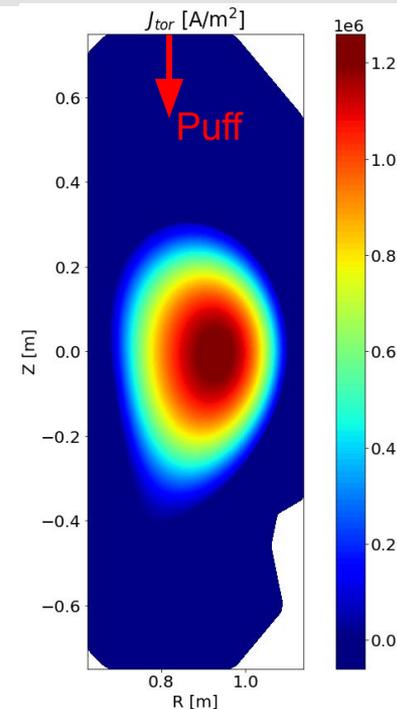
- Recycling at the wall + puff rate in particles/sec + pump with imposed pumping speed [m^3/s]

$$-D_{n_n} \nabla n_n \cdot \mathbf{n} = -R(-D \nabla_{\perp} n + nu\mathbf{b}) \cdot \mathbf{n} - \Gamma_{\text{puff}} \cdot \mathbf{n} + \Gamma_{\text{pump}} \cdot \mathbf{n}$$

TCV-X21 simulation setup



- Steady state
- Equilibrium from TCV-X21 github page
- I_p calculated based on poloidal flux
- $D=\mu=0.2 \text{ m}^2/\text{s}$, $\chi_e=\chi_i=1 \text{ m}^2/\text{s}$ (as in SOLPS-ITER)
- Ohmic heating, Z_{eff} adjusted to have $P_{\text{in}} \approx 130 \text{ kW}$
- $R=0.9$
- Puff adjusted to have flux on the wall around 3×10^{21} particles/s Plasma current density



