



# Edge modelling of C-Wall JT-60SA with SOLEDGE2D-EIRENE

Luca Balbinot, Paolo Innocente (Consorzio RFX-Italy)



UNIVERSITÀ  
DEGLI STUDI  
DI PADOVA



This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014-2018 and 2019-2020 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.



- Introduction to the modelling activity
- Description of the recent modelling activity on scenario 2
- Future perspectives



## Previous activities:

- H. Kawashima et al. “*Evaluation of heat and particle controllability on the JT-60SA divertor*” J. Nucl. Mater. **415** (2011)
- R. Zagorski et al. “*Numerical analyses of baseline JT-60SA design concepts with the COREDIV code*” Nucl. Fus. **57** (2017)
- M. Romanelli et al. “*Investigation of sustainable high- scenarios in the JT-60SA C-wall*” Nucl. Fus. **57** (2017)

## Recent Activities:

- 2019: Transport parameter evaluation on JET
- 2019-2020: JT-60SA *Scenario 2* modelling

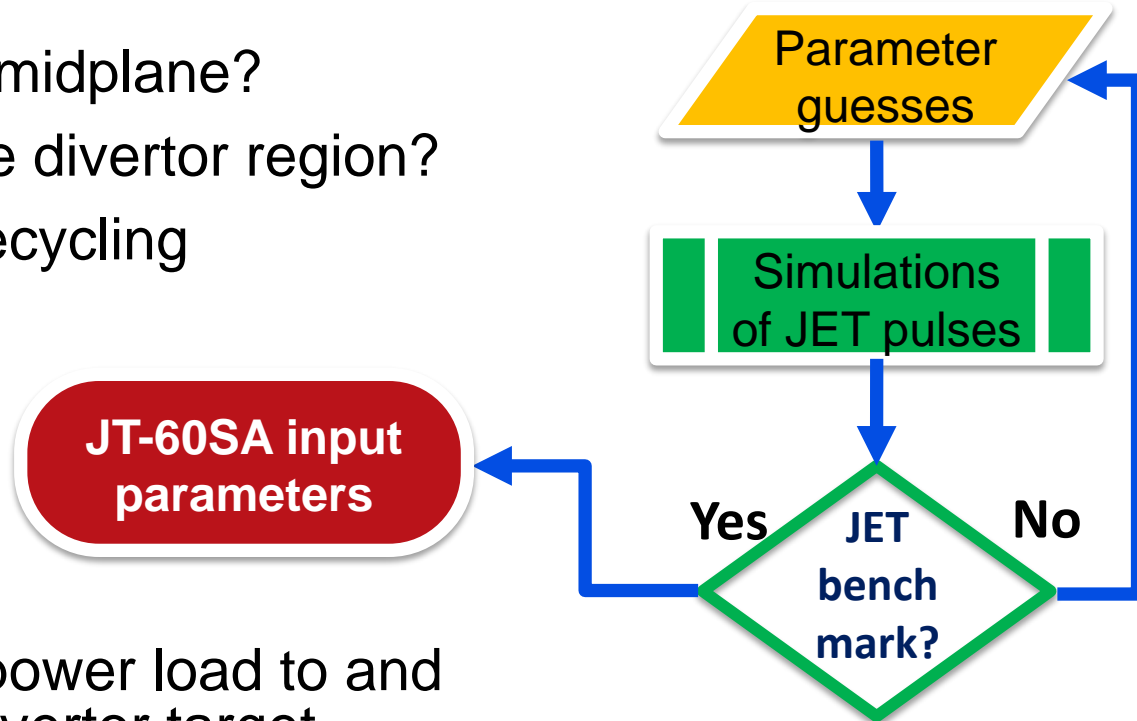
## Foreseen activities:

- Modelling of *Initial research phase scenario* with SOLEDGE2D-EIRENE
- Modelling with SOLEDGE3X

# Modelling activity conceptualization



- **Transport param.** at midplane?
- Transport profile in the divertor region?
- Is **C** production and recycling well estimated?



