




# Core-edge transport modeling of a full WEST discharge with SOLEEDGE-HDG

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# Context

- **Aim:** turbulent transport modeling and prediction of the entire discharges to investigate heat and particle exhaust
- Most transport simulations are focused on steady state, edge or core plasma:
  - large uncertainties on ramp-up phase with neglecting loads on limiters
  - core and edge plasma are either not coupled or through crude boundary conditions
- **In this work:**
  - two improvements of SolEdge-HDG model are demonstrated
    - revision of transverse turbulent modelling (starting from Baschetti, et al. 2021)
    - modification of the sources: advanced fluid neutrals and additional heating
  - Two physical points addressed:
    - Evolution of heat and particle fluxes at the PFC during the ramp-up
    - Distribution of heat and energy between ions and electrons with respect to different heating regimes

# Outline

- SolEdge-HDG model
- A k-model to go towards a self-consistent transport model
- An advanced fluid neutral model with non-constant diffusion
- Results:
  - Time evolution of heat and particle fluxes at the wall during ramp-up WEST discharge
  - Repartition between ion and electron channels with additional heating
- Preliminary investigation on growth rate modification

# SolEdge-HDG

- Fluid transport code based on Hybridized Discontinuous Galerkin method (Giorgiani, et al. 2018)
- Magnetic equilibrium free high-order meshes
- Solves Braginskii conservative equations for plasma density, momentum, ion and electron energies for deuterium and electrons
- But! How to define the cross-field transport coefficients?

$$\partial_t n + \nabla \cdot (n\mathbf{u}) - \nabla \cdot (D\nabla_{\perp} n) = S_n$$

*continuity*

$$\partial_t(m_i n u) + \nabla \cdot (m_i n u^2 \mathbf{b}) + \nabla_{\parallel} (k_b n (T_e + T_i)) - \nabla \cdot (\mu \nabla_{\perp} (m_i n u)) = S_{\Gamma}$$

*momentum conservation*

$$\begin{aligned} & \partial_t \left( \frac{3}{2} k_b n T_i + \frac{1}{2} m_i n u^2 \right) + \nabla \cdot \left( \left( \frac{5}{2} k_b n T_i + \frac{1}{2} m_i n u^2 \right) u \mathbf{b} \right) - n u E_{\parallel} \\ & - \nabla \cdot \left( \frac{3}{2} k_b (T_i D \nabla_{\perp} n + n \chi_i \nabla_{\perp} T_i) \right) - \nabla \cdot \left( \frac{1}{2} m_i u^2 D \nabla_{\perp} n + \frac{1}{2} m_i \mu \nabla_{\perp} u^2 \right) \\ & - \nabla \cdot (k_{\parallel i} T_i^{\frac{5}{2}} \nabla_{\parallel} T_i \mathbf{b}) + \frac{3}{2} \frac{k_b n}{\tau_{ie}} (T_e - T_i) = S_{E_i} \end{aligned}$$

*ion energy*

$$\begin{aligned} & \partial_t \left( \frac{3}{2} k_b n T_e \right) + \nabla \cdot \left( \frac{5}{2} k_b n T_e u \mathbf{b} \right) + n u E_{\parallel} - \nabla \cdot \left( \frac{3}{2} k_b (T_e D \nabla_{\perp} n + n \chi_e \nabla_{\perp} T_e) \right) \\ & - \nabla \cdot (k_{\parallel e} T_e^{\frac{5}{2}} \nabla_{\parallel} T_e \mathbf{b}) - \frac{3}{2} \frac{k_b n}{\tau_{ie}} (T_e - T_i) = S_{E_e} \end{aligned}$$

*electron energy*

# SolEdge-HDG fluid turbulent model revision

- Heuristic model of turbulent model transport (Baschetti et al. NF 2021)

*turbulent  
energy  
evolution*

$$\partial_t k + \nabla \cdot (k v_{\parallel} \mathbf{b}) - \nabla \cdot (D_k \nabla_{\perp} k) = \gamma_I k - c_{\varepsilon} k^2$$

1. parallel transport with plasma parallel velocity
2. Perpendicular diffusion with self-consistently defined D:

$$D_k = k \tau_{\parallel} = k \frac{L_{\parallel}}{c_s} = k \frac{2\pi q R}{c_s}$$

3. The same coefficient is used for plasma transport equations

$$D_k = D = \mu = \chi_i = \chi_e$$

# SolEdge-HDG fluid turbulent model revision

- Heuristic model of turbulent model transport (Baschetti et al. NF 2021)