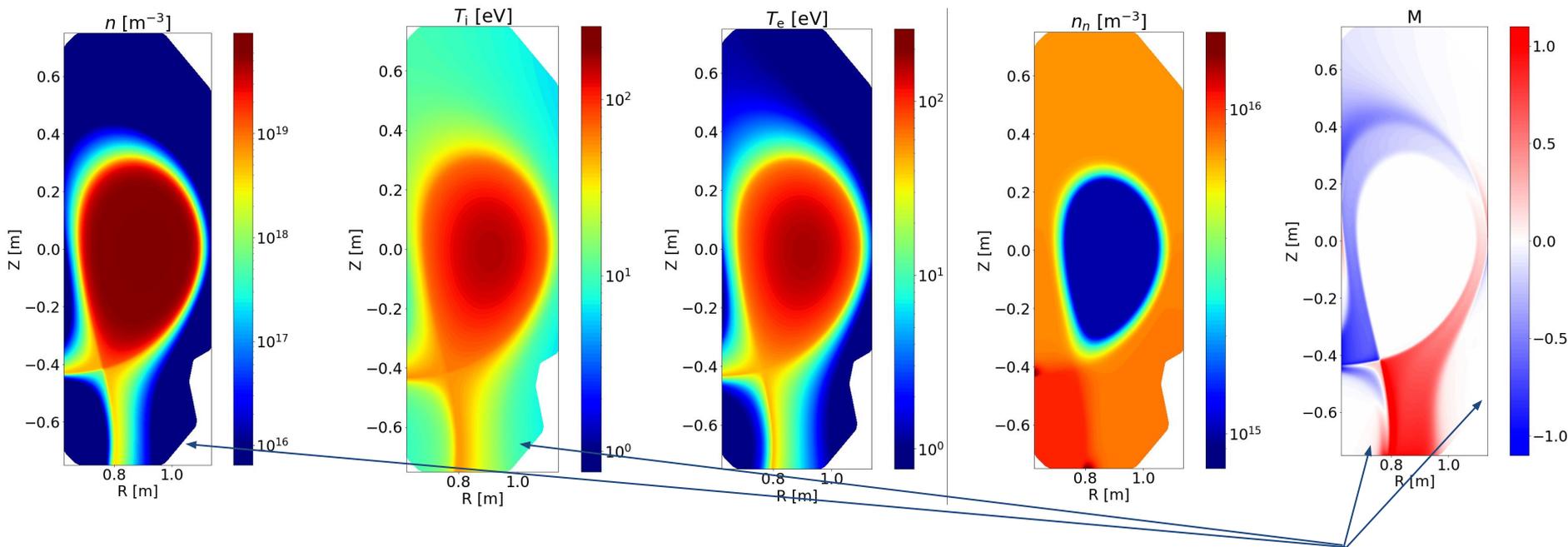


- Due to assumption $T_i = T_n$ the ionization term in ion energy equation “heats” plasma too much

$$n_n n \langle \sigma v \rangle_{iz} R_E \left[\frac{3}{2} k_b T_i \right]$$

- I had to reduce Z_{eff} to 0.3 (non-physical, of course) and even then $P_{tot,vol} = 140$ kW, with $P_{iz} = 60$ kW
- First analysis will be made with this setup
- Next step will be to remove this energy term

2D poloidal plots of solution



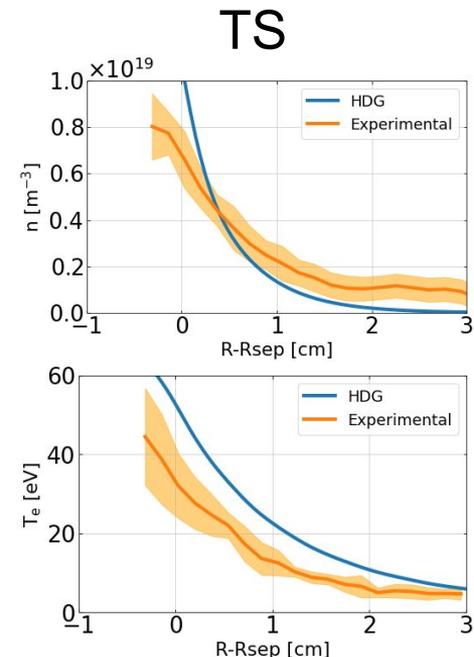
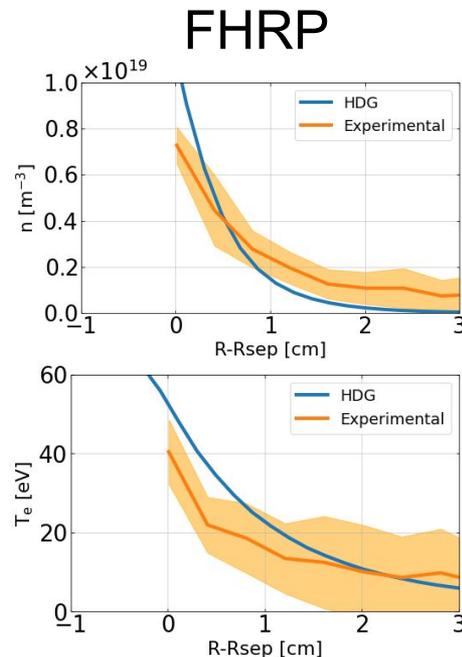
Bohm BC is suppressed, where plasma energy content is low for stability

