

Interim report of project TOKEDGE

A BOUT++ extension for interplay between flow, low-n mode and turbulence

Haruki Seto (QST)

Project Title: Collaboration on code development and simulations of tokamak edge MHD and turbulence (FY2020-FY2021, 2 years)

- Introduction: BOUT++ code and objectives of TOKEDGE project
- Numerical Issue on Poisson solvers in BOUT++ and a new 2D Poisson solver for low-n modes
- Verification test of 2D Poisson solver by linear problems (pressure-driven modes)
- Preliminary pedestal collapse simulation in annular full torus domain in shifted circular geometry
- Summary and future work (research plan in FY2021)

BOUT++ framework as an edge tokamak simulation code [Dudson CPC2009]

- BOUT++ calculates middle- n ($O(n) > 1$) and high- n ($O(n) \gg 1$) structure with high accuracy in complex boundary region in tokamak plasmas
- BOUT++ employs flute-ordering $k_{\parallel} = 0$ on Poisson solver for $n \neq 0$ modes calculating flow potential from vorticity
 - ✓ Flute-ordering may not be accurate for low- n modes ($O(n) \sim 1$) especially in diverted geometries

TOKEDGE is a two years project to extend BOUT++ framework for tokamak edge simulation solving interplay between $n=0$, low- n , middle- n and high- n modes in diverted geometries

➔ **improvement of current-driven ELMs, RMPs, full annular torus edge turbulence simulations, etc...**

- FY2020: development of flute-ordering-free Poisson solver for low- n modes (main topic of this talk)

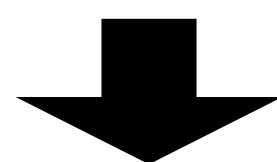
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BOUT++ describes differential operators with **radial (ψ) derivative of flux surface coords. (ψ, θ, ζ)** and **parallel (y) derivative of field-aligned coords. (x, y, z)** a.k.a. shifted metric and radial derivative method

Linearized Poisson solver for $n=n'$ mode vorticity ($n_{i1}/n_{i0} \ll O(1)$) in Fourier space

$$U_1(\cdot, \cdot, n') = \nabla \cdot \left(\frac{n_{i0}}{B_0} \nabla_{\perp} \phi_1 \right) = \mathcal{L}_{\text{shifted}}(\partial_{\psi}, \partial_{\psi}^2, \partial_y, \partial_y^2, n) \phi_1(\cdot, \cdot, n') \longrightarrow \phi_1(\cdot, \cdot, n') = \mathcal{L}_{\text{shifted}}^{-1}(\partial_{\psi}, \partial_{\psi}^2, \partial_y, \partial_y^2, n') U_1(\cdot, \cdot, n') \quad ?$$

Poisson solver however **cannot be defined as a boundary problem straightforwardly** due to coexistence of **ψ -derivatives (flux-surface coords.)** and **y -derivatives (field-aligned coords.)**



- **1D Poisson solver in flux-surface coordinates** for $n \neq 0$ modes using flute-ordering approximation ($\partial_y = 0$) [Dudson CPC2009]

$$\phi_1(\psi, \theta, n') = \mathcal{L}_{\text{shifted}}^{-1}(\partial_{\psi}, \partial_{\psi}^2, n') U_1(\psi, \theta, n')$$

- **2D Poisson solver in field-aligned coordinates** for $n=0$ mode using toroidal symmetry ($\partial_x = \partial_{\psi} + I \partial_{\zeta} = \partial_{\psi}$) [Dudson PPCF2017]

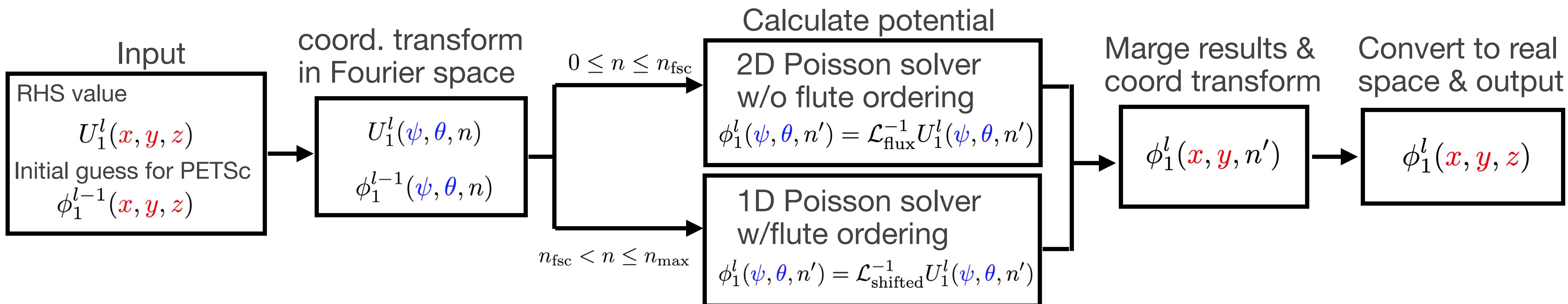
$$\phi_1(x, y) = \mathcal{L}_{\text{shifted}}^{-1}(\partial_x, \partial_x^2, \partial_y, \partial_y^2) U_1(x, y)$$

- **2D Poisson solver in flux-surface coordinates** for low-n modes with flux-surface coordinates' metrics

$$\phi_1(\psi, \theta, n') = \mathcal{L}_{\text{flux surface}}^{-1}(\partial_\psi, \partial_\psi^2, \partial_\theta, \partial_\theta^2, n')U_1(\psi, \theta, n')$$

- **Self-consistent flow potential without flute-ordering for low-n modes**
- **Poloidal grid resolution must be fine enough to describe poloidal structure of low-n modes**
- Iterative solver (PETSc library+ hypre* preconditioning) based on Ref.[Dudson PPCF 2017]
- Applicable for non-diverted geometry (circular), single-null and double-null diverted geometries

Workflow in Poisson solver function developed in TOKEDGE



- Introduction: BOUT++ code and objectives of TOKEDGE project
- Numerical Issue on Poisson solvers in BOUT++ and a new 2D Poisson solver for low-n modes
- Verification test of 2D Poisson solver by linear problems (pressure-driven modes)
 - Ideal ballooning mode instability in shifted circular geometry
 - Resistive ballooning mode instability in single-null diverted geometry
- Preliminary pedestal collapse simulation in annular full torus domain in shifted circular geometry
- Summary and future work

2D Poisson solver is tested by comparing linear IBM growth rate in circular geometry by 2D Poisson solver and 1D flute-ordered Poisson solver

Linearized IBM model

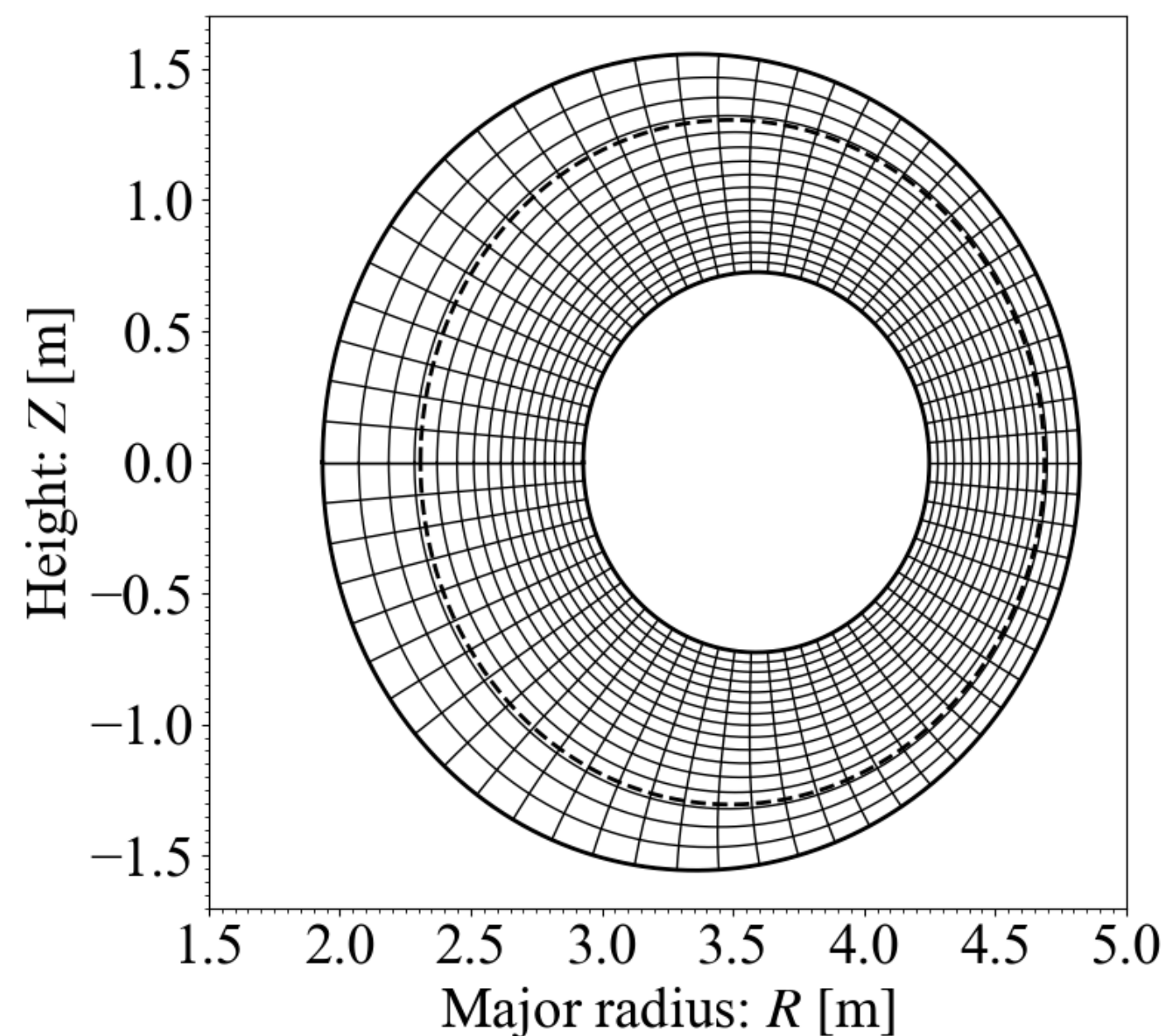
$$\frac{\partial \varpi_1}{\partial t} = B_0 \partial_{\parallel} \left(\frac{J_{\parallel}}{B_0} \right) - B_0 \left[A_{1\parallel}, \frac{J_{\parallel 0}}{B_0} \right] + \frac{\mathbf{b}_0 \times \boldsymbol{\kappa}_0 \cdot \nabla P_1}{B_0}$$

$$\frac{\partial P_1}{\partial t} = - [\phi_1, P_0]$$

$$\frac{\partial A_{\parallel 1}}{\partial t} = - \partial_{\parallel} \phi_1$$

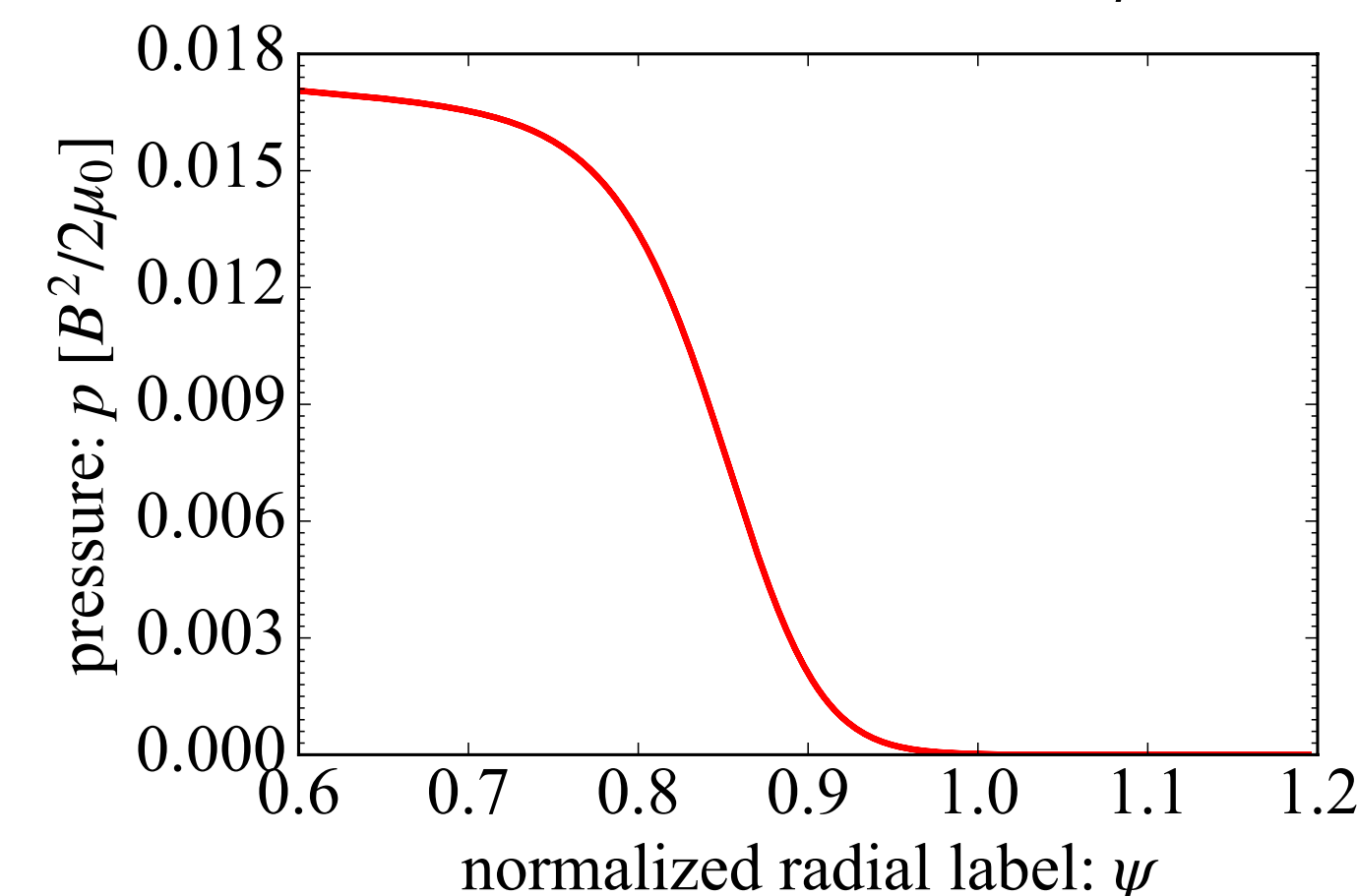
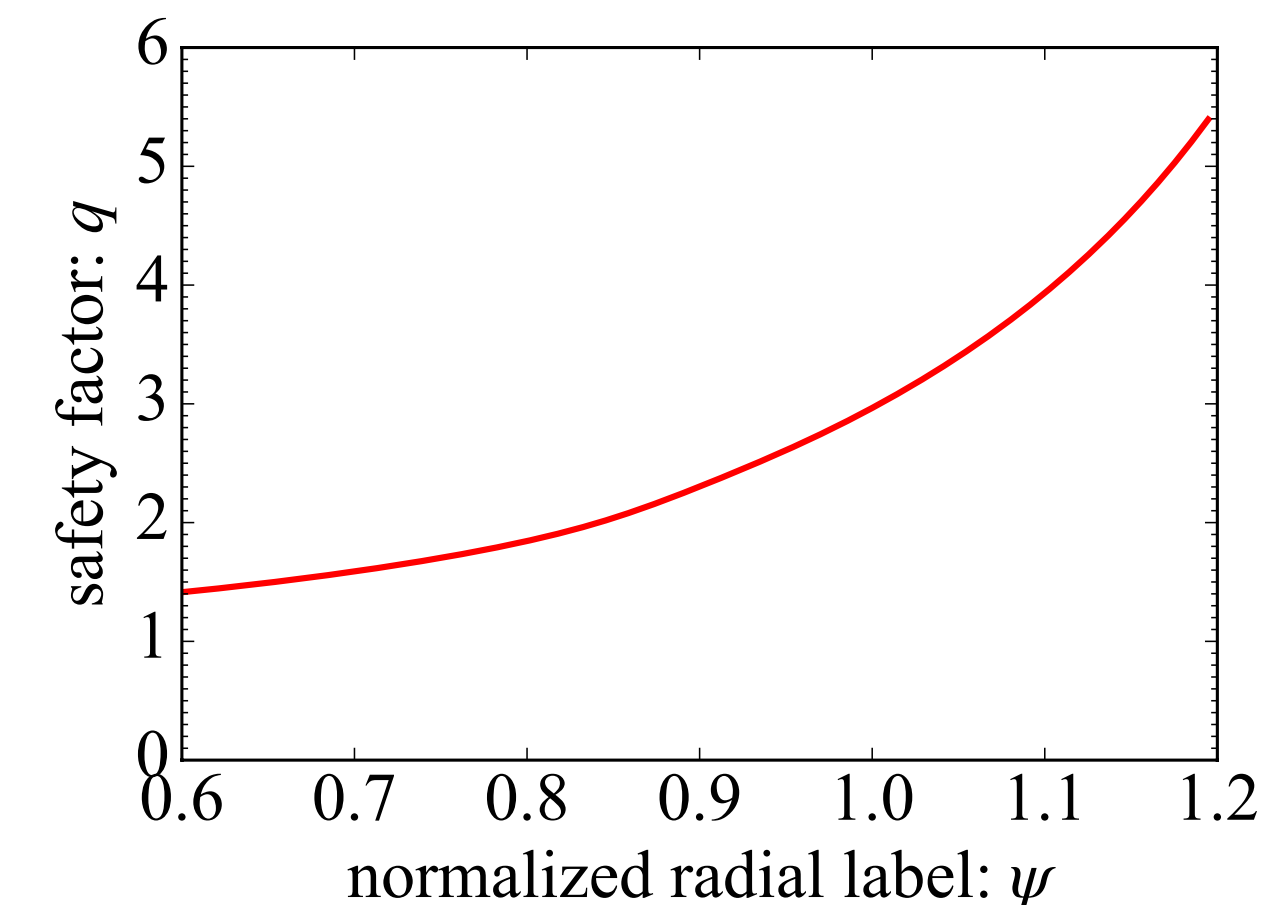
$$\varpi_1 = \nabla \cdot \left(\frac{1}{B_0^2} \nabla_{\perp} \phi_1 \right), \quad J_{\parallel 1} = \nabla_{\perp}^2 A_{\parallel 1}$$