1. Predict particle and power load to and temperature at the divertor target
2. Which is the minimum radiated power to obtain sustainable power flux to divertor?
3. Which is the impurity level required to radiate such power
4. Do the scenario need to be modified to obtain sustainable power flux

# Modelling activity overview

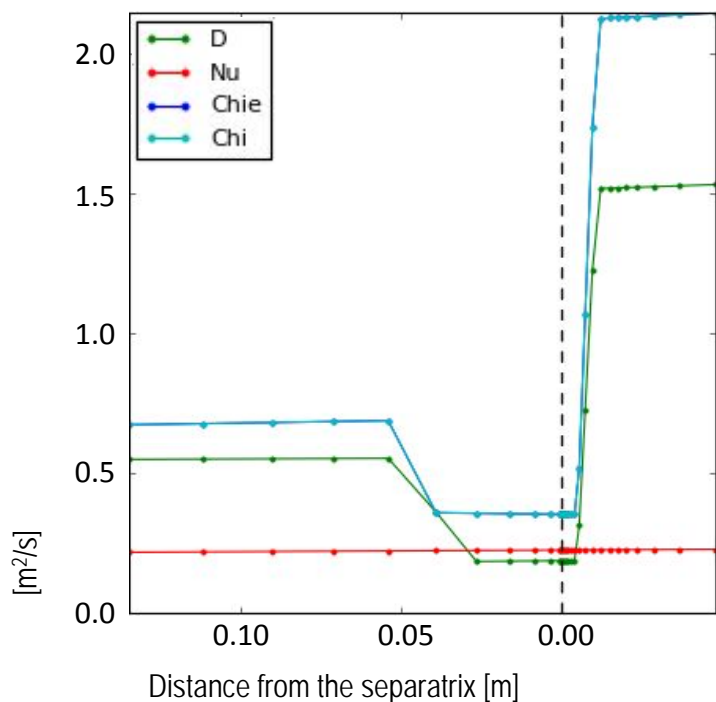


	Initial research phase I	Scenario 2	JET #69890	Diff
Toroidal field $B_T$ [T]	2.25	2.25	2.18	3%
Plasma Current $I_p$ [MA]	5.5	5.5	2.0	64%
Elongation $K_x$		1.87	1.6	14%
$\beta_N$		3.1	2.3	26%
Core dens. $n_c$ [ $10^{19} \text{ m}^{-3}$ ]	4.5/6.3	6	7	17%
Sep. dens. $n_s$ [ $10^{19} \text{ m}^{-3}$ ]	$\sim 1/2$	1/2	3	200/50%
G. dens. Frac		0.5	0.6	20%
Heating Power $P_{in}$ [MW]	26.5	41	21	49%
Magn. Conf.	High elong. SN	High elong. SN	High elong. SN	-
Mode	H	H	H	-
Strike point pos.	2 vertical	2 vertical	1 vert., 1 horiz.	
Wall composition	C	C	C	-
Seeding	No	Ne/Ar	No	
Pumping speed [ $\text{m}^3/\text{s}$ ]	Up to 100	Up to 100	-	

