





The Dynamics of Wall Elements (DWE) code: a recycling model for SolEdge-EIRENE

> TSVV5 meeting June 06, 2025



Ofusion

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Recycling in SolEdge-EIRENE



MATERIAL

HI

Recycling handled in **EIRENE**:

 $RECYCT = R_n + (1 - R_n)R_m$

- **Reflection**: $R_n = \frac{\Gamma_{ref}}{\Gamma_{inc}}$ calculated self-consistently with tabulated **TRIM** tables
- **Desorption**: $R_m = \frac{\Gamma_{out}}{\Gamma_{imp}^{i+} + \Gamma_{imp}^{at}}$ set **ad-hoc** by the user often = 1 \rightarrow force particle conservation or < 1 \rightarrow wall pumping

Recycling in SolEdge-EIRENE



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- **Reflection**: $R_n = \frac{\Gamma_{ref}}{\Gamma_{inc}}$ calculated self-consistently with tabulated **TRIM** tables

Desorption: $R_m(t) = \frac{\Gamma_{out}(t)}{\Gamma_{imp}^{i+}(t) + \Gamma_{imp}^{at}(t)}$ set ad hoc by the user $\Gamma_{imp}^{i+}(t) + \Gamma_{imp}^{at}(t)$ often = 1 \rightarrow force particle conservation $- \text{or} < 1 \rightarrow \text{wall pumping}$

Outline

- 1) The Dynamics of Wall Elements (DWE) code
- 2) Wall initialisation with the DWE code (before coupled plasma-wall simulation)
- 3) Reduced model for hydrogen retention as a tool for DWE simulation analysis
- 4) Conclusions

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The Dynamics of Wall Elements (DWE) code



J. Denis et al., Nuclear Materials and Energy Fusion, 19 (2019) J. Denis et al., PhD thesis (2020)

The Dynamics of Wall Elements (DWE) code



Wall temperature heat equation

J. Denis et al., Nuclear Materials and Energy Fusion, 19 (2019) J. Denis et al., PhD thesis (2020)

WE-temp: Wall Element temperature

- Temperature profile in thin layer of surface material (< 1 mm)
- Handle different PFC technologies (inertial, actively-cooled) and design (materials)
- Handle steady-state and transient heat loads
- \rightarrow 1D linear heat equation solved using superposition theorem

$$\phi_{net}(t) = \sum_{k=1}^{N_{\phi}(t)} \Delta \phi_k \mathcal{H}(t - t_k)$$

$$\Delta T_1(x, t) = \overline{T_1}(x, t) - T(0) = \sum_{k=1}^{N_{\phi}(t)} \Delta \phi_k T_1^{step}(x, t - t_k)$$



PFC step response

 \Rightarrow calculated using quadrupole method

+ numerical or analytical inverse Laplace transform

J. Denis et al., PhD thesis (2020)

The Dynamics of Wall Elements (DWE) code



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$$\frac{\partial n_m(x,t)}{\partial t} = \frac{\partial}{\partial x} \left(D(T) \cdot \frac{\partial n_m}{\partial x} \right) - \sum_{i=1}^{N_{trap}} \frac{\partial n_{t,i}}{\partial t} + S_{ext}^{i+}(x,t) + S_{ext}^{at}(x,t)$$
$$\frac{\partial n_{t,i}(x,t)}{\partial t} = v_{t,i}^*(T) \cdot \frac{n_i(x) - n_{t,i}}{n_{IS}} n_m - v_{dt,i}(T) \cdot n_{t,i}$$
B. C. at $x = 0$: $n_m(0,t) = 0$
B. C. at $x = L$:
$$\begin{vmatrix} n_m(L,t) = 0 \\ or \\ D(T) \cdot \frac{\partial n_m(L,t)}{\partial x} = 0 \end{vmatrix}$$

Particles divided in 2 populations :