- constant ion density $n_{i0} = 10^{19} \text{ [m}^{-3}\text{]}$
- normalized with poloidal Alfvén unit

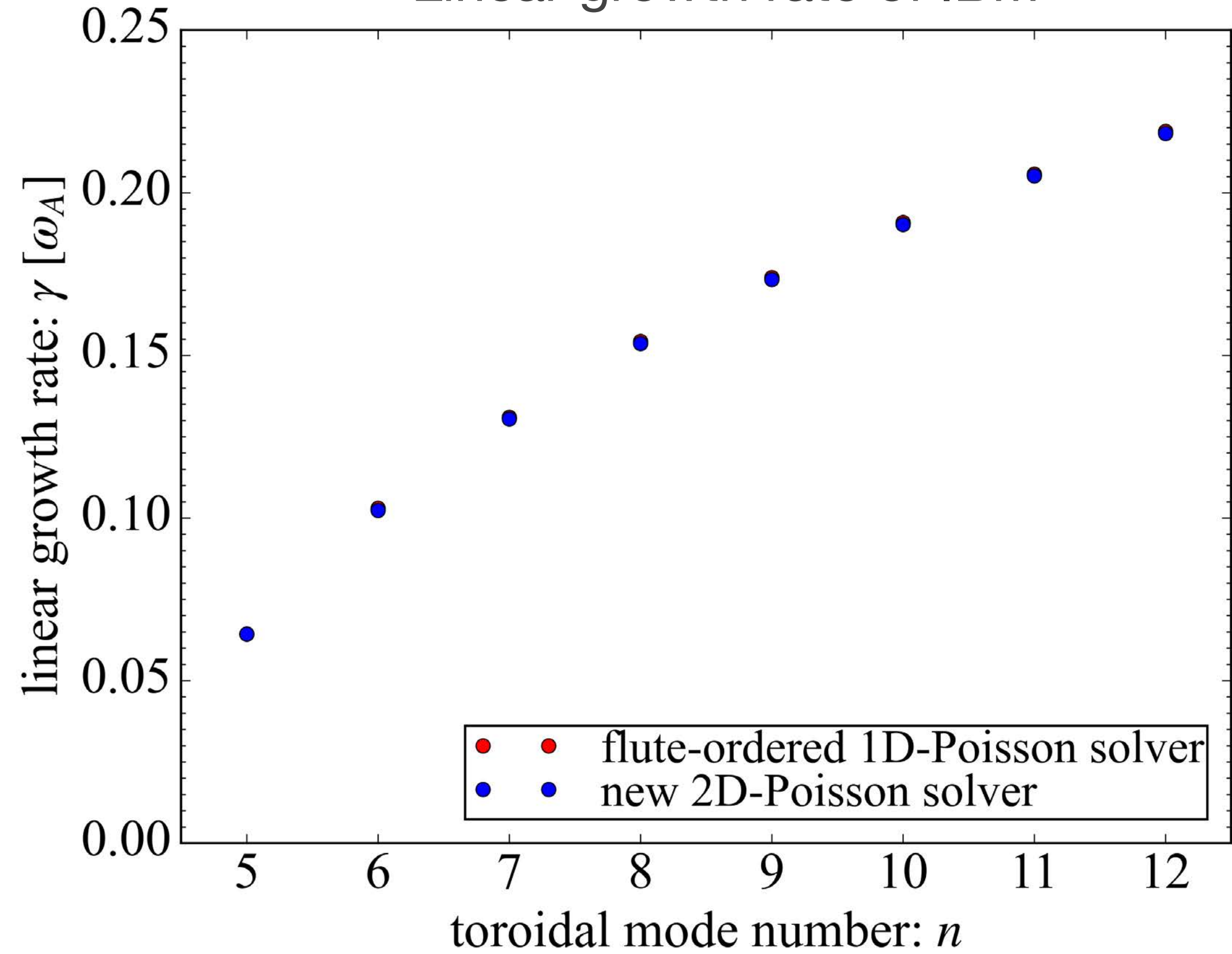


Resolution	Nx	Ny	Nz
1D Poisson	512	64	16
2D Poisson	512	512	16

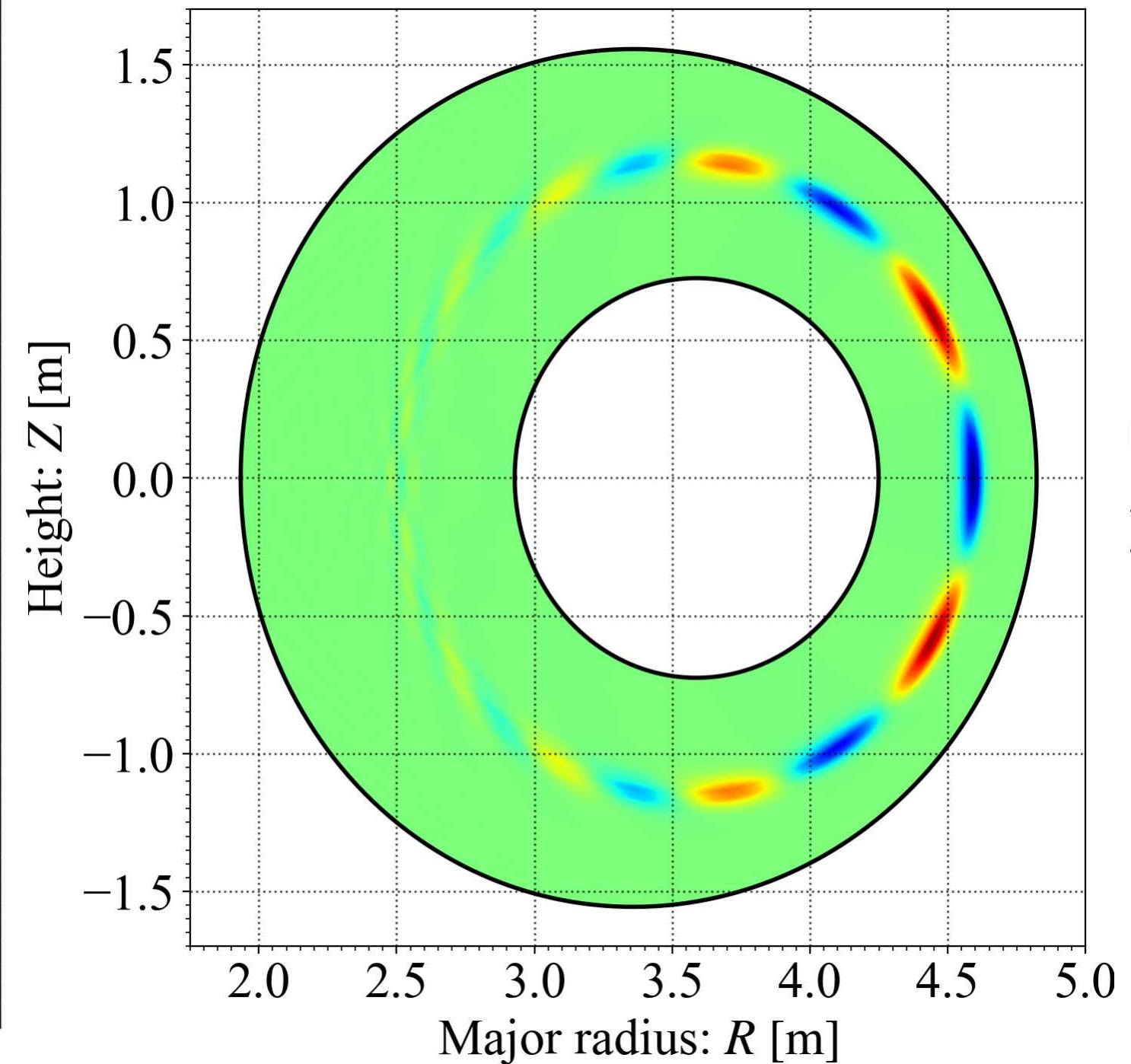
- $1/n$ -th annular wedge domain for $n=5, \dots, 12$
- z-derivatives are evaluated with FFT



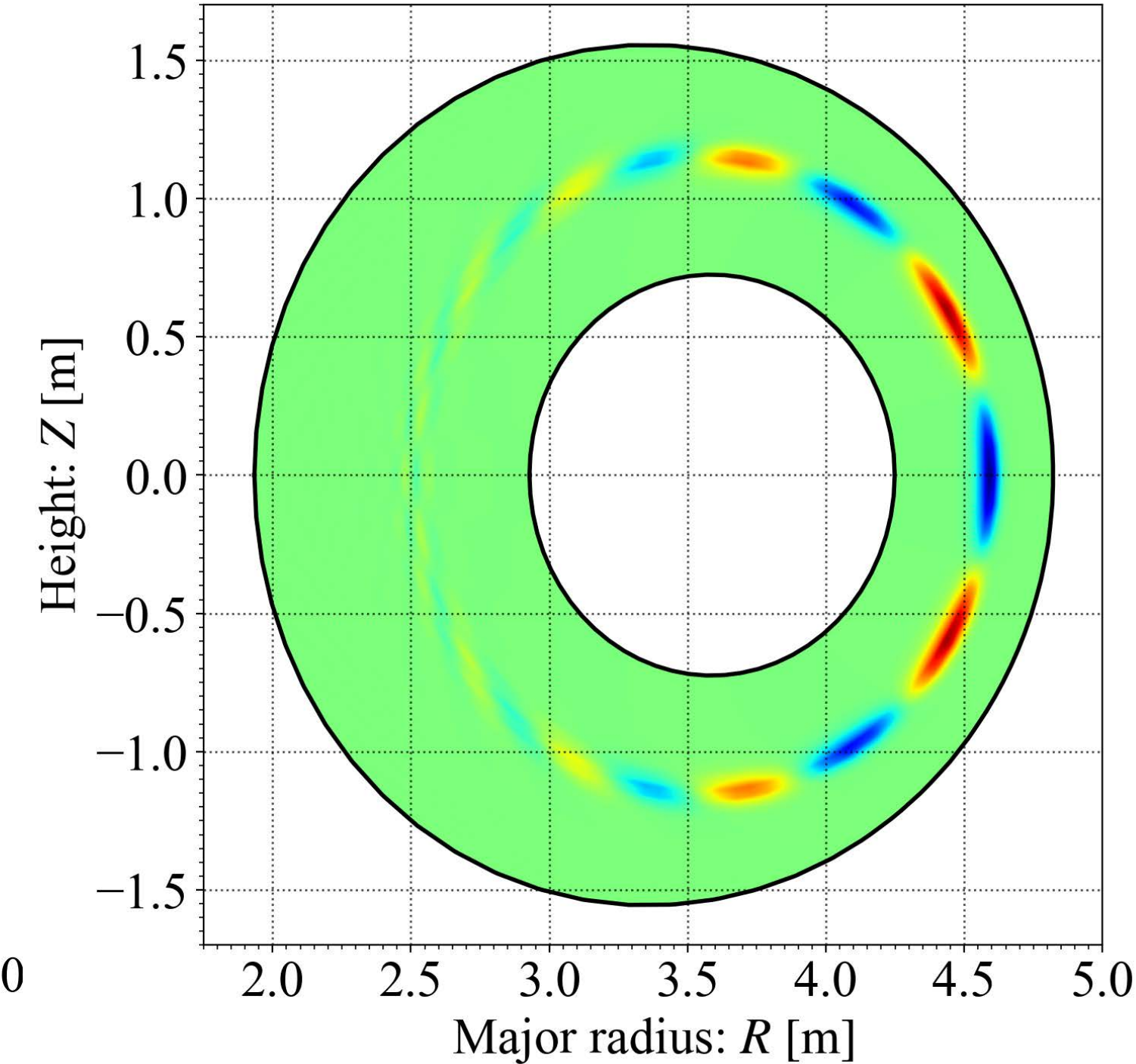
Linear growth rate of IBM



$n=5$ perturbed pressure by 2D Poisson solver



$n=5$ perturbed pressure by 1D Poisson solver



- IBM growth rates show good agreement
- 2D Poisson solver test with current-driven linear instabilities is in preparation