$$c_s \rightarrow c_s \cdot \frac{1}{1 + \frac{(nE)_{th}}{nE_i}}$$

Midplane profiles



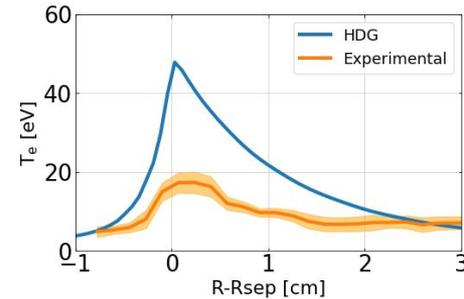
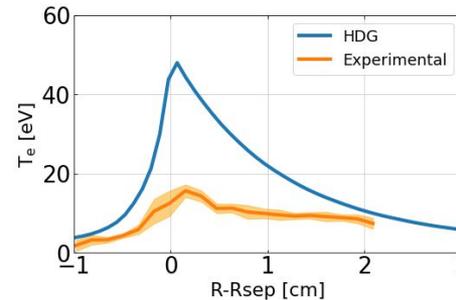
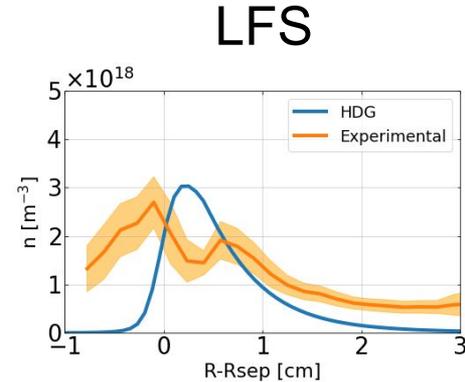
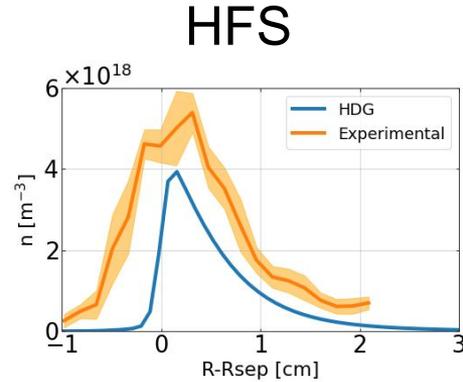
- Both T and n profiles in the simulation decay faster
- Higher density at the core also leads to higher Ohmic heating
- It seems that transport coefficient from SOLPS are too small for SolEdge-HDG. Why?



Divertor profiles



- Density profiles match better
- T is overestimated. Impurity radiation losses missing?
- Both profiles decay faster than experimental ones.
Should I use my own diffusivities and not SOLPS ones?



Removing ionization source of energy

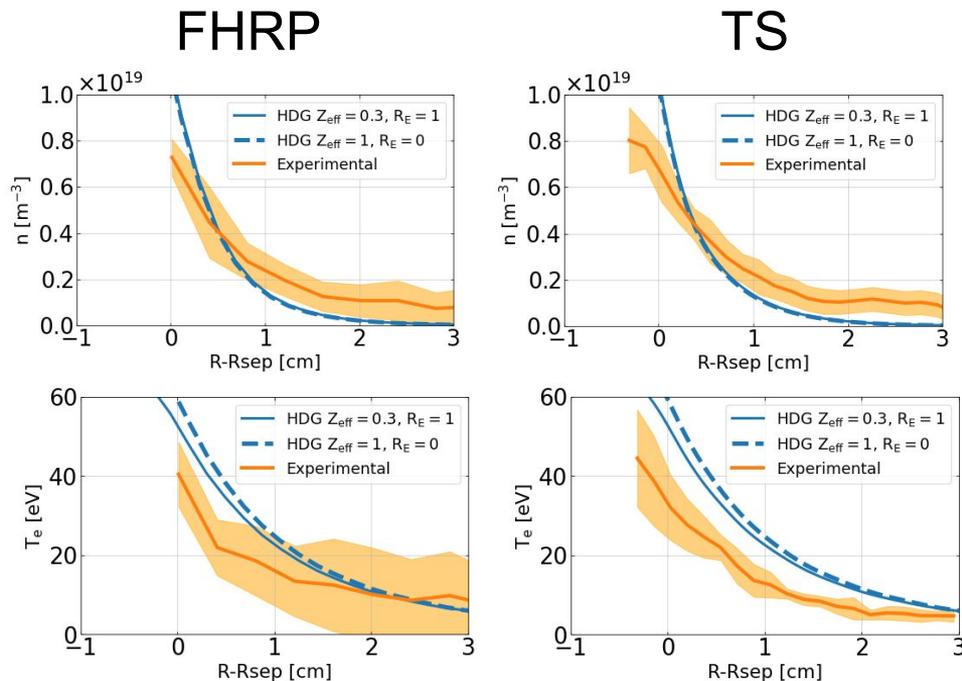


- Assuming that at first ionization energy of neutrals is negligible, we assume $R_E=0$
 $n_n n \langle \sigma v \rangle_{iz} R_E \left[\frac{3}{2} k_b T_i \right]$
- $D=\mu=0.2 \text{ m}^2/\text{s}$, $\chi_e=\chi_i=1 \text{ m}^2/\text{s}$ (as in SOLPS-ITER)
- $Z_{\text{eff}} = 1$ (deuterium plasma); $P_{\text{Ohm}} = 180 \text{ kW}$
- With the same perpendicular transport coefficients total Ohmic power is larger than in other TCV-X21 simulations (too large transport?)