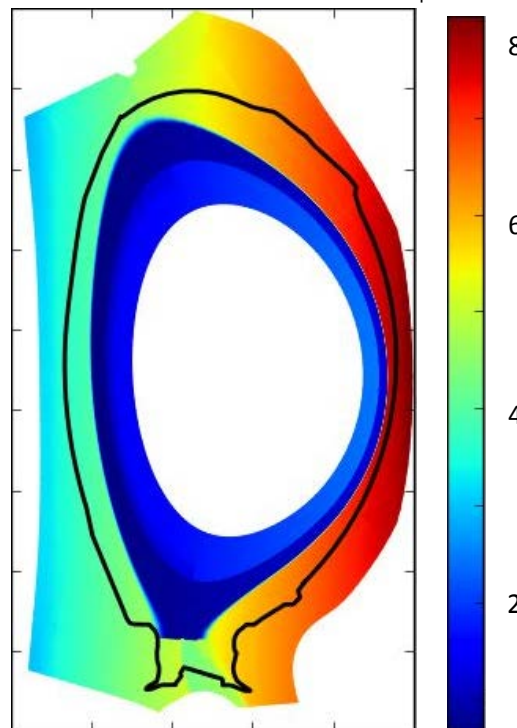
# Chosen input parameters



Transport param. Radial cut



Ratio between  $X_{e,i}$  and  $X_{e,i; sep}$



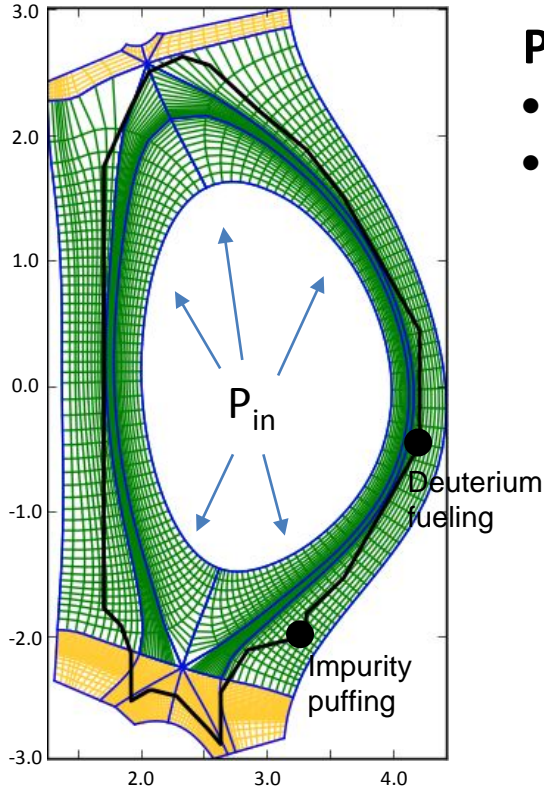
Previous modelling with SONIC was performed using uniform  $D=0.3$   $Chi=1.0m^2/2$  Impurity as a fraction of  $n_D$

Experimental data C-wall JET:

- LIDAR
- Bolometry
- Spectroscopy ( $D\alpha$ , CII, CIII emission lines)
- Langmuir probes

- $D_{sep} = 0.16 m^2/s$
- $X_{e/i, sep} = 0.27 m^2/s$  (Ac. To Eich scaling)
- $D/Chi$  increase in the SOL
- $D/Chi$  increase below X-point
- $1/Bt$  factor
- Using no drifts

L.Balbinot, 3<sup>rd</sup> IAEA Tech. Meet. On Divertor Concept



## Pure deuterium simulations

- Used as setup for impurity introduction
- Maximum input power ( $P_{in,MAX}$ ) to have partial detachment is about **9 MW**.

## Deuterium and Carbon simulations

- C impurity radiate up to **8MW** with standard simulation setup
- $P_{in,MAX}$  **16MW** with  $n_{e,sep} = 2.0 \times 10^{19} m^{-3}$  and power flux to the targets below the maximum allowed
- Significant **asymmetry** inner/outer divertor power load
- Future topic for the *Initial research phase I* modelling

## Ar puffing

$$\Gamma_{Ar} = 1 \times 10^{20} s^{-1}$$

$$Z_{eff,sep} \approx 3.0$$

$$P_{in} = P_{aux} - P_{elm} - P_{rad,core} = 30 MW$$

## Ne puffing

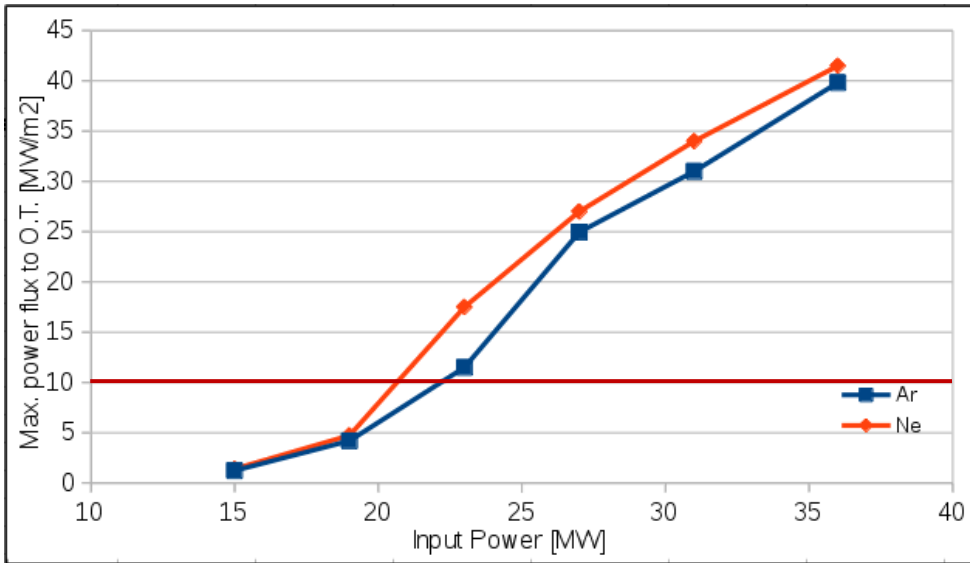
$$\Gamma_{Ne} = 2 \times 10^{20} s^{-1}$$