2D Poisson solver is tested in single-null geometry by comparing linear RBM growth rates by 2D Poisson solver and those by 1D flute-ordered Poisson solver

Linearized RBM model with dissipation

$$\frac{\partial \varpi_1}{\partial t} = B_0 \partial_{\parallel} \left(\frac{J_{\parallel}}{B_0} \right) - B_0 \left[A_{1\parallel}, \frac{J_{\parallel 0}}{B_0} \right] + \frac{\mathbf{b}_0 \times \boldsymbol{\kappa}_0 \cdot \nabla P_1}{B_0} + \mu_{\perp} \nabla_{\perp}^2 \varpi_1 + \mu_{\parallel} \partial_{\parallel}^2 \varpi_1$$

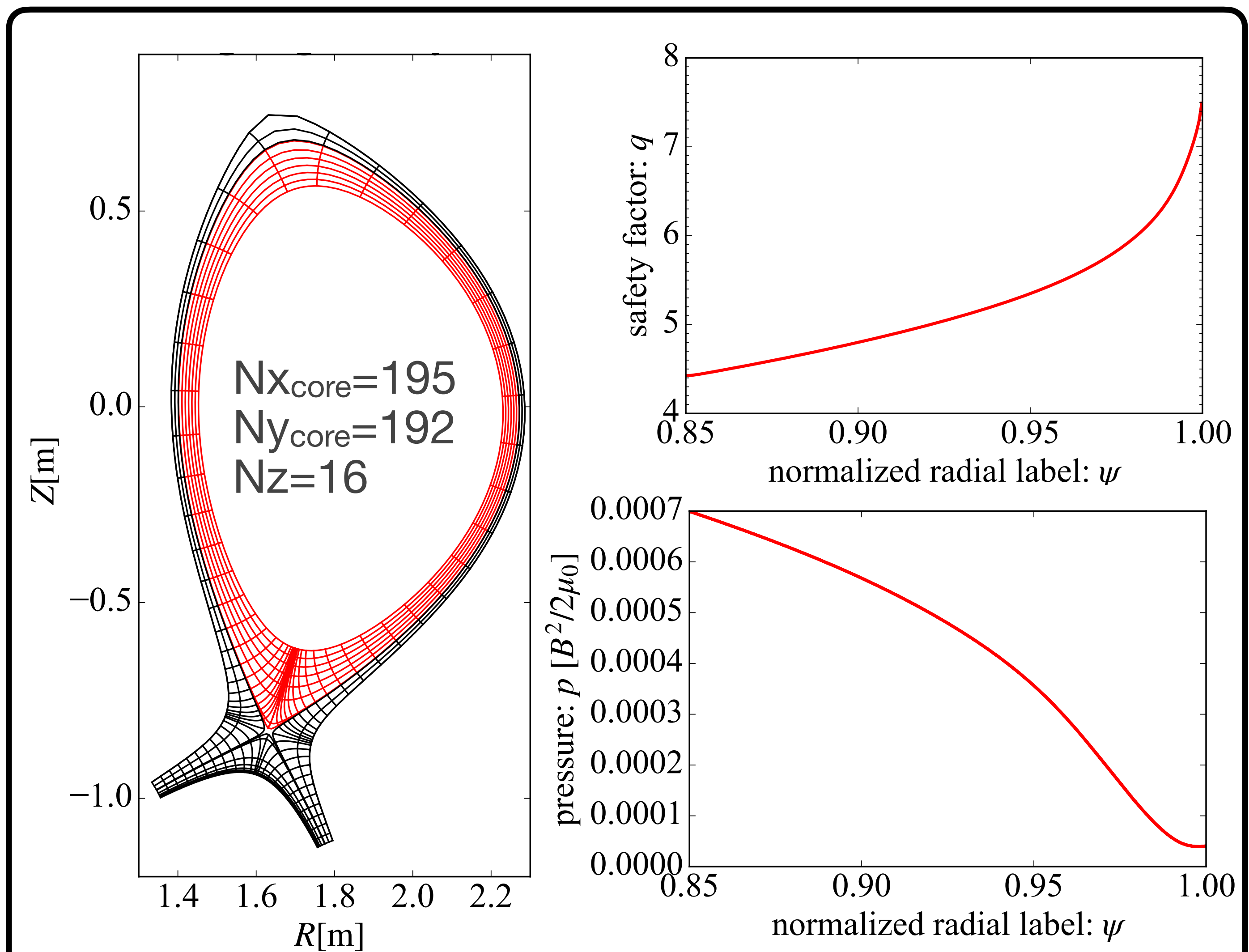
$$\frac{\partial P_1}{\partial t} = -[\phi_1, P_0]$$

$$\frac{\partial A_{\parallel 1}}{\partial t} = -\partial_{\parallel} \phi_1 + \eta J_{\parallel 1}$$

$$\varpi = \nabla \cdot \left(\frac{1}{B_0^2} \nabla_{\perp} \phi \right), \quad J_{\parallel 1} = \nabla_{\perp}^2 A_{\parallel 1}$$

$$\eta = 10^{-6}, \quad \mu_{\perp} = 10^{-7}, \quad \mu_{\parallel} = 10^{-1}$$

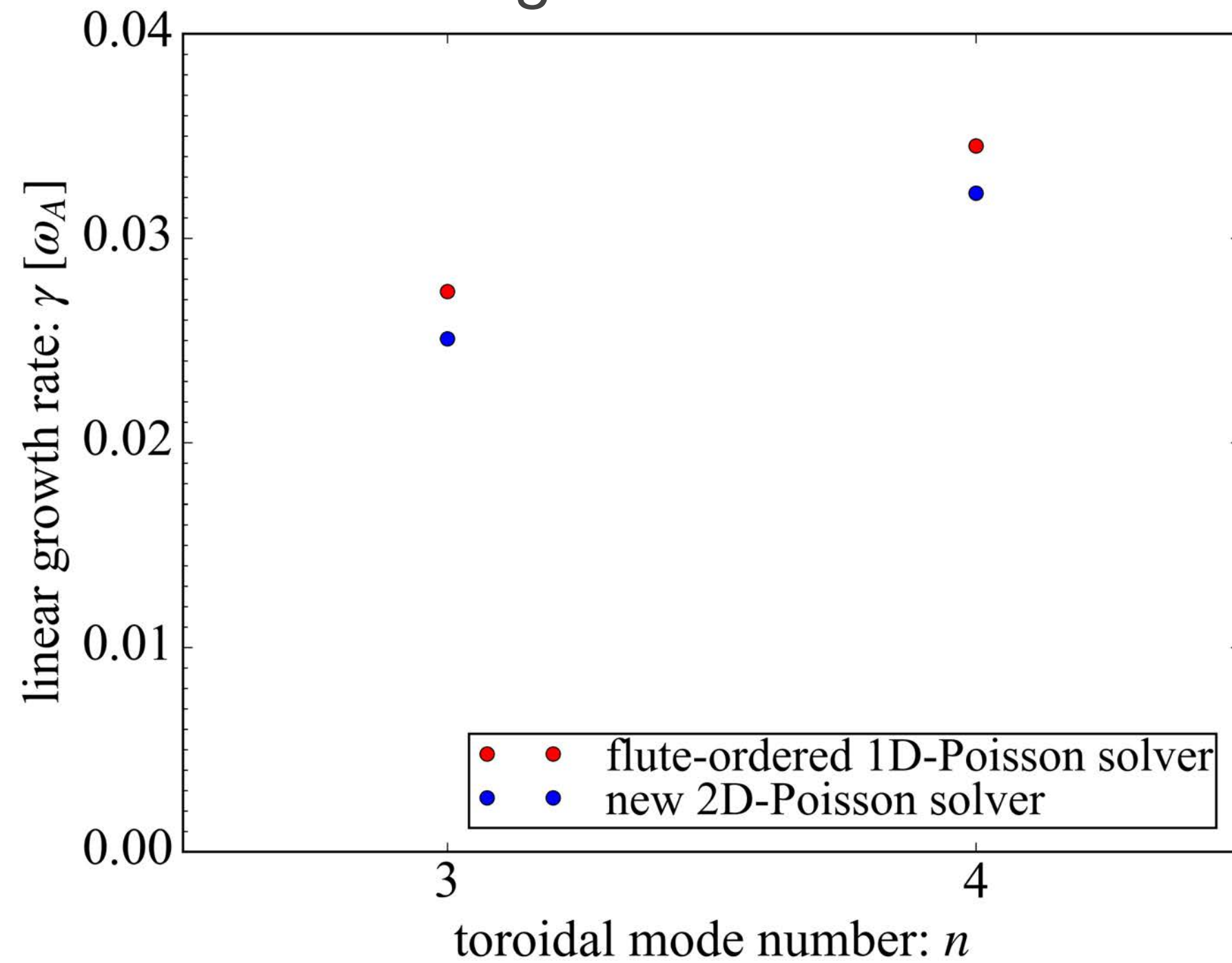
- constant ion density $n_{i0} = 10^{19} \text{ [m}^{-3}\text{]}$
- Dissipations in vorticity equation are required for numerical stability in both 2D and 1D Poisson solver.



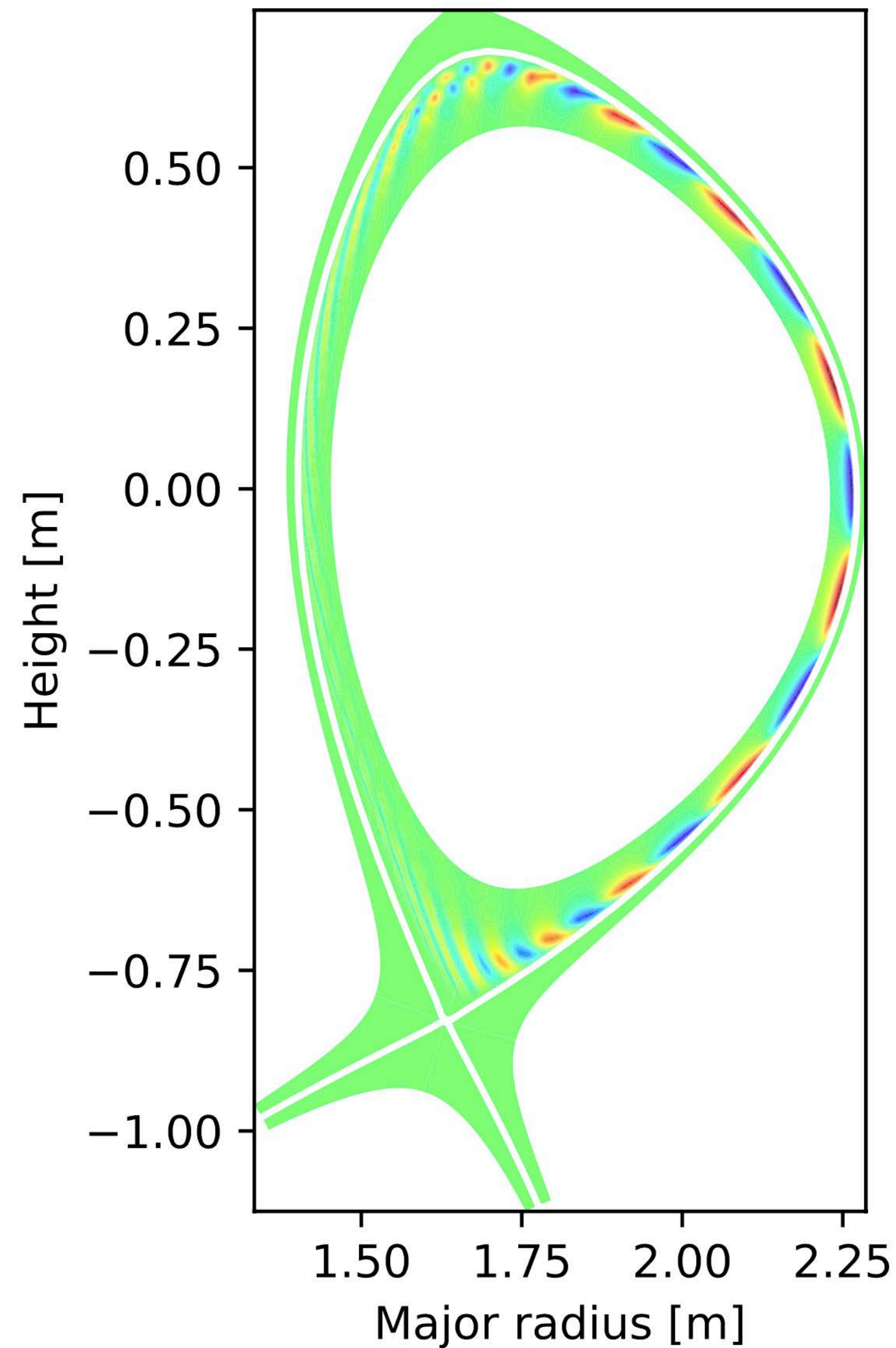
- $1/n$ -th annular wedge domain for $n=3,4$
- z-derivatives are evaluated with FFT

2D Poisson solver captures RBM instability but growth rates are different

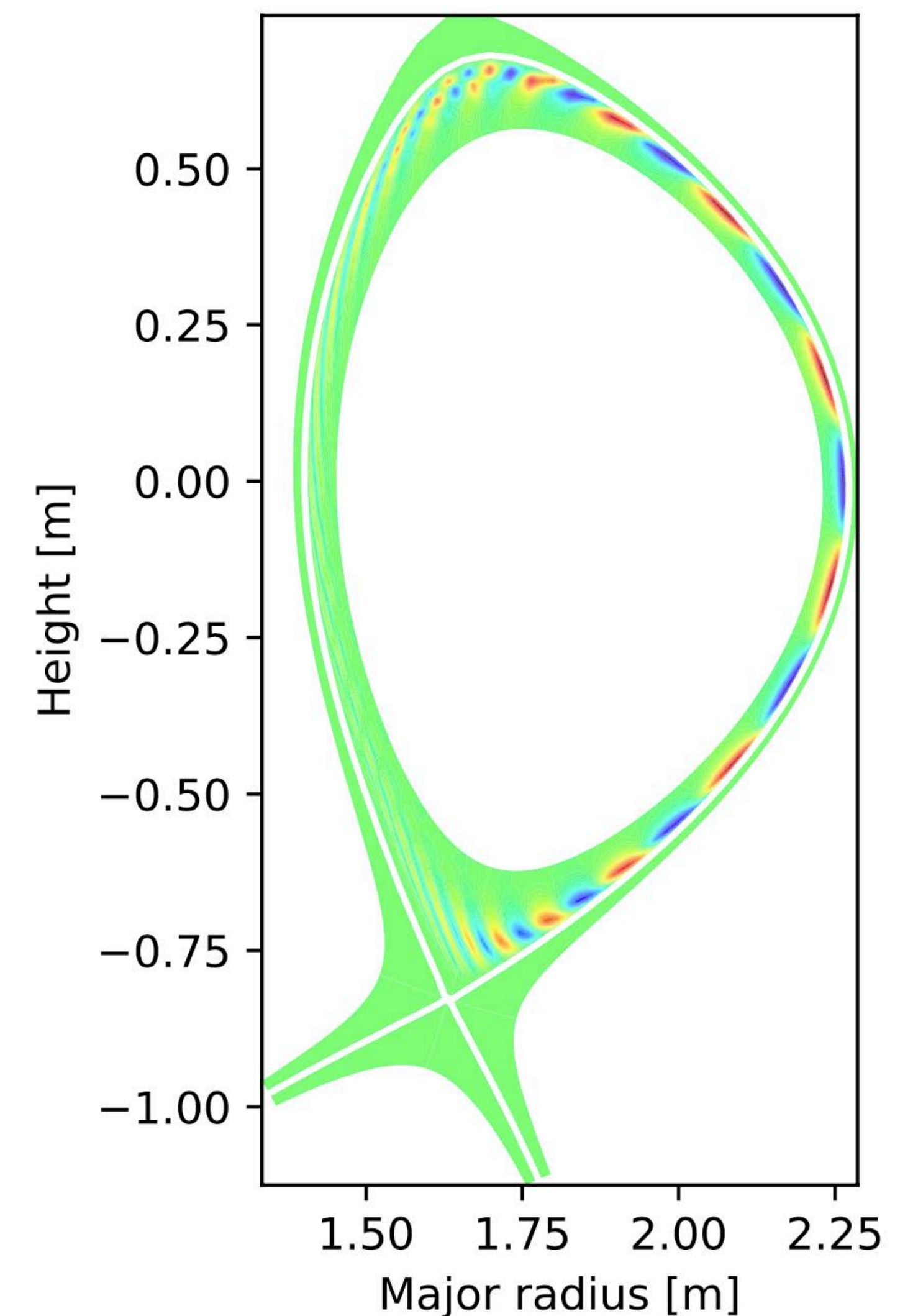
Linear growth rate of RBM



$n=4$ perturbed pressure by 1D Poisson solver



$n=4$ perturbed pressure by 2D Poisson solver



RBM eigen-functions are clearly obtained by both Poisson solvers but their growth rates are different by 6~8%