Midplane profiles



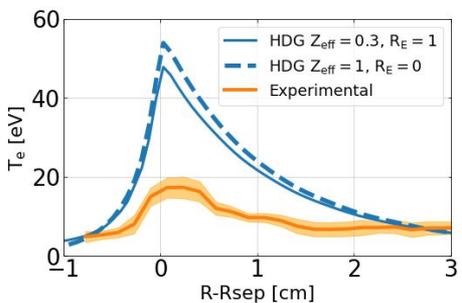
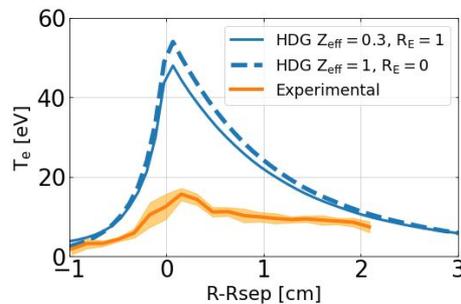
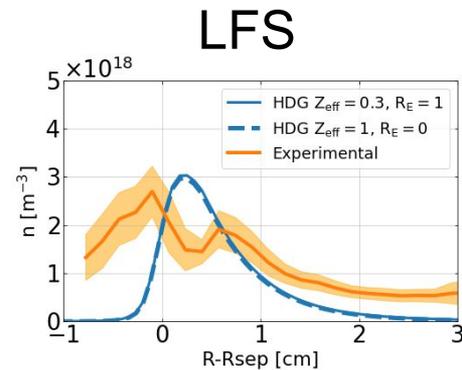
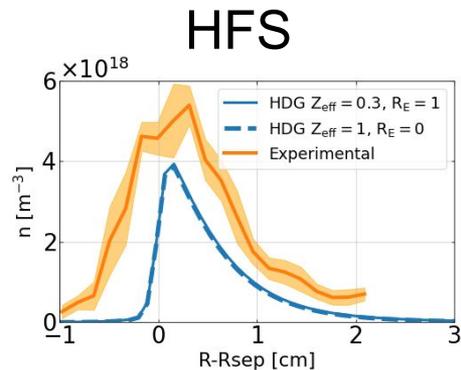
- Almost no difference in density
- Temperature is higher due to higher input power (180 kW vs 140 kW)
- To match experimental profiles one have to reduce perpendicular transport