*turbulent  
energy  
evolution*

$$\partial_t k + \nabla \cdot (k v_{\parallel} \mathbf{b}) - \nabla \cdot (D_k \nabla_{\perp} k) = \boxed{\gamma_I k} - \boxed{c_{\varepsilon} k^2}$$

## 1. Growth rate due to interchange instability

$$\gamma_I = \begin{cases} c_s \sqrt{\frac{\nabla p_i \cdot \nabla \mathbf{B}}{p_i \mathbf{B}} - \frac{\theta}{R^2}}, & \frac{\nabla p_i \cdot \nabla \mathbf{B}}{p_i \mathbf{B}} - \frac{\theta}{R^2} \geq 0 \\ 0, & \frac{\nabla p_i \cdot \nabla \mathbf{B}}{p_i \mathbf{B}} - \frac{\theta}{R^2} < 0 \end{cases}$$

## 2. Sink rate closure by assumption of energy balance in SOL

$$\frac{\chi_e p_e}{\lambda_q^2} = \frac{2\gamma_e p_e c_s}{L_{\parallel}} \quad \text{and} \quad \chi_e = D_k = k \frac{L_{\parallel}}{c_s} \quad \text{and} \quad k = \gamma_I / c_{\varepsilon} \quad \Rightarrow \quad c_{\varepsilon} = \frac{L_{\parallel}^2}{2\gamma_e \lambda_q^2 c_s^2} \gamma_I \quad \text{Scaling}$$

$$\lambda_q = 4q\rho L$$

# SolEdge-HDG neutral model

- First introduced for SolEdge-HDG in (d'Abusco, et al. 2022)

*continuity  
neutrals*

$$\partial_t n_n - \nabla \cdot (D_{n_n} \nabla_{\perp} n_n) = -n_n n \langle \sigma v \rangle_{iz} + n^2 \langle \sigma v \rangle_{rec}$$

- recently modified with **self-consistent neutral diffusion coefficient** (accepted to Front. Phys.)

*depends on mean free  
path of neutrals*

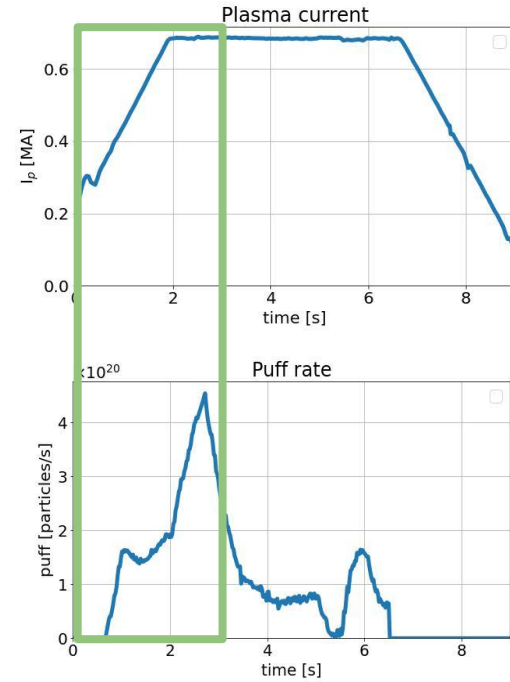
$$D_{n_n} = \frac{eT_i[\text{eV}]}{m_i n (\langle \sigma v \rangle_{cx} + \langle \sigma v \rangle_{iz})}$$

- Neutral moment and boundary conditions should be modified

$$-D_{n_n} \nabla n_n \cdot \mathbf{n} = -R(-D_n \nabla_{\perp} n \cdot \mathbf{n} + n u \mathbf{b} \cdot \mathbf{n}) - \Gamma_{puff} \cdot \mathbf{n}$$