➔ Further tests (mesh convergence etc...) are required to clarify impact of flute-ordering in complex geometries

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four-field RMHD model: RBM+drift wave [Seto CPP2020]

$$\frac{\partial}{\partial t} \varpi_1 = - [F_1, \varpi] - [F_0, \varpi_1] + \mathcal{C}(p_1, F) + \mathcal{C}(p_0, F_1) - B_0 \partial_{\parallel} \left(\frac{J_{\parallel 1}}{B_0} \right) + B_0 \left[A_{\parallel 1}, \frac{J_{\parallel}}{B_0} \right] + \mathcal{K}(p_1) + \mu_{\parallel} \partial_{\parallel}^2 \varpi_1 + \mu_{\perp} \nabla_{\perp}^2 \varpi_1,$$

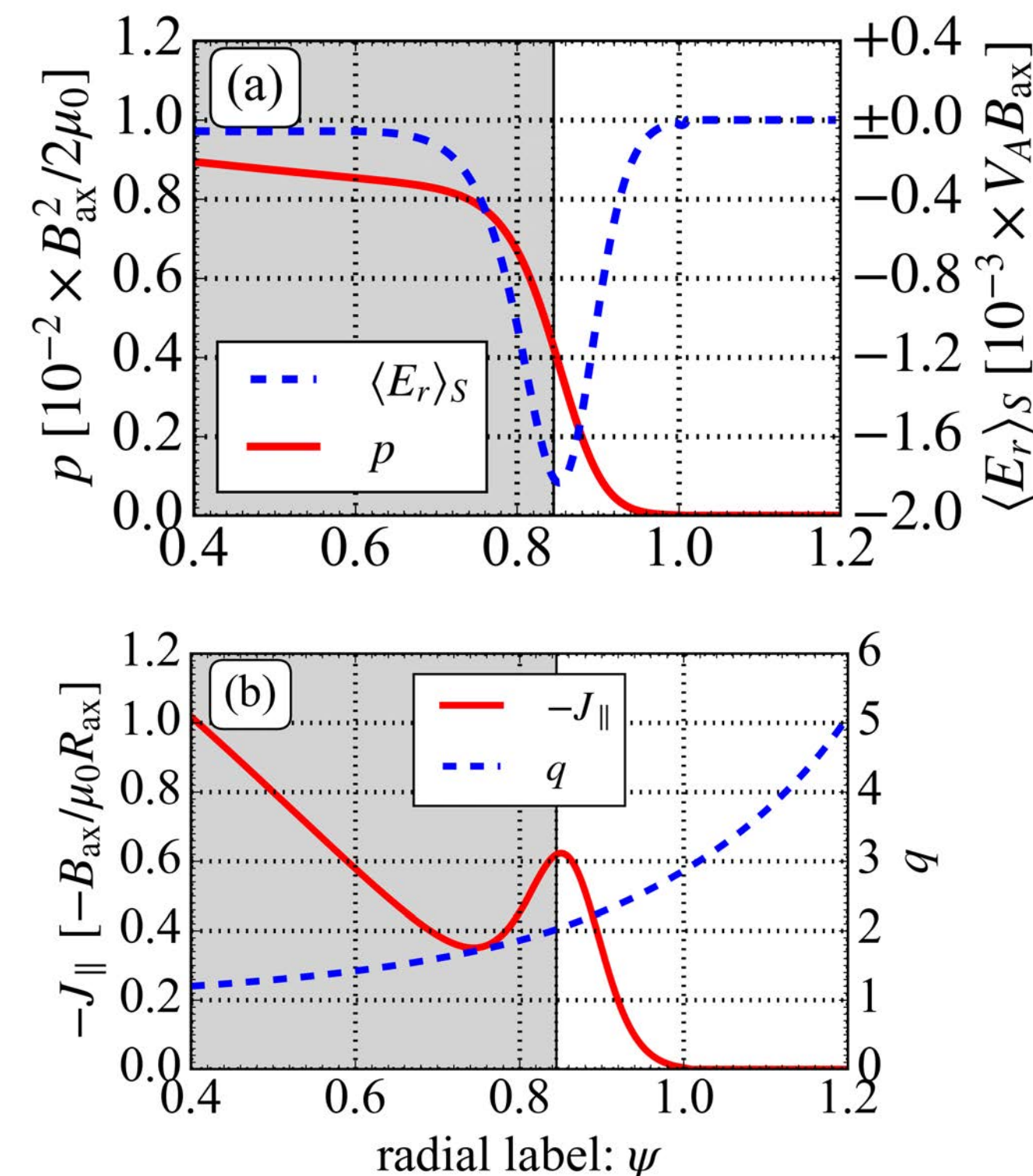
$$\frac{\partial}{\partial t} p_1 = - [\phi_1, p] - [\phi_0, p_1] - 2\beta_* \left(\mathcal{K}(p_1) - B_0 \partial_{\parallel} \left(\frac{v_{\parallel 1} + d_i J_{\parallel 1}}{2B_0} \right) + B_0 \left[A_{\parallel 1}, \frac{v_{\parallel 1} + d_i J_{\parallel 1}}{2B_0} \right] \right) + \chi_{\parallel} \partial_{\parallel}^2 p_1 + \chi_{\perp} \nabla_{\perp}^2 p_1,$$

$$\frac{\partial}{\partial t} A_{\parallel 1} = - [\phi, A_{\parallel 1}] - \partial_{\parallel} \phi_1 + \delta_e (\partial_{\parallel} p_1 - [A_{\parallel 1}, p]) + \eta J_{\parallel 1} - \lambda \nabla_{\perp}^2 J_{\parallel 1},$$

$$\frac{\partial}{\partial t} v_{\parallel 1} = - [\phi, v_{\parallel 1}] - \frac{1}{2} (\partial_{\parallel} p_1 - [A_{\parallel 1}, p]) + v_{\perp} \nabla_{\perp}^2 v_{\parallel 1},$$

$$\varpi = \nabla_{\perp}^* F, \quad J_1 = \nabla_{\perp}^2 A_{\parallel}, \quad F = \phi + \delta_i p, \quad \phi = \phi_0 + \phi_1, \quad p = p_0 + p_1, \quad \mathbf{B} = \mathbf{B}_0 + \nabla A_{\parallel 1} \times \mathbf{b}_0, \quad J_{\parallel} = J_{\parallel 0} + J_{\parallel 1},$$

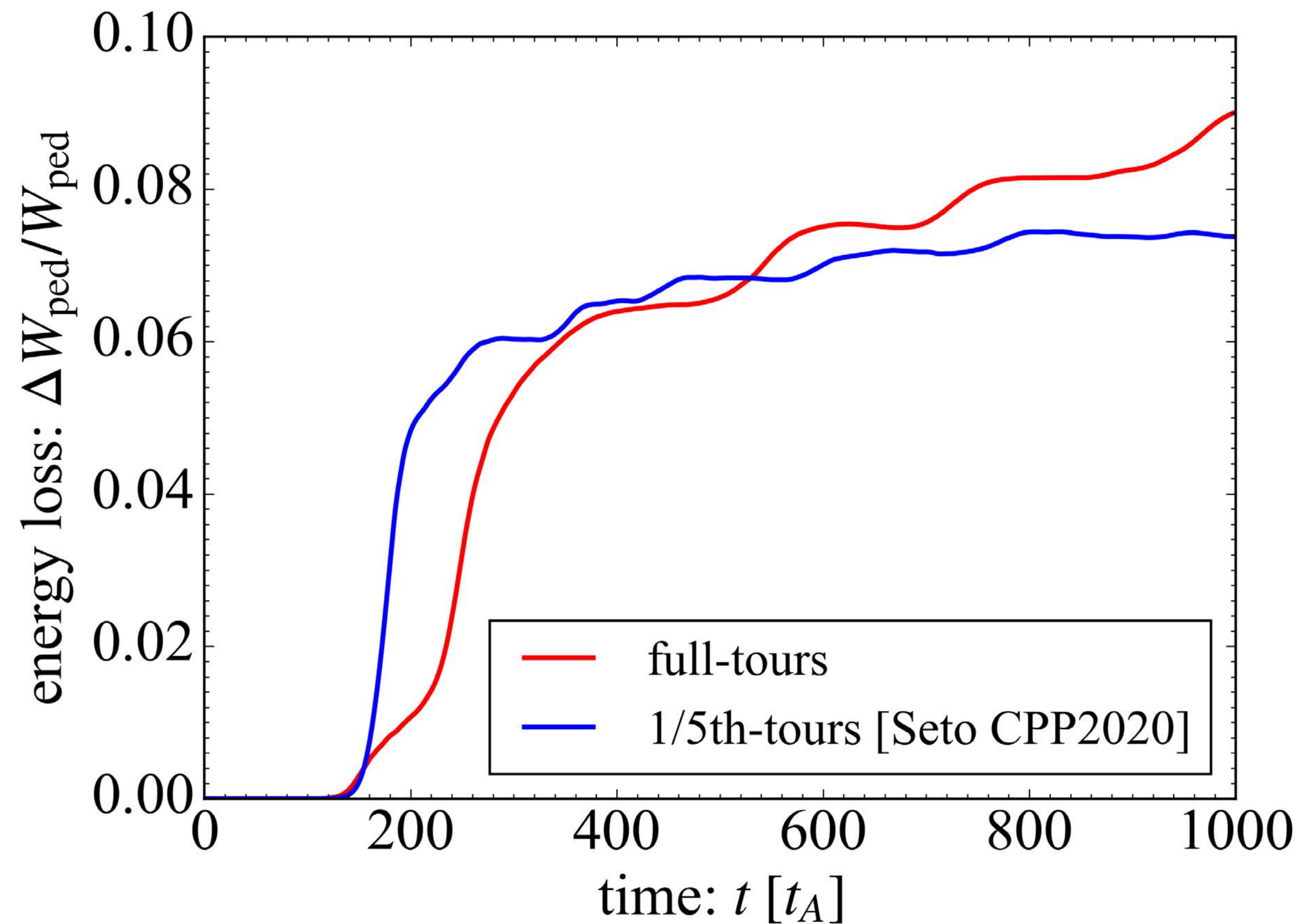
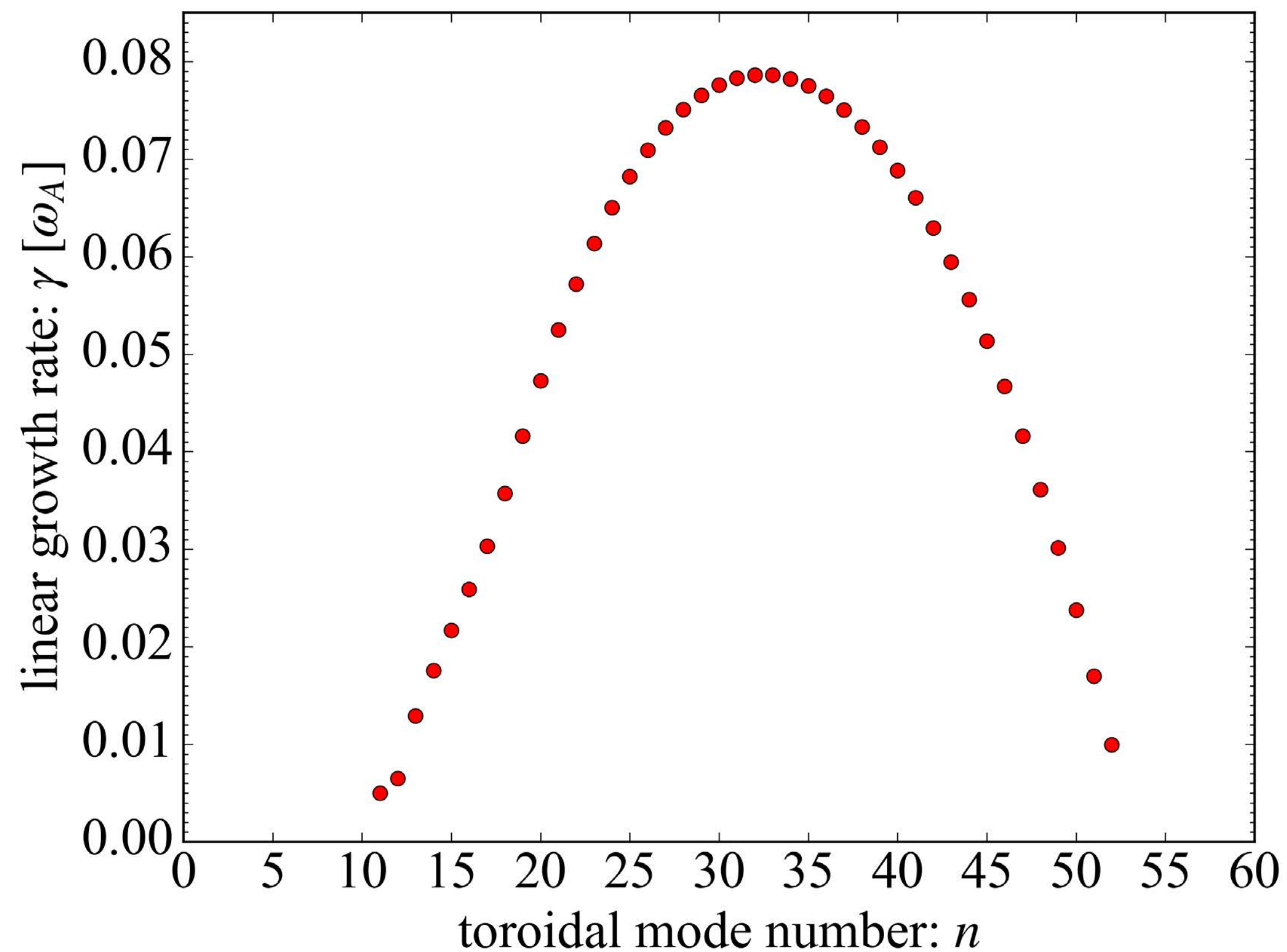
$$n_{i0} = 10^{19} [m^{-3}], \quad \eta = 10^{-8}, \quad \lambda = 10^{-12}, \quad \mu_{\perp} = \chi_{\perp} = \nu_{\perp} = 10^{-7}, \quad \mu_{\parallel} = \chi_{\parallel} = 10^{-1}$$