$$\Gamma_{D2} = 1 \times 10^{22} s^{-1}$$

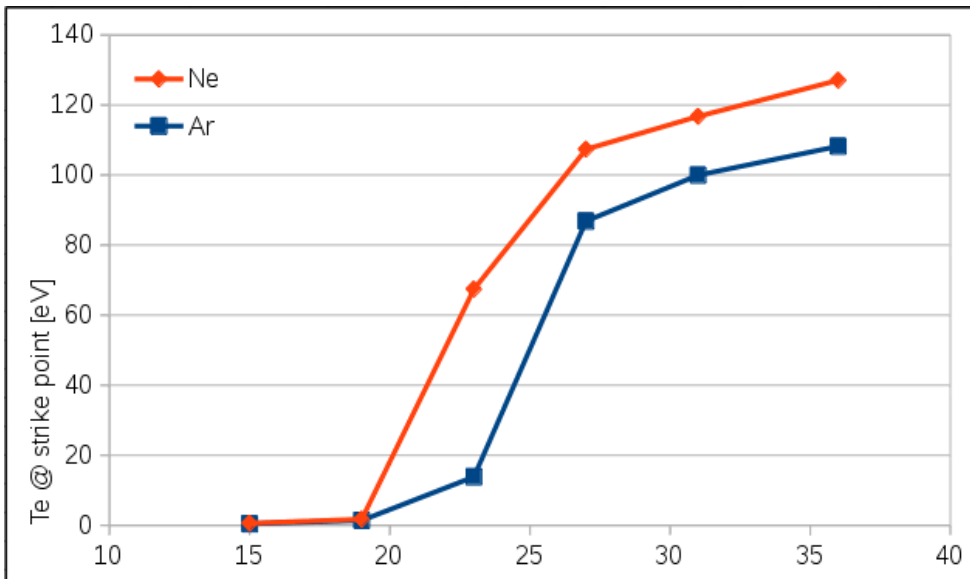
Albedo

$$\text{Minimum density } n_{e,sep} = 2 \times 10^{19} m^{-3}$$

# Neon and Argon cooling performances

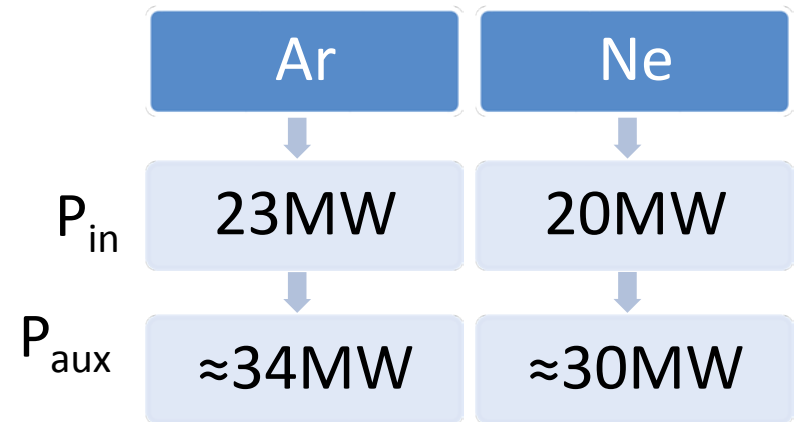


- $N_{e,sep}$ :  $2.2/2.3 \times 10^{19} m^{-3}$
- $n_{D,sep}/n_{e,sep} \approx 0.76$   $Z_{eff,sep} \approx 3.0$
- D puffing fixed as the standard simulation.
- **Ar is more efficient at high  $T_e$ , but no relevant difference when approaching detachment**