Divertor profiles



- Similar trend as at midplane
- Temperature is even higher

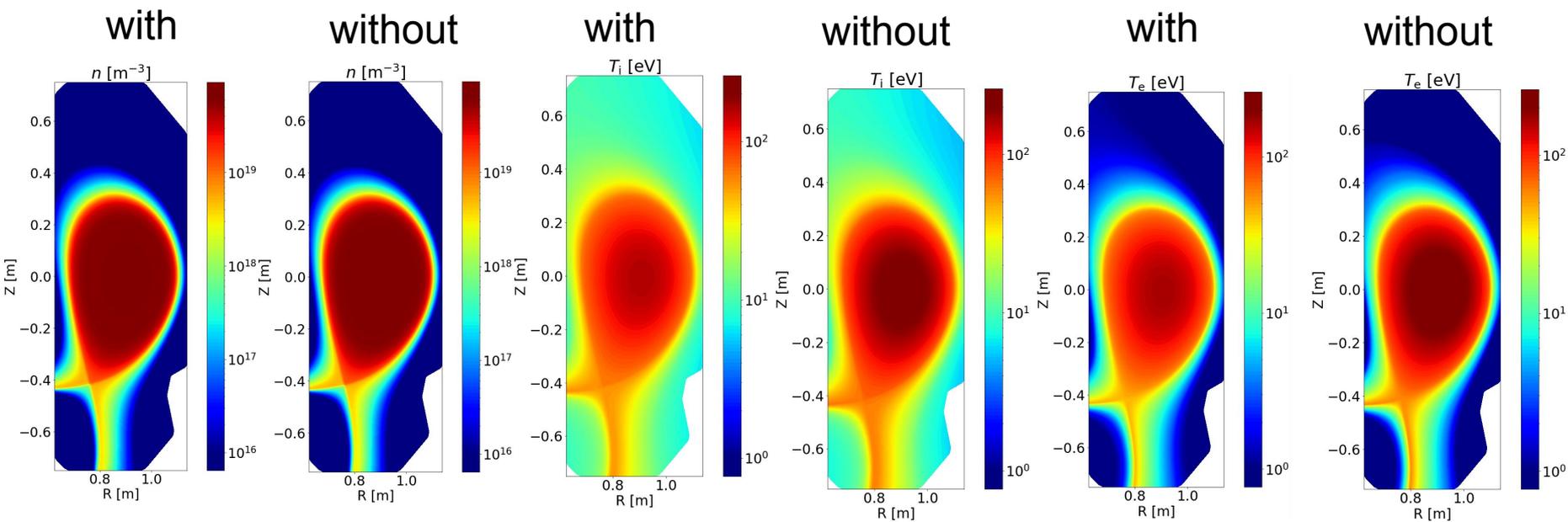


Conclusions

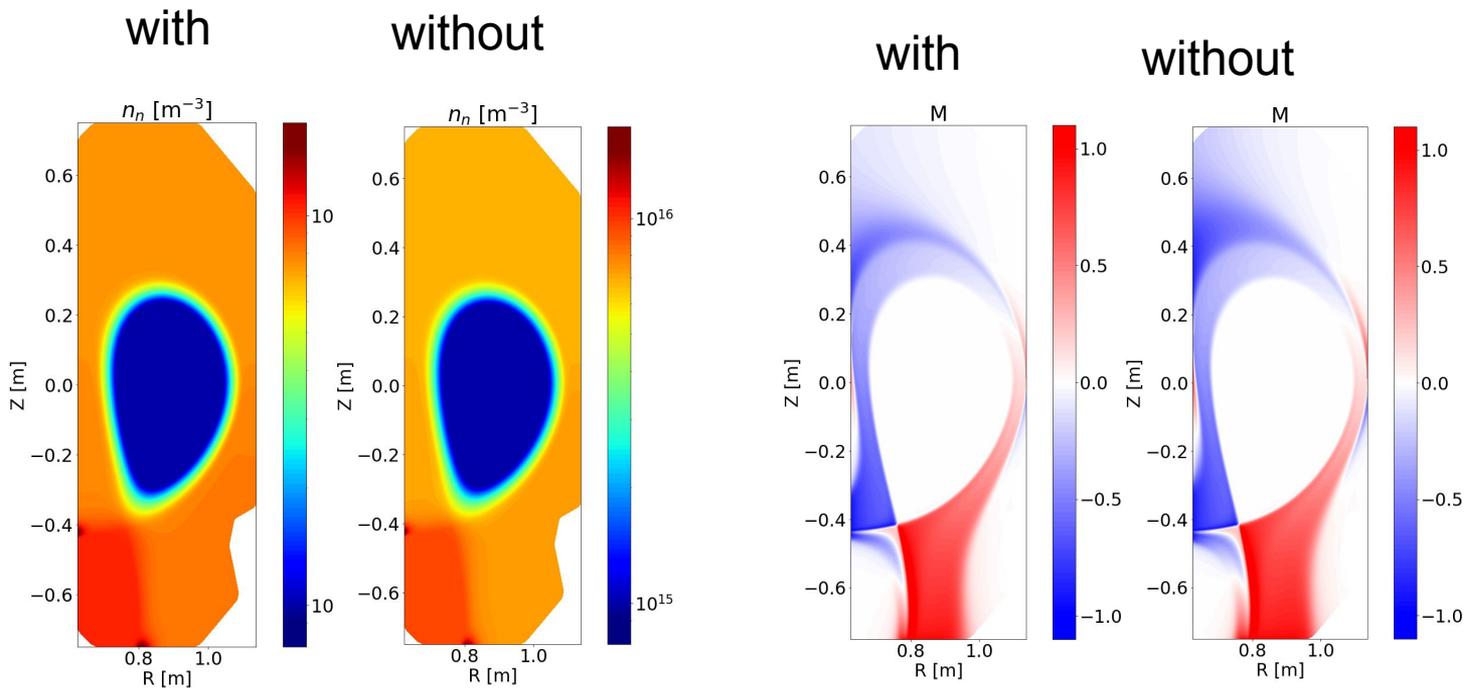


- TCV-X21 modelling pipeline is developed and tested for SolEdge-HDG
- Mesh adaptivity nicely catches separatrix and divertor legs
- In the absence of neutral energy equation one should be careful with neutral-ion energy coupling
- SOLPS-ITER set of transport coefficients result in too large gradients of n and T
- Density is generally in better match than temperature
- Change of power input from “fake” neutral one to Ohmic source leads to almost no change in profiles

With/without energy source from neutrals



With/without energy source from neutrals



SolEdge-HDG system of equations



- Continuity equation

$$\partial_t n + \underbrace{\nabla \cdot (n \mathbf{u})}_{\parallel \text{ advection}} - \overbrace{\nabla \cdot (D \nabla_{\perp} n)}^{\perp \text{ anomalous diffusion}} = S_n$$

- Momentum conservation

$$\partial_t (m_i n u) + \underbrace{\nabla \cdot (m_i n u^2 \mathbf{b})}_{\parallel \text{ advection}} + \underbrace{\nabla_{\parallel} (k_b n (T_e + T_i))}_{\text{pressure stress}} - \overbrace{\nabla \cdot (m_i (n \mu \nabla_{\perp} u + u D \nabla_{\perp} n))}^{\perp \text{ anomalous diffusion}} = S_{\Gamma}$$

- Neutral continuity equation

$$\partial_t n_n - \underbrace{\nabla \cdot (D_{n_n} \nabla n_n)}_{\text{neutral diffusion}} = S_{n_n}$$



- Electron energy conservation

$$\begin{aligned}