IBM marginally stable shifted circular equilibrium

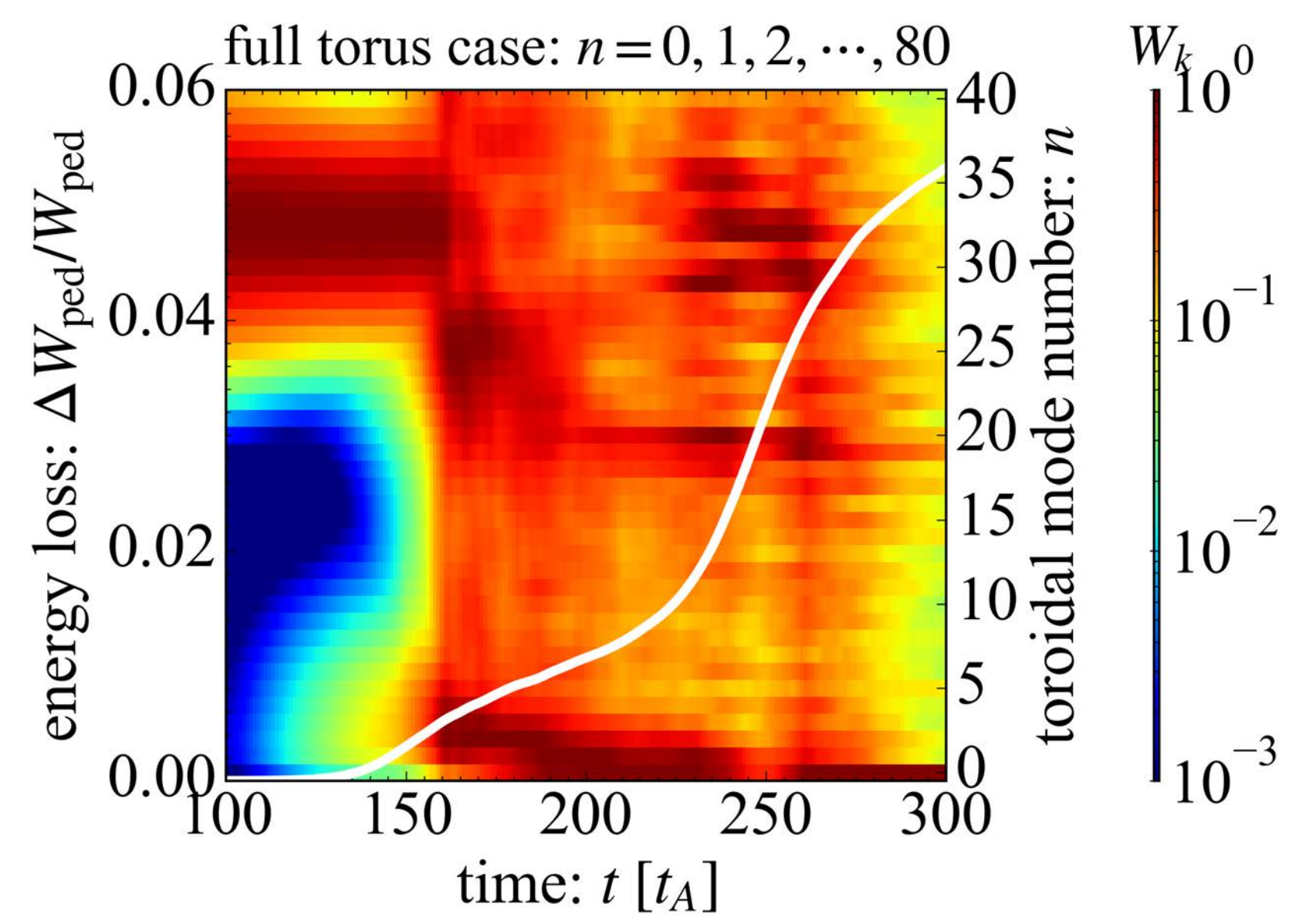
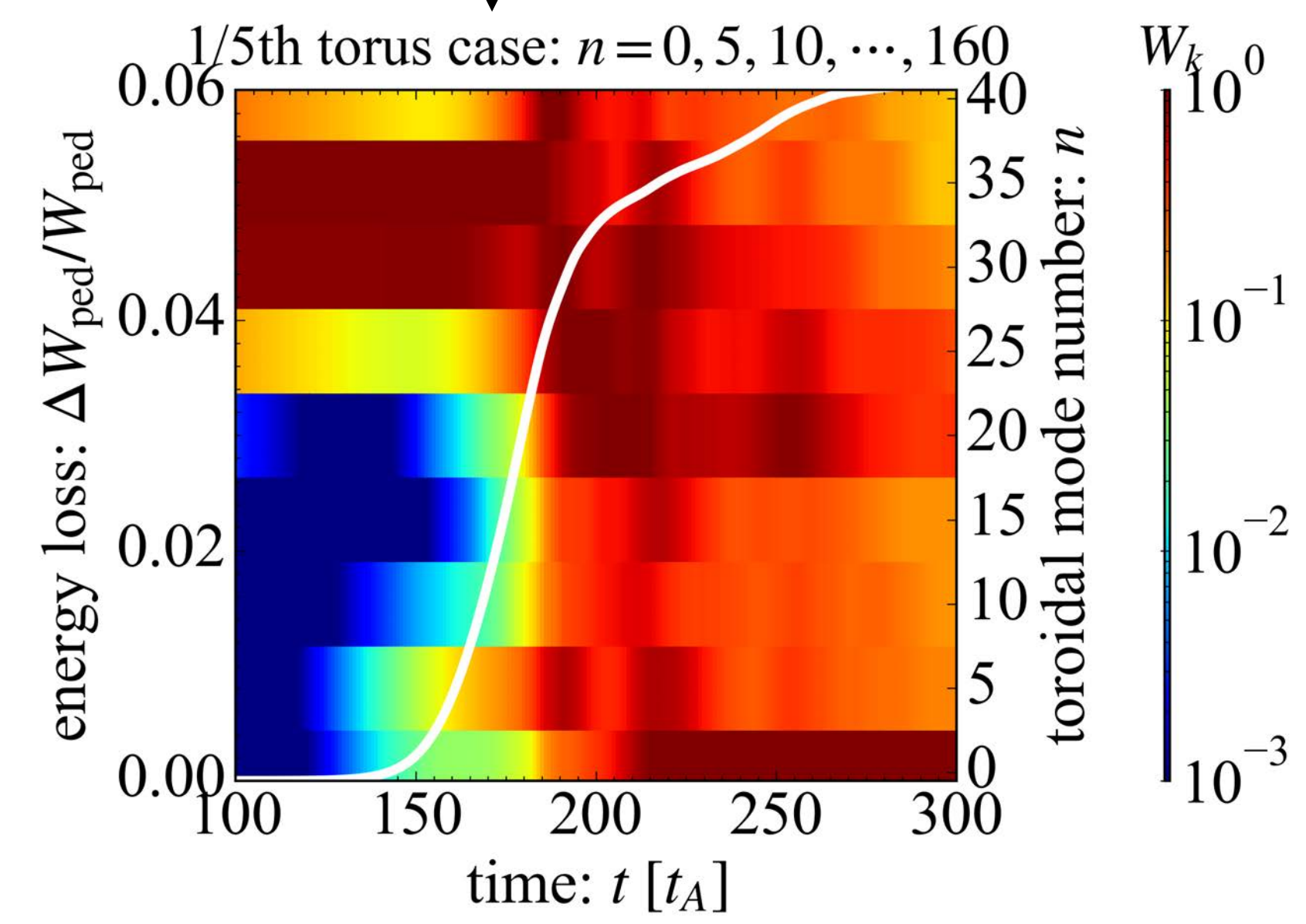
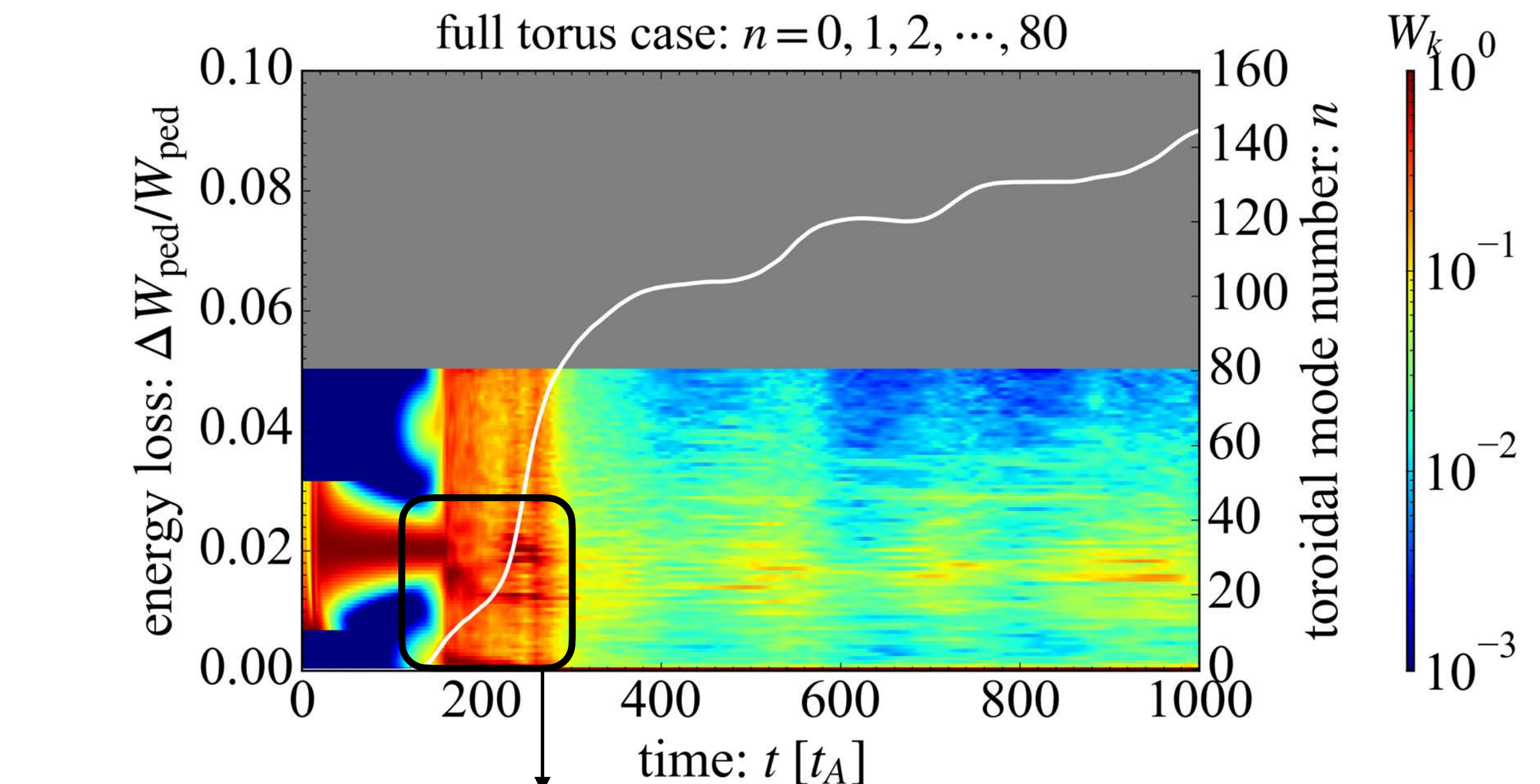
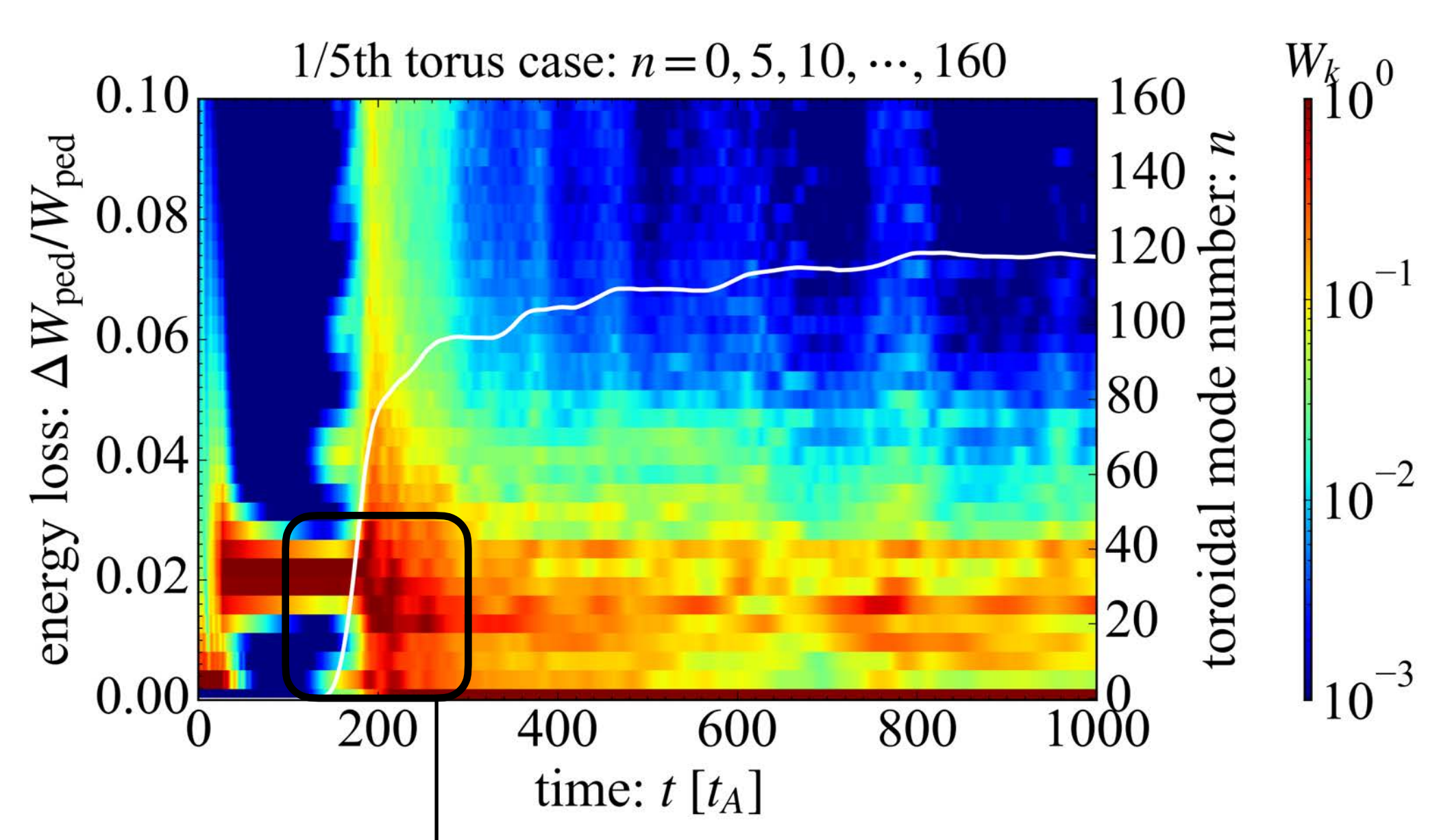
- Resolution: $N_x=512$, $N_y=128$, $N_z=256$ ($n=0,1,\dots,80$) for full annular tours
 - $n=0,1,2,3,4$ modes are solved with 2D Poisson solver without flute-ordering
 - $n=5,6,\dots,80$ modes are solved with 1D Poisson solver with flute-ordering
- just for test run and radial and toroidal resolution may not be not enough for production run
 - cf.) **$N_x=1536$** , $N_y=64$, $N_z=129$ for 1/5th annular tours (**$n=0,5,\dots,155,160$**) in Seto CPP2020