## Maximum power in the scenario

$$P_{in} = P_{aux} - P_{rad,core} - P_{i-elms}$$

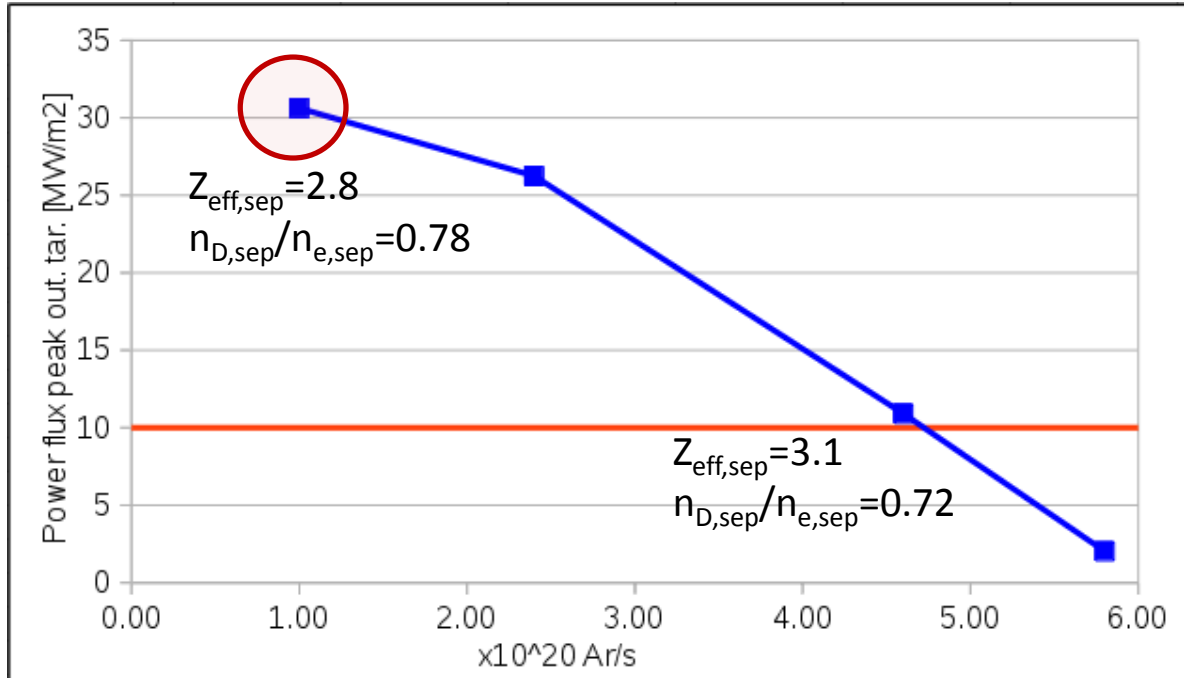


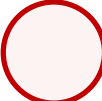


# What if plasma purity is reduced?



Plasma purity defined as:  $\xi = n_{D,sep}/n_{e,sep}$  Scenario reference:  $\xi = 0.8$



 'standard simulation'

$P_{in} = 30\text{MW}$

It is possible to obtain sustainable condition reducing plasma purity

- When detachment is achieved,  $T_{e,sep}$  and pumping is increased. Ar influx is 4 times bigger, total argon content is 2 times bigger but  $T_{e,sep}$  drops from 240eV to 150eV
- Higher separatrix density is not possible due to Greenwald limit



- A good set of input parameters was found simulating compatible JET pulses
- Carbon, carbon+neon and carbon+argon were compared and  $P_{in,max}$  was obtained for all scenarios
- Minimum  $n_{e,sep} = 2 \times 10^{19} m^{-3}$
- Sustainable power loads can be obtained with  **$P_{in,max} = 20/23$  MW.**  
Correspondent  **$P_{aux} = 30/34$  MW**
- It is possible to achieve sustainable condition with maximum input power decreasing plasma purity of 10%



## Foreseen activities:

- Modelling of *Initial research phase* scenario with SOLEDGE2D-EIRENE (G. Falchetto)
- Possible modelling activity with SOLEDGE3X
- Development of synthetic diagnostics (ex. VUV)
- Development of tool for experimental data analysis for edge modelling
- Study of possible interesting scenarios for the initial research phase

## Future area of interests (2022+):

- Studying the effects of drifts on plasma radiation and divertor power load distribution
- Modelling of double-null configuration (towards extended research phase – W wall)



Thank you for your attention