 & \partial_t \left(\frac{3}{2} k_b n T_e \right) + \underbrace{\nabla \cdot \left(\frac{5}{2} k_b n T_e \mathbf{u} \mathbf{b} \right)}_{\parallel \text{ advection}} - \overbrace{\nabla_{\parallel} (n k_b T_e)}^{\parallel \text{ electric field}} - \underbrace{\nabla \cdot \left(\frac{3}{2} k_b (T_e D \nabla_{\perp} n + n \chi_e \nabla_{\perp} T_e) \right)}_{\perp \text{ anomalous diffusion}} \\
 & - \underbrace{\nabla \cdot (k_{\parallel e} T_e^{\frac{5}{2}} \nabla_{\parallel} T_e \mathbf{b})}_{\parallel \text{ heat conductivity}} - \overbrace{\frac{3}{2} \frac{k_b n}{\tau_{ie}} (T_e - T_i)}^{\text{temperature-exchange}} = S_{E_e}
 \end{aligned}$$

- Ion energy conservation

$$\begin{aligned}
 & \partial_t \left(\frac{3}{2} k_b n T_i + \frac{1}{2} m_i n u^2 \right) + \underbrace{\nabla \cdot \left(\left(\frac{5}{2} k_b n T_i + \frac{1}{2} m_i n u^2 \right) \mathbf{u} \mathbf{b} \right)}_{\parallel \text{ advection}} + \overbrace{\nabla_{\parallel} (n k_b T_e)}^{\parallel \text{ electric field}} \\
 & - \underbrace{\nabla \cdot \left(\frac{3}{2} k_b (T_i D \nabla_{\perp} n + n \chi_i \nabla_{\perp} T_i) \right)}_{\perp \text{ anomalous diffusion}} - \nabla \cdot \left(\frac{1}{2} m_i u^2 D \nabla_{\perp} n + \frac{1}{2} m_i \mu n \nabla_{\perp} u^2 \right) \\
 & - \underbrace{\nabla \cdot (k_{\parallel i} T_i^{\frac{5}{2}} \nabla_{\parallel} T_i \mathbf{b})}_{\parallel \text{ heat conductivity}} + \overbrace{\frac{3}{2} \frac{k_b n}{\tau_{ie}} (T_e - T_i)}^{\text{temperature-exchange}} = S_{E_i}
 \end{aligned}$$