Pedestal collapse is triggered by $n \sim 30$ resistive ballooning modes



Computational cost for full tours simulation: 2048core x 2day in JFRS1

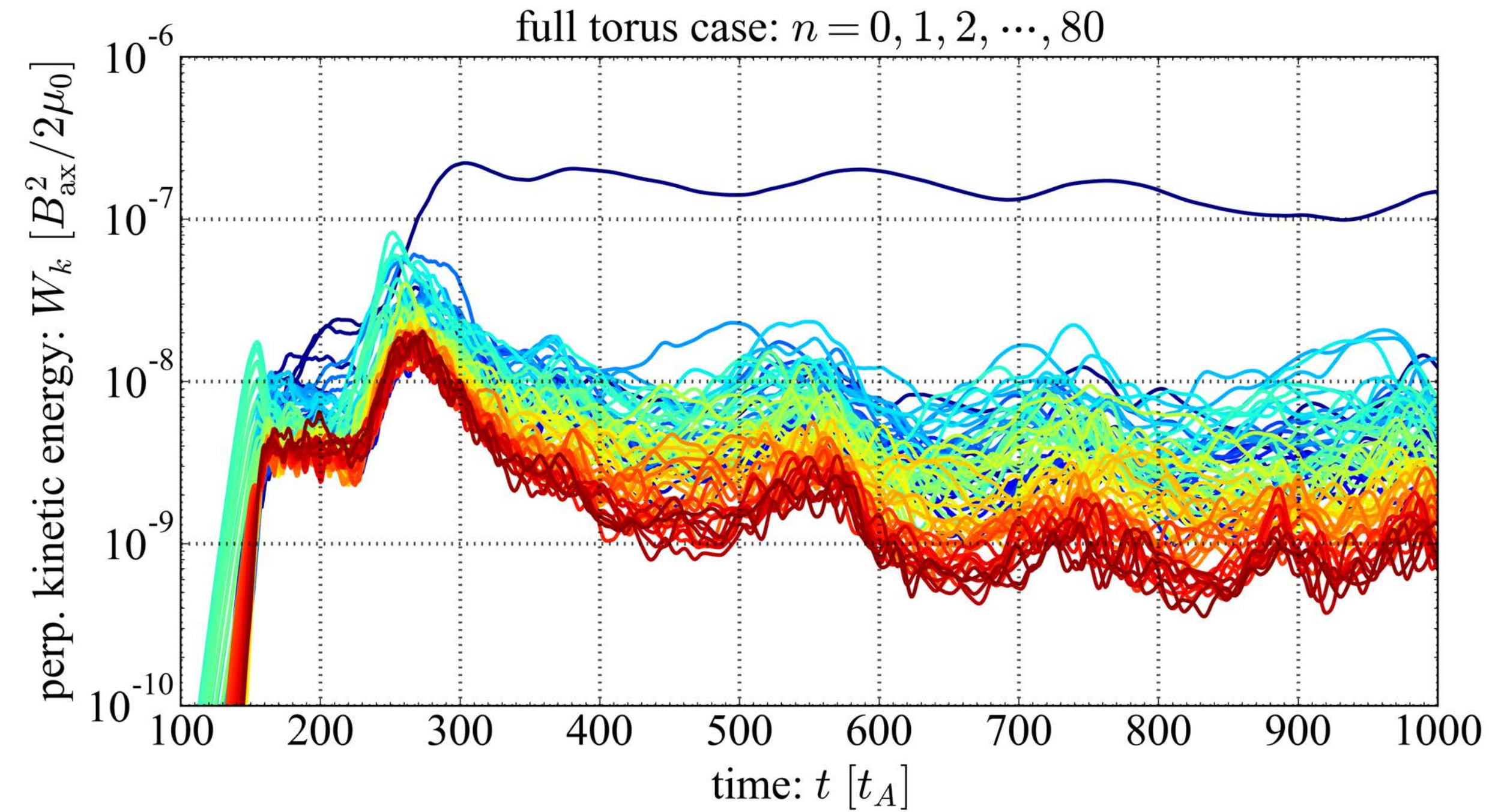
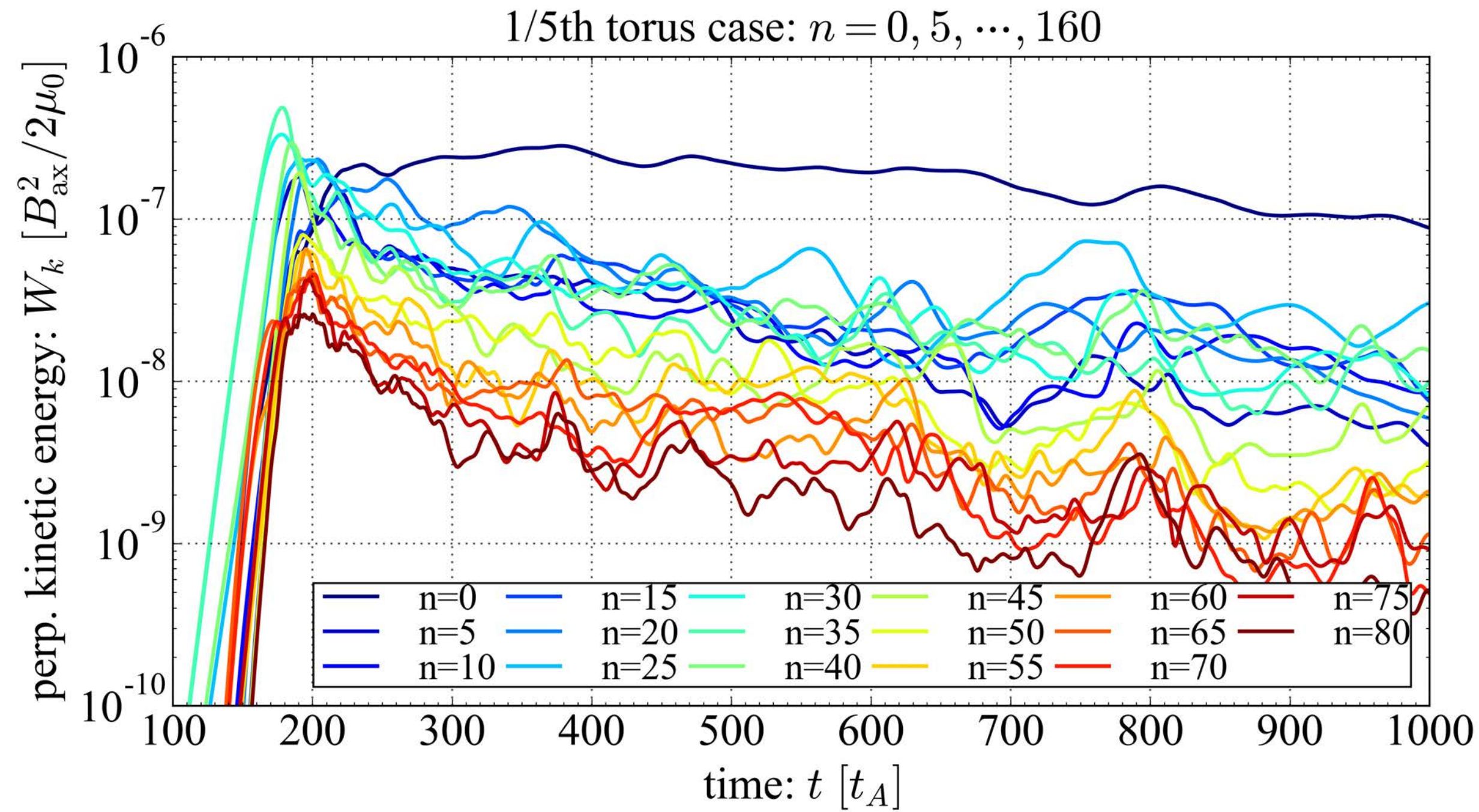
Energy loss dynamics during pedestal collapse changes qualitatively



W_k :
perpendicular
kinetic energy

$$W_k = \int_V \frac{|\nabla_{\perp} F_1|^2}{2B_0^2} dV$$

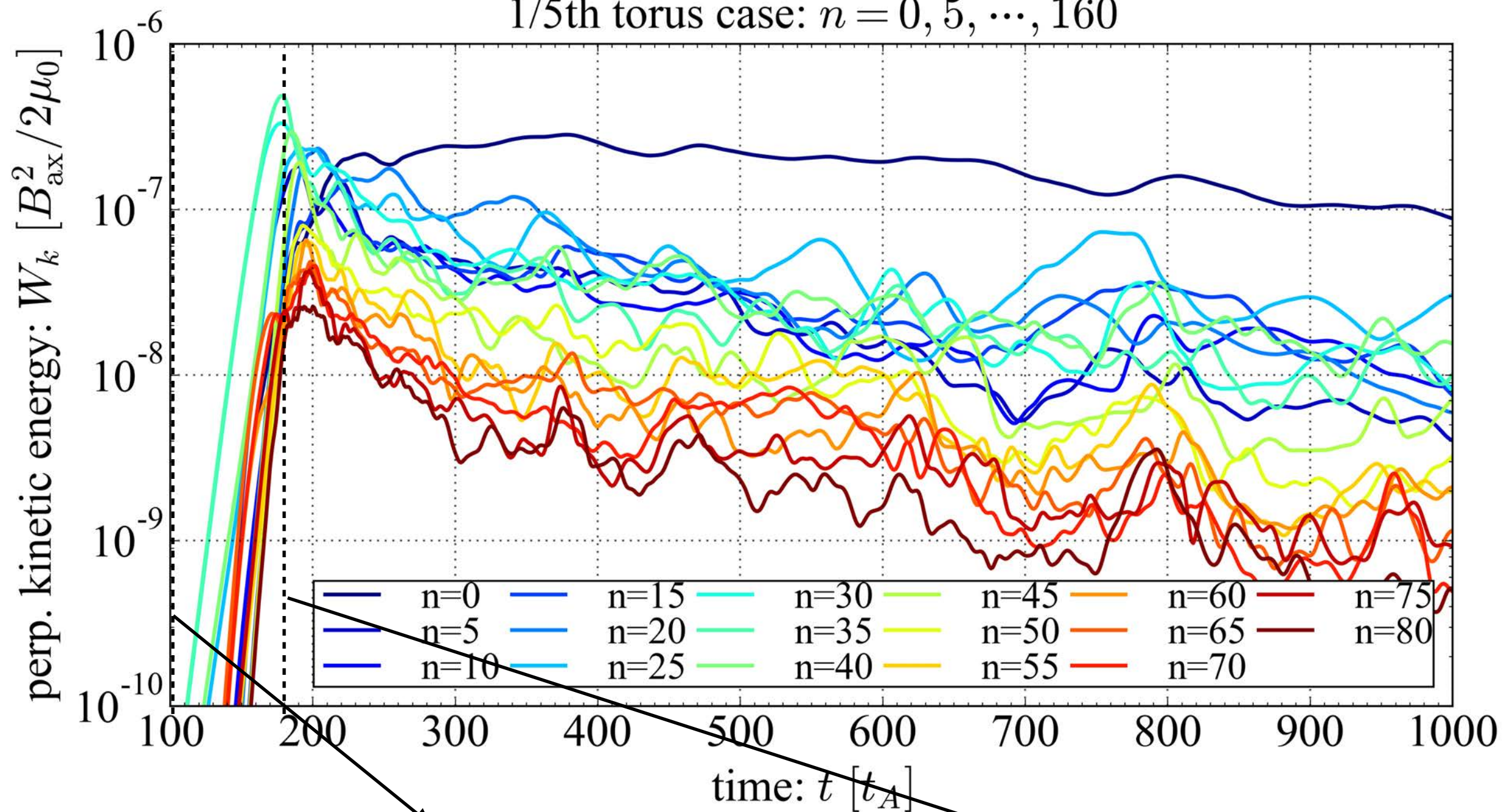
Time evolution of perpendicular kinetic energy from $n=0$ to $n=80$



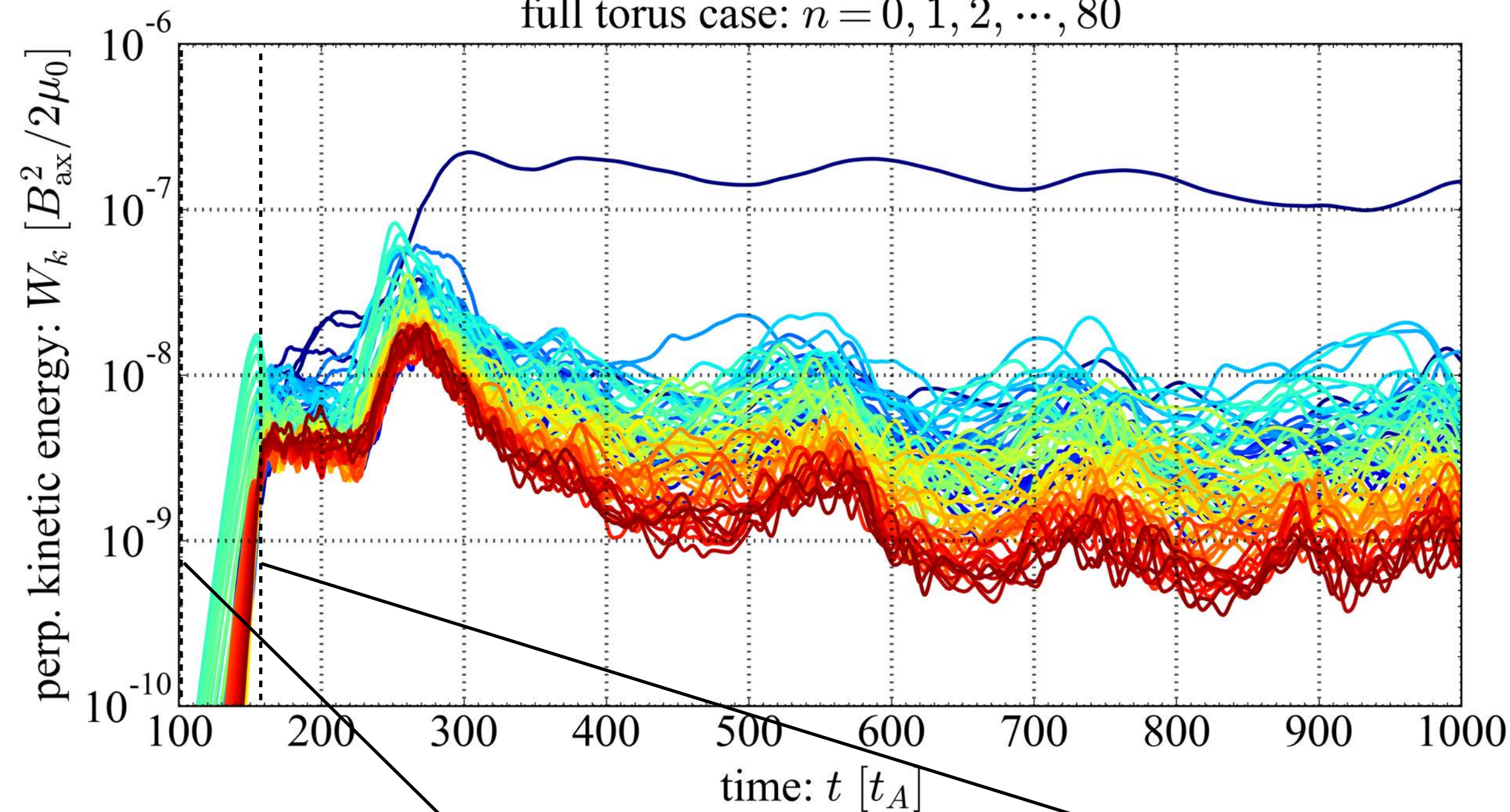
- Amplitude of kinetic energy of most unstable mode decreases by one order in full torus case
 ➔ increase of unstable toroidal modes driving pedestal collapse in simulated system
- Amplitude of zonal flow ($n=0$ energy) after pedestal collapse are similar order $O(10^{-7})$
- Pedestal collapse has two phases in full torus case