# Simulation set-up

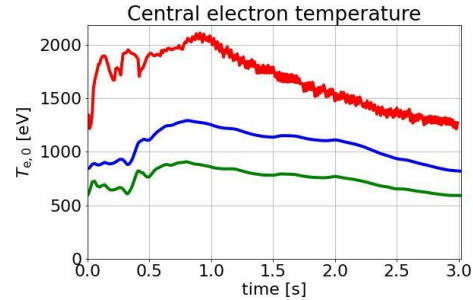
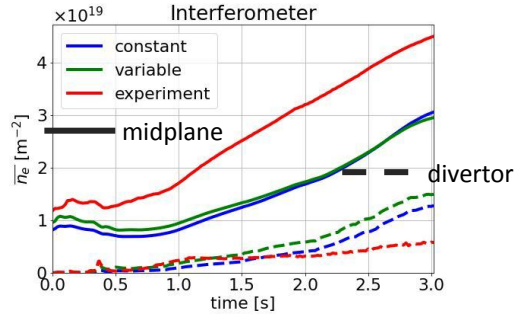
- WEST Ohmic discharge #54487
- *Current, magnetic field and puff rate from WEST IMAS*
- Recycling R = 0.998
- Two transport models:
  - constant  $D = \mu = \chi_i = \chi_e = 0.5 \text{ m}^2/\text{s}$
  - variable  $D = \mu = \chi_i = \chi_e = D_k = k \frac{L_{\parallel}}{c_s}$   
*for numerical stability*  $D_{\min} = 0.3 \text{ m}^2/\text{s}$   $D_{\max} = 20 \text{ m}^2/\text{s}$   $D_{n_0} = 1000 \text{ m}^2/\text{s}$
- Focusing ramp-up (up to  $t = 3\text{s}$ )





# Evolution of core plasma parameters

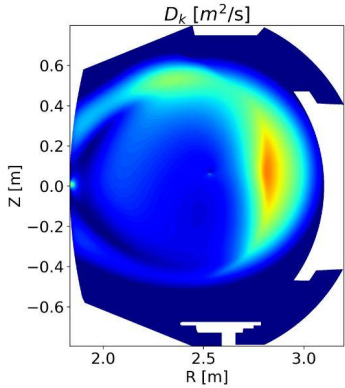
Evolution of poloidal profiles of plasma parameters for simulation with variable diffusion



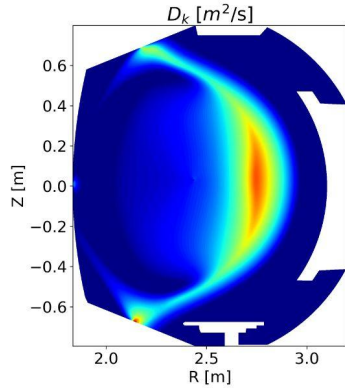
- Turbulent model causes higher perpendicular transport:
  - wider density profile
  - lower energy content
- Trends are similar, but absolute values are not:
  - should be higher recycling (probably varying)
  - More heating  $\Rightarrow$  take into account higher  $Z_{eff}$

# Predicted diffusion

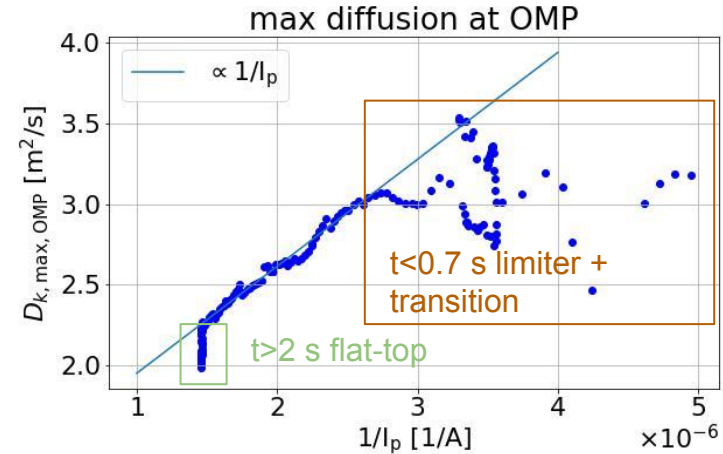
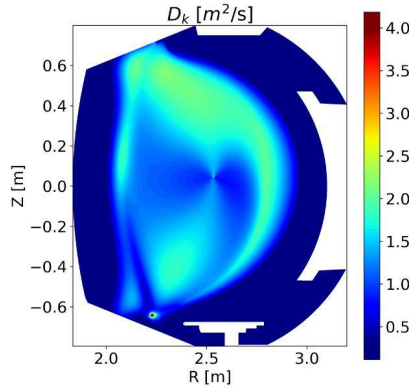
Limiter phase