- Mobile particles (diffusion): $n_{\rm m}(x, t)$
- Trapped particles: $n_{t,i}(x, t)$

$$\frac{\partial n_m(x,t)}{\partial t} = \frac{\partial}{\partial x} \left(D(T) \cdot \frac{\partial n_m}{\partial x} \right) - \sum_{i=1}^{N_{trap}} \frac{\partial n_{t,i}}{\partial t} + S_{ext}^{i+}(x,t) + S_{ext}^{at}(x,t) + S_{ex$$

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$$\frac{\partial n_{t,i}(x,t)}{\partial t} = v_{t,i}^*(T) \cdot \frac{n_i(x) - n_{t,i}}{n_{IS}} n_m - v_{dt,i}(T) \cdot n_{t,i}$$

$$B. C. at x = 0: n_m(0,t) = 0$$

$$B. C. at x = L: \begin{vmatrix} n_m(L,t) = 0 \\ 0 \\ D(T) \cdot \frac{\partial n_m(L,t)}{\partial x} = 0 \end{vmatrix}$$

$$[HI]_m + Trap_{free} \leftrightarrow [HI]_t$$

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Particles divided in 2 populations :

- Mobile particles (diffusion): $n_{\rm m}(x, t)$
- Trapped particles: $n_{t,i}(x, t)$

$$\Gamma_{out} = D(T) \cdot \frac{\partial n_m}{\partial x} (x = 0)$$

surface processes not rate-limiting

$$R_m(t) = \frac{\Gamma_{out}(t)}{\Gamma_{imp}^{i+}(t) + \Gamma_{imp}^{at}(t)}$$

 $R_m(t \to \infty) \to 1$



But the direct coupling with SolEdge3X-EIRENE is not operational



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Indirect coupling of SolEdge-EIRENE and DWE for wall initialisation



Indirect coupling of SolEdge-EIRENE and DWE for wall initialisation



Plasma backgrounds



DWE outputs



DWE outputs



Simulation of similar discharges in full-W JET



Dynamic retention during discharges: retention rate



Dynamic retention during discharges: retention rate



The retention rate is reproducible from the 3rd discharge → the wall is initialised

> J. Denis et al., Nuclear Materials and Energy Fusion, 19 (2019) J. Denis et al., PhD thesis (2020)

Retention rate in the simulation is consistent with experimental observations



Recycling coefficient at t = 2 s



Recycling coefficient at t = 2 s?

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Recycling coefficient at t = 2 s



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Reduced model for hydrogen retention

Hypothesis:

- (1) Fixed implantation conditions : flux $\Gamma_{imp,j}$, energy $E_{imp,j}$
- (2) Two point sources : $j = H^+$, H
- (3) Wall temperature constant : T
- (4) Steady-state
- → Hydrogen inventory dominated by traps
- → Density of trapped H in subsurface layer (µm) at steady-state: $n_{t,i}(x) = f_{\text{stat},i} n_i(x)$

Trap filling ratio:

$$\boldsymbol{f}_{\text{stat},i}(T, \Gamma_{\text{imp},j}, E_{\text{imp},j}) = \frac{1}{1 + \frac{\nu_{\text{dt},i}(T)}{\nu_{\text{t},\text{stat}}(\Gamma_{\text{imp},j}, E_{\text{imp},j})}}$$

- when $v_{dt,i} \gg v_{t,stat}$, $f_{stat,i} \rightarrow 0$ (empty traps)

- when
$$v_{\mathrm{dt},i} = v_{\mathrm{t,stat}}$$
, $f_{\mathrm{stat},i} = 0.5$

- when $v_{dt,i} \ll v_{t,stat}$, $f_{stat,i} \rightarrow 1$ (saturated traps)



J. Denis et al., Journal of Nuclear Materials 570 (2022)









Retention dynamics in low-energy traps during transition H-mode \rightarrow L-mode



Reduced model as a tool to explain inventory variation during discharges



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Reduced model as a tool to explain inventory variation during discharges



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