perpendicular kinetic energy spectrums just before 1st crash show similar trend

1/5th torus case: $n = 0, 5, \dots, 160$

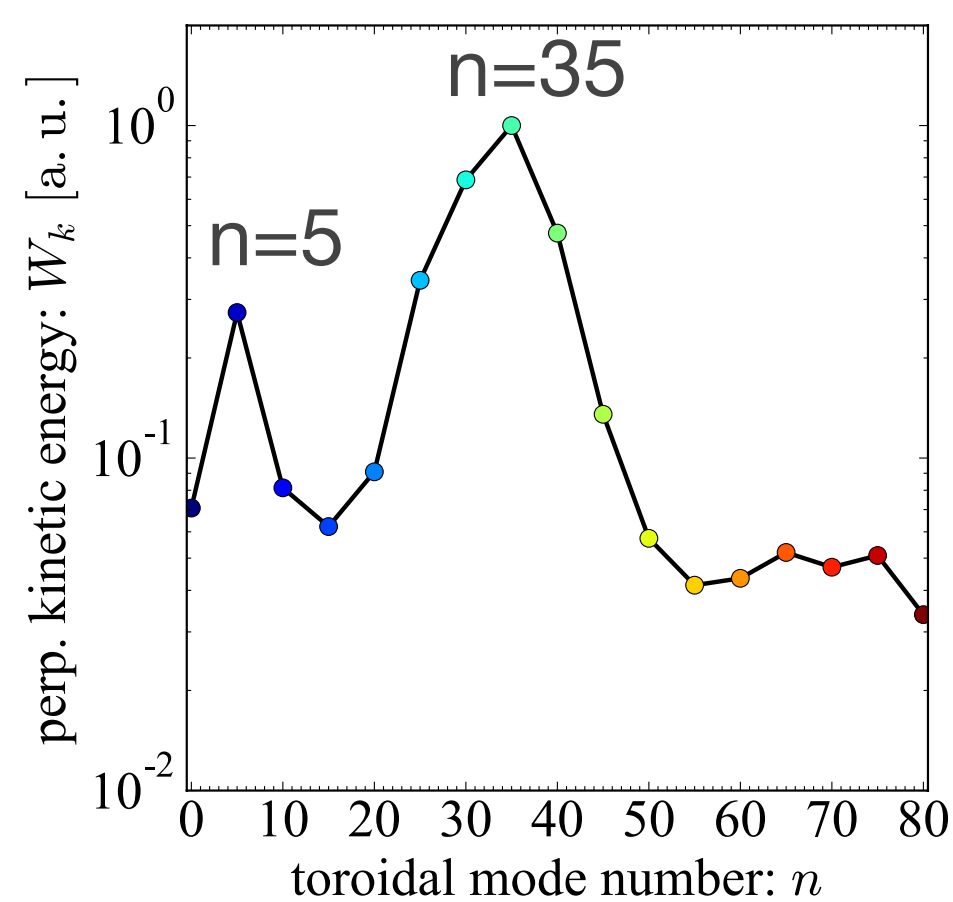
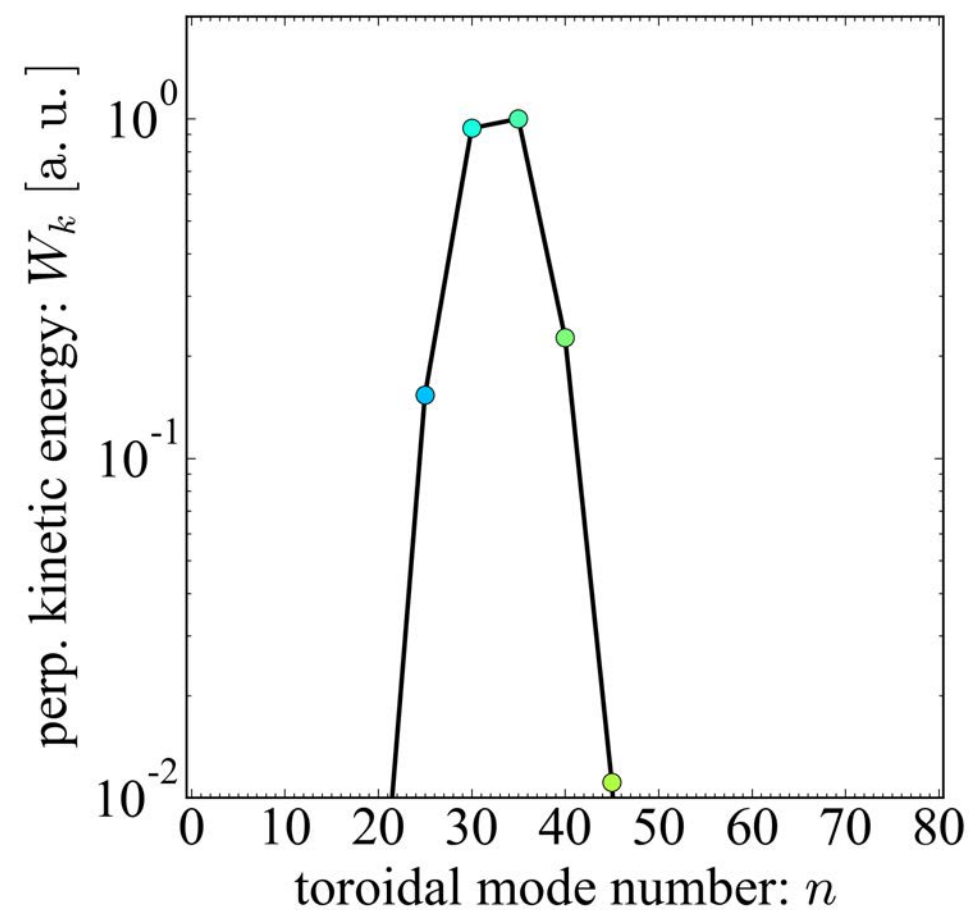


full torus case: $n = 0, 1, 2, \dots, 80$



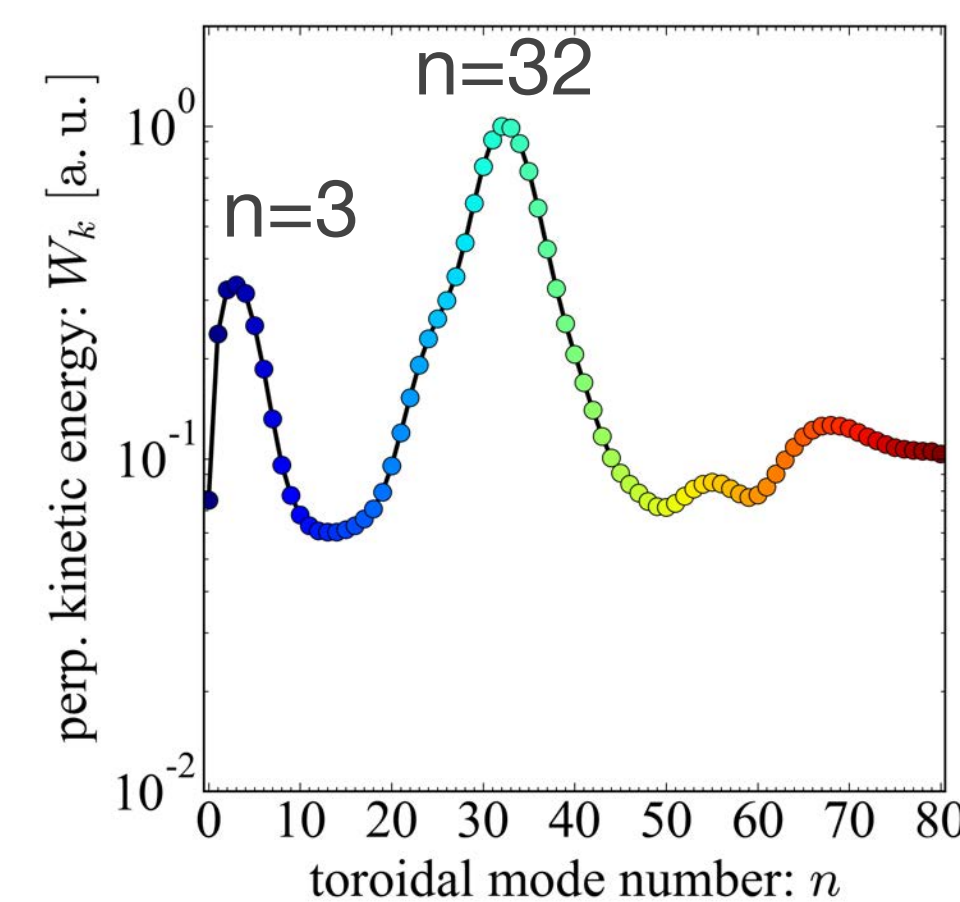
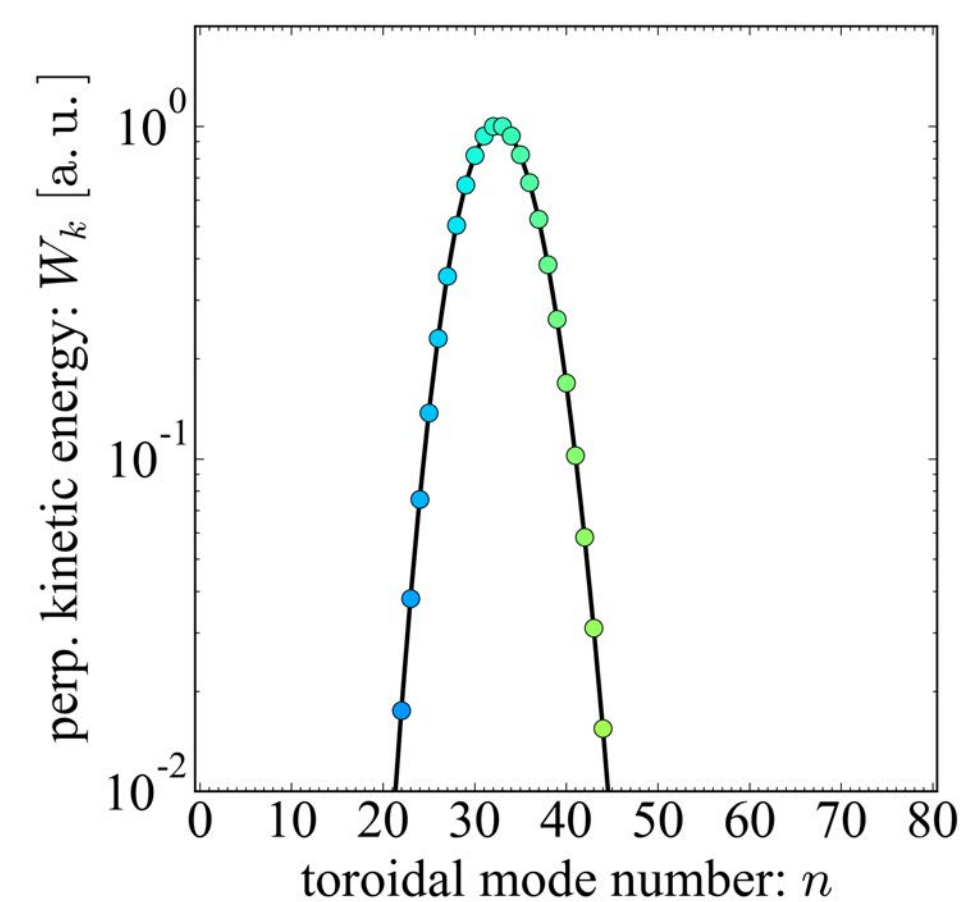
Linear phase: $t=100t_A$