Limiter-divertor transition

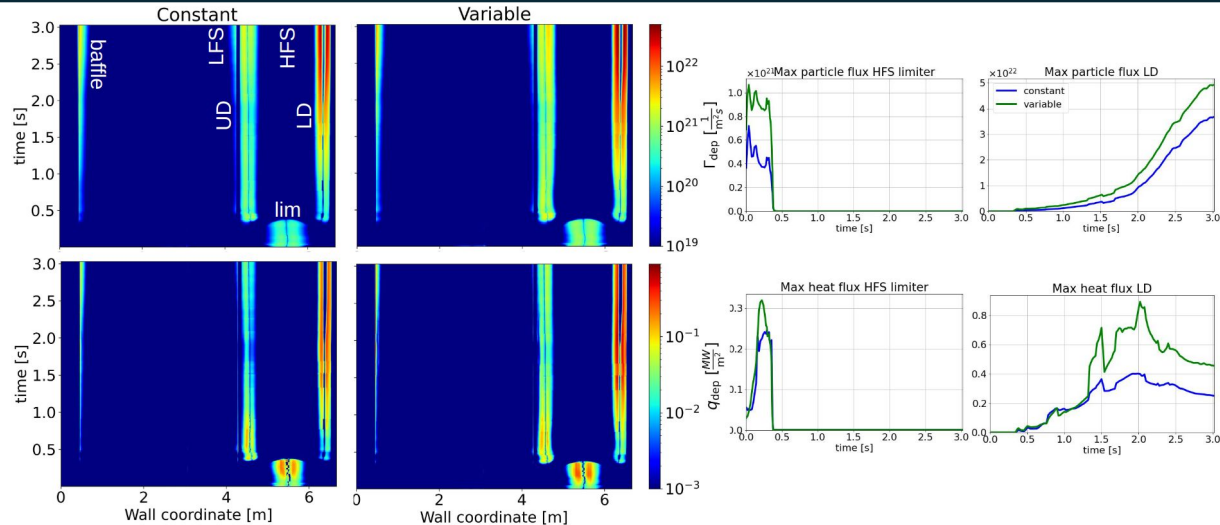


flat-top



- The model predicts higher transport at LFS and at regions with high connection length at plasma edge
- Non-local turbulent transport effects
- During ramp-up of current the maximum value of diffusion decreases as  $1/I_p$ , which corresponds to global confinement scaling

# Evolution of simulated fluxes onto the wall



- Increased turbulent transport causes higher and wider profiles particle fluxes
- However, during first 1.3 s peak heat values in both simulations are comparable
- Significant fluxes predicted on baffle and upper divertor (especially during limiter-divertor transition)

# Steady state additional heating simulation

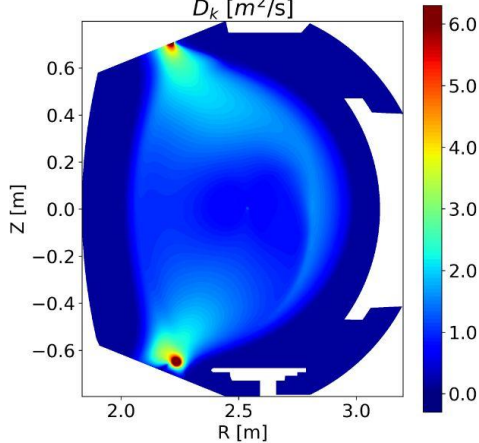
- Gaussian circle source of 2 MW applied to ions or electrons
- Centered at the magnetic axis of plasma with width of 15 cm
- Equilibrium at t=4.5 s of discussed discharge, steady-state
- Recycling R = 0.998
- Transport model:

- plasma  $D = \mu = \chi_i = \chi_e = D_k = k \frac{L_{\parallel}}{c_s}$
- neutrals  $D_{n_n} = \frac{eT_i[\text{eV}]}{m_i n (\langle \sigma v \rangle_{cx} + \langle \sigma v \rangle_{iz})}$

# Turbulent diffusion for different heating

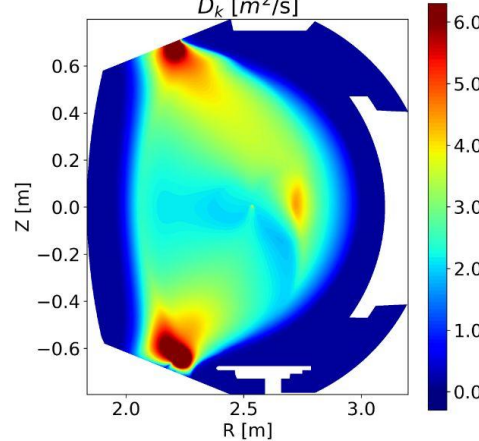
Ohmic

$D_k$  [ $m^2/s$ ]



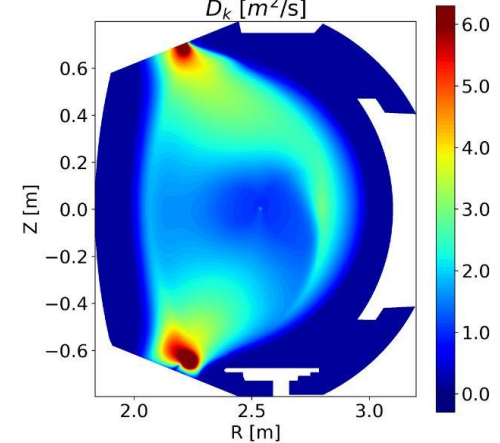
Ohmic +2 MW ions

$D_k$  [ $m^2/s$ ]



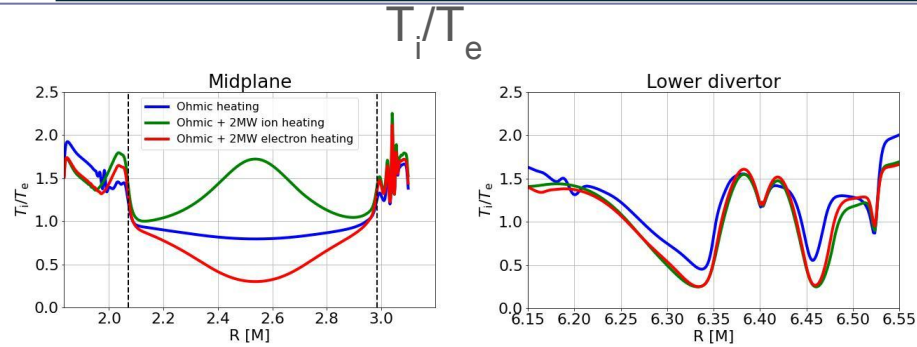
Ohmic +2 MW elects

$D_k$  [ $m^2/s$ ]

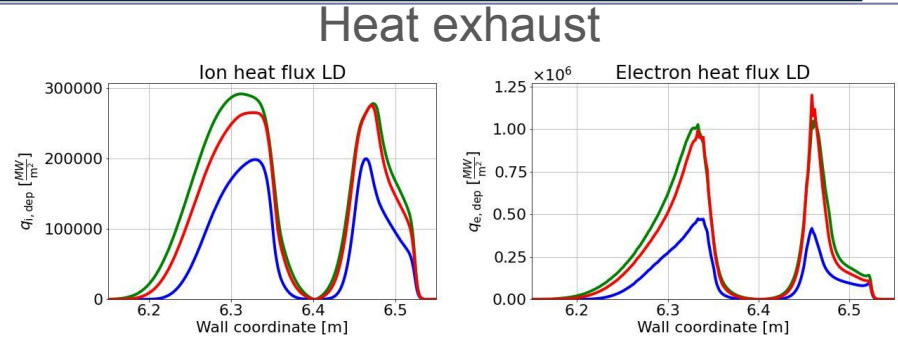


- Additional heating causes significantly higher transport at both divertors
- Since the growth rate is proportional to ion pressure gradient, ion heating leads to more transport increase

# Ion/electron heat channel distribution



- In far SOL heating generally leads to  $T_i/T_e$  reduction
- In core the change  $T_i/T_e$  corresponds to the heating channel



- Additional heating goes preferentially through electron channel
- Slightly lower heat fluxes for the electron heating are due to lower plasma resistivity and hence lower Ohmic heating

# Conclusions

- On the way of physical model enrichment in SolEdge-HDG:
  - turbulent self-consistent transport model has been revised
  - neutral model now employs self-consistent diffusion coefficient
  - additional heating sources has been implemented
- Simulation of ramp-up of WEST discharge:
  - Turbulent diffusivity scales as  $1/I_p$  and mostly localized at separatrix (LFS), and X-points
  - Heat and particle fluxes are increased compared to constant diffusion simulation
- Additional heating sources simulation
  - Significantly increased turbulent transport near lower and upper divertor
  - Reduction of  $T_i/T_e$  in far SOL
  - Additional heating escapes plasma mostly through electron channel

# Perspectives: drift-wave instability and parallel losses

- We start from set of 2 equations:

*continuity equation*

$$\partial_t n_e + \nabla \cdot (n_e (\mathbf{v}_E + \mathbf{v}_{*,e})) + \nabla \cdot (-D_{\perp} \nabla_{\perp} n_e) = S_n - \nabla_{\parallel} \Gamma_{\parallel,e}$$

*divergence of total current*

$$\nabla \cdot (\mathbf{J}_{pol} + \sum_{\text{species } \alpha} (q_{\alpha} n_{\alpha} \mathbf{v}_E + q_{\alpha} n_{\alpha} \mathbf{v}_{*,\alpha})) = -\nabla_{\parallel} \mathbf{J}_{\parallel}$$

*parallel losses*

*electric drift*

$$\mathbf{J}_{pol} = \frac{\mathbf{B}}{B^2} \times m_i \frac{d}{dt} (n_i (\mathbf{v}_E + \mathbf{v}_{*,i}))$$

*diamagnetic drift*

*polarization current*

- Leaving 1st order terms in 1st equation and up to 2nd order in the 2nd  
Linearizing, low  $\beta$  limit, Boussinesq approximation for density, cold ion limit:

$$\partial_t n + D_B \mathbf{b} \cdot (\nabla \phi \times \nabla \bar{n}) - D_{\perp} \nabla_{\perp}^2 n = S_n - \sigma_{n,n} n + n_0 \sigma_{n,\phi} \phi$$

*vorticity*

$$\partial_t W - \nu_{\perp} \nabla_{\perp}^2 W - 2D_B \mathbf{b} \cdot \left( \frac{\nabla B}{B} \times \frac{\nabla n}{n_B} \right) = -\sigma_{\phi,n} \frac{n}{n_B} + \sigma_{\phi,\phi} \phi$$

$W = \rho_s^2 \nabla_{\perp}^2 (eU/T_e)$



# Perspectives: linearization of loss terms

- We want to linearize parallel losses in a simple form:

$$-\nabla_{\parallel} \Gamma_{e\parallel,e} = -\sigma_{n,n} n + n_0 \sigma_{n,\phi} \phi$$

$$\frac{1}{en_B} \nabla_{\parallel} \mathbf{J}_{\parallel} = -\sigma_{\phi,n} \frac{n}{n_B} + \sigma_{\phi,\phi} \phi$$

Confined region?

yes

no

Electron collisions

yes

Collision length much smaller than connection length?

$$\frac{L_{coll}}{L_{\parallel}} \ll \sqrt{m_e/m_i}$$

no

Sheath limited regime

$$\sigma_{n,n} = \sigma_{\phi,n} = \sigma_{n,\phi} = \sigma_{\phi,\phi} = C_{\parallel} = \frac{T_e k_{\parallel}^2}{\nu_e m_e}$$

$$\sigma_{n,n} = \sigma_{n,\phi} = \sigma_{\phi,\phi} = C_{\parallel} = \frac{c_s}{L_{\parallel}}$$

$$\sigma_{\phi,n} = 0$$

# Perspectives: adding more physics to turbulent model

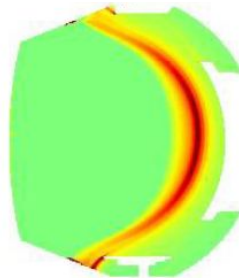
- Current growth rate does not include interchange instability damping

$$\gamma_I = \begin{cases} c_s \sqrt{\frac{\nabla p_i \cdot \nabla \mathbf{B}}{p_i \mathbf{B}} - \frac{\theta}{R^2}}, & \frac{\nabla p_i \cdot \nabla \mathbf{B}}{p_i \mathbf{B}} - \frac{\theta}{R^2} \geq 0 \\ 0, & \frac{\nabla p_i \cdot \nabla \mathbf{B}}{p_i \mathbf{B}} - \frac{\theta}{R^2} < 0 \end{cases}$$

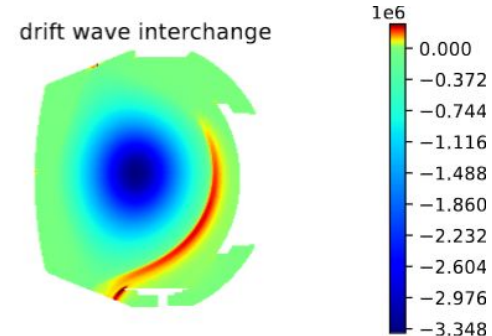
$$\gamma = \frac{-A + \sqrt{\frac{g_r + |g|}{2}}}{\tau}$$

Preliminary estimation on fixed plasma background

old model



new model



# Perspectives: stability analysis

- Making fourier transformation and solving dispersion equation:

$$\gamma = \frac{-A + \sqrt{\frac{g_r + |g|}{2}}}{\tau}$$

$$A = \frac{a_n + a_\phi}{2}$$

$$g_r = A^2 - a_n a_\phi \frac{b_{nr} b_{\phi r} - b_{ni} b_{\phi i}}{C_{\parallel} / \Omega_i}$$

$$g_i = -\frac{b_{nr} b_{\phi i} + b_{ni} b_{\phi r}}{C_{\parallel} / \Omega_i}$$

$$\frac{1}{\tau} = \sqrt{C_{\parallel} \Omega_i}$$

polarization  
current

$$a_n = \frac{D_{\perp}}{D_B d_{\perp}} + (C_{\parallel} / \Omega_i)^{1/2}$$

$$a_{\phi} = \frac{\nu_{\perp}}{D_B d_{\perp}} + d_{\perp}$$

$$b_n = \frac{\rho_{\star}}{\sqrt{2} d_{\perp}^{1/2}} \left( \hat{e}_R \cdot \frac{a \nabla \bar{n}}{n_B} - \hat{e}_z \cdot \frac{a \nabla \bar{n}}{n_B} \right) + i (C_{\parallel} / \Omega_i)^{3/4}$$

$$b_{\phi} = -\sqrt{2} d_{\perp}^{1/2} \rho_{\star} \left( \hat{e}_R \cdot \frac{a \nabla B}{B} \right) + i \frac{C_{\parallel, \star}}{C_{\parallel}} d_{\perp} (C_{\parallel} / \Omega_i)^{3/4}$$

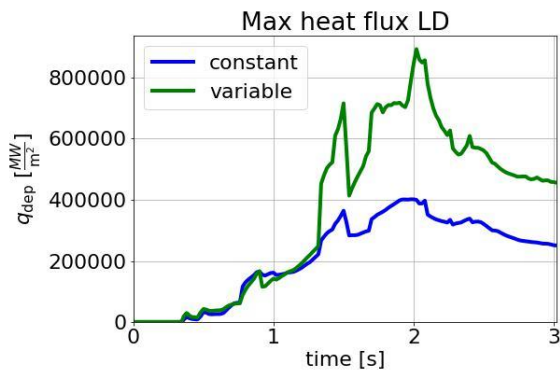
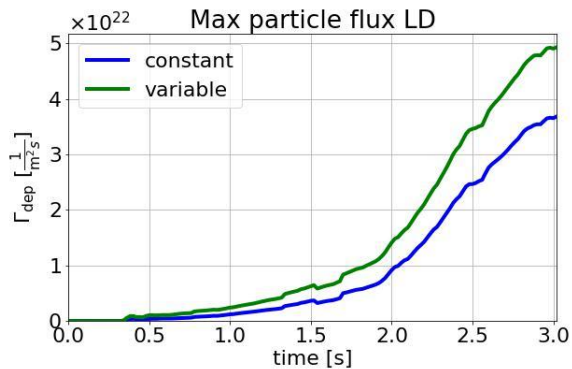
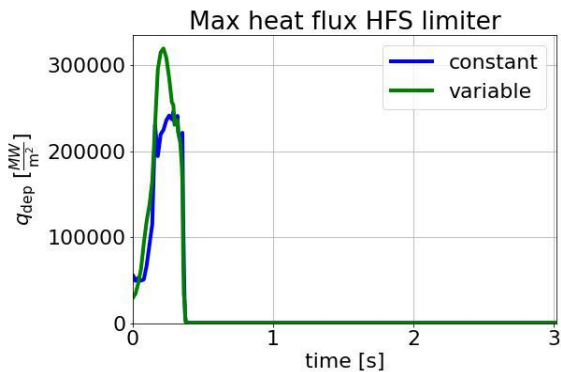
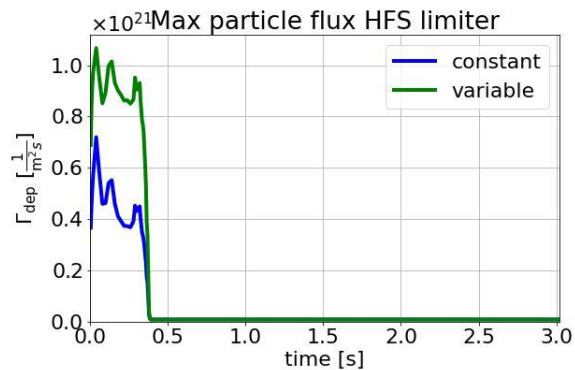
parallel losses

electric drift

diamagnetic  
drift

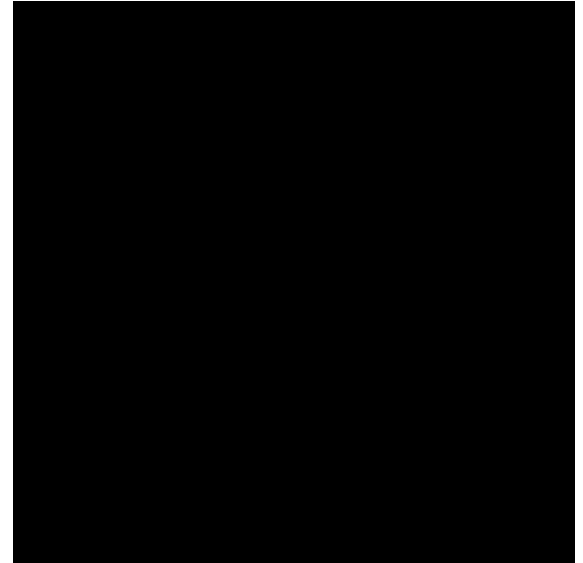
- Parallel losses act generally as a damping term
- Drifts are driving the instability
- Though interplay between different terms should be studied in details

# Max fluxes for varying equilibrium



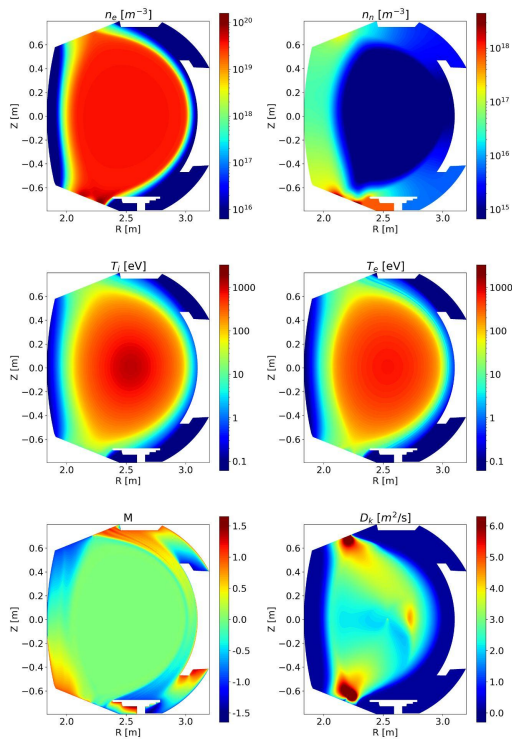
# SolEdge-HDG

- Fluid transport code based on Hybridized Discontinuous Galerkin method (Giorgiani, et al. 2018)
- Magnetic equilibrium free, high-order meshes

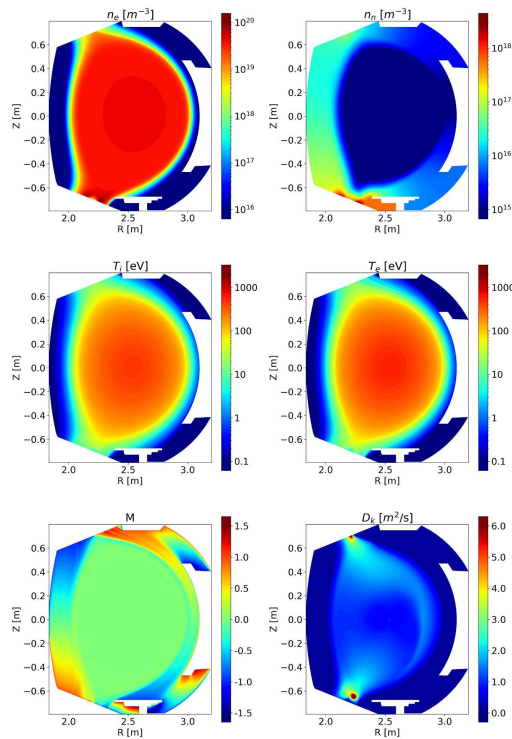


# Overview poloidal profiles

## Ohmic +2 MW ions



## Ohmic



## Ohmic +2 MW elects