Just before collapse: $t=180t_A$

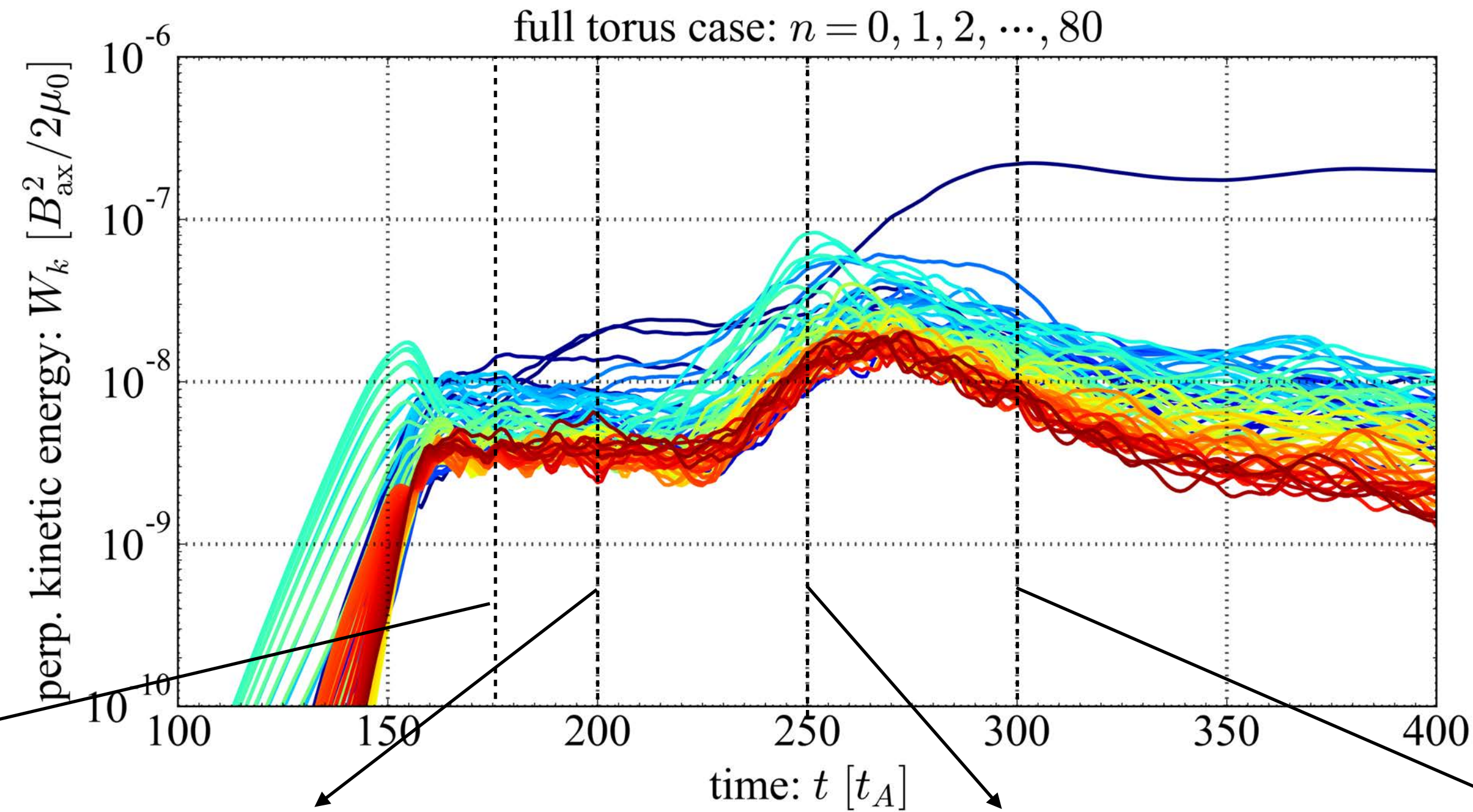


Linear phase: $t=100t_A$

Just before 1st collapse: $t=155t_A$



Low- n modes may play a role between two crashes in full torus case

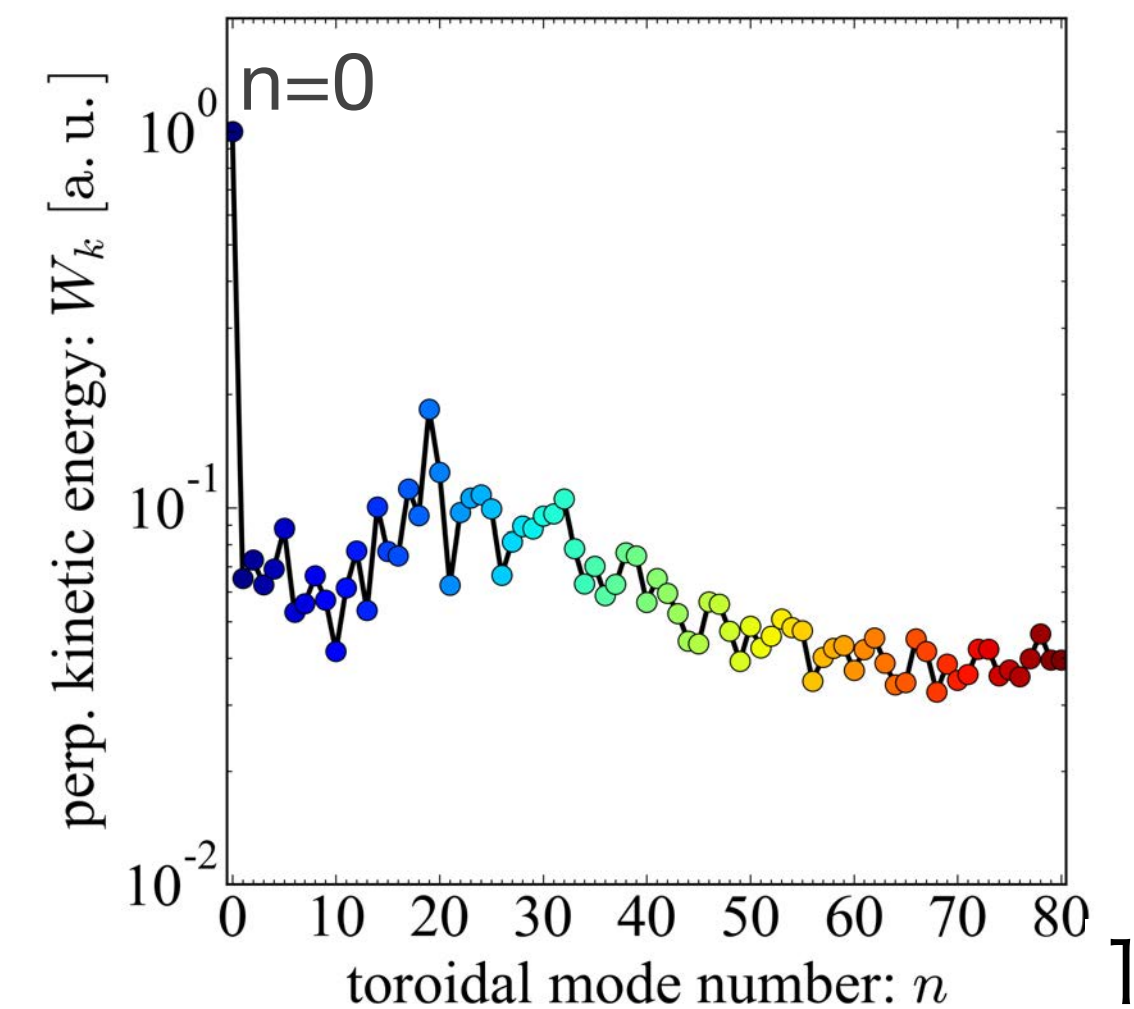
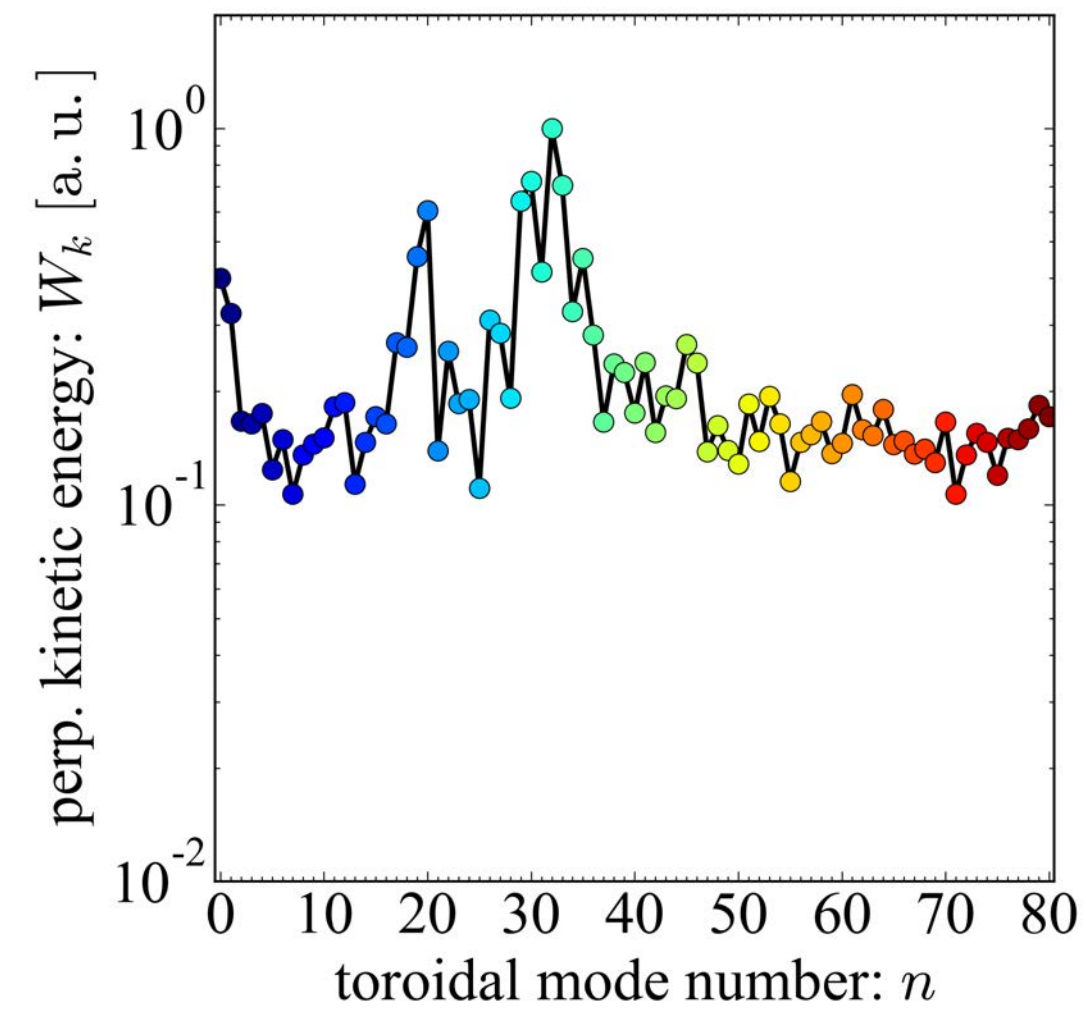
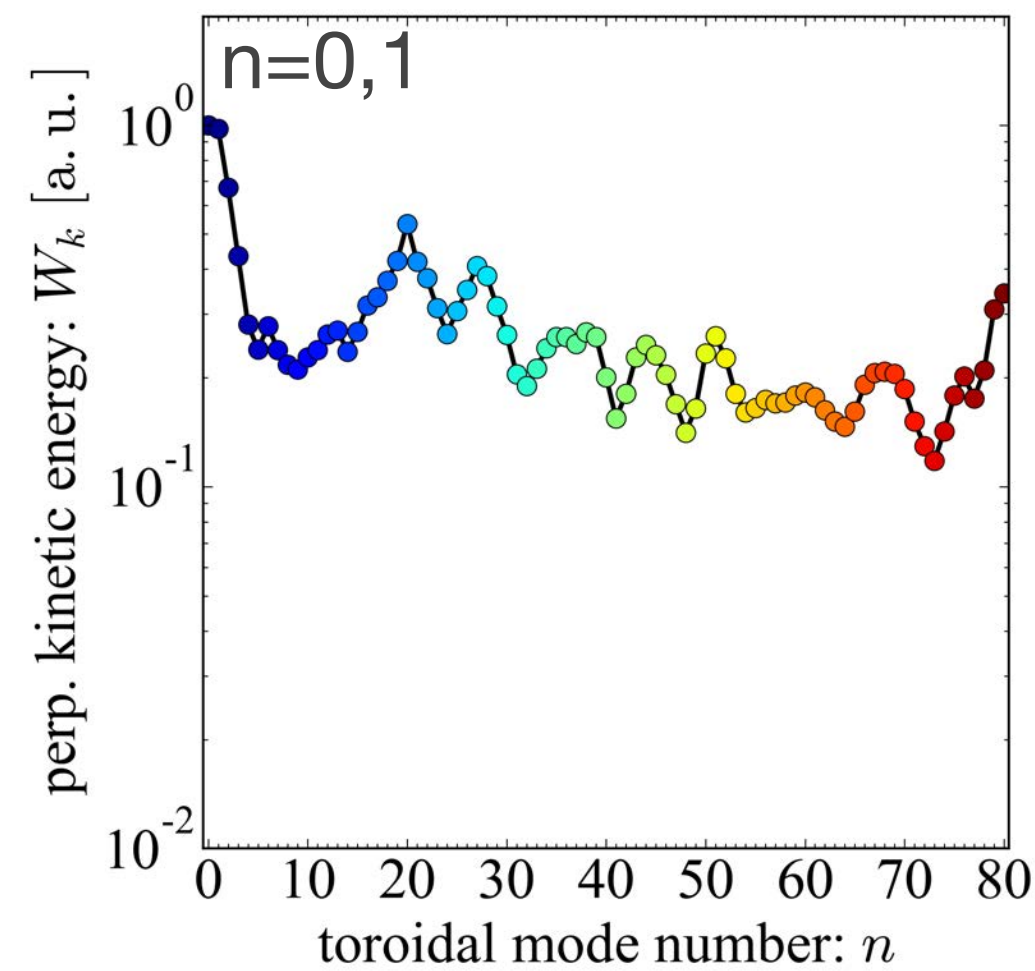
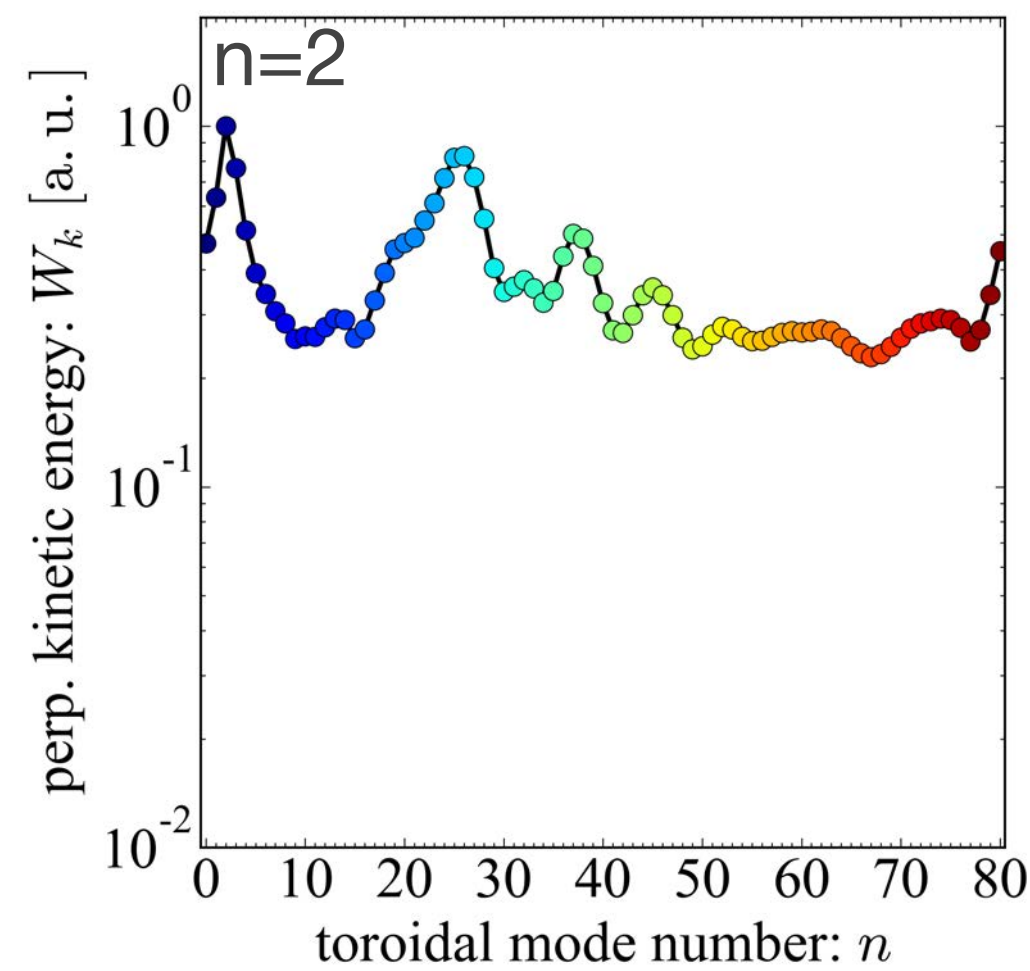


After 1st collapse: $t=175t_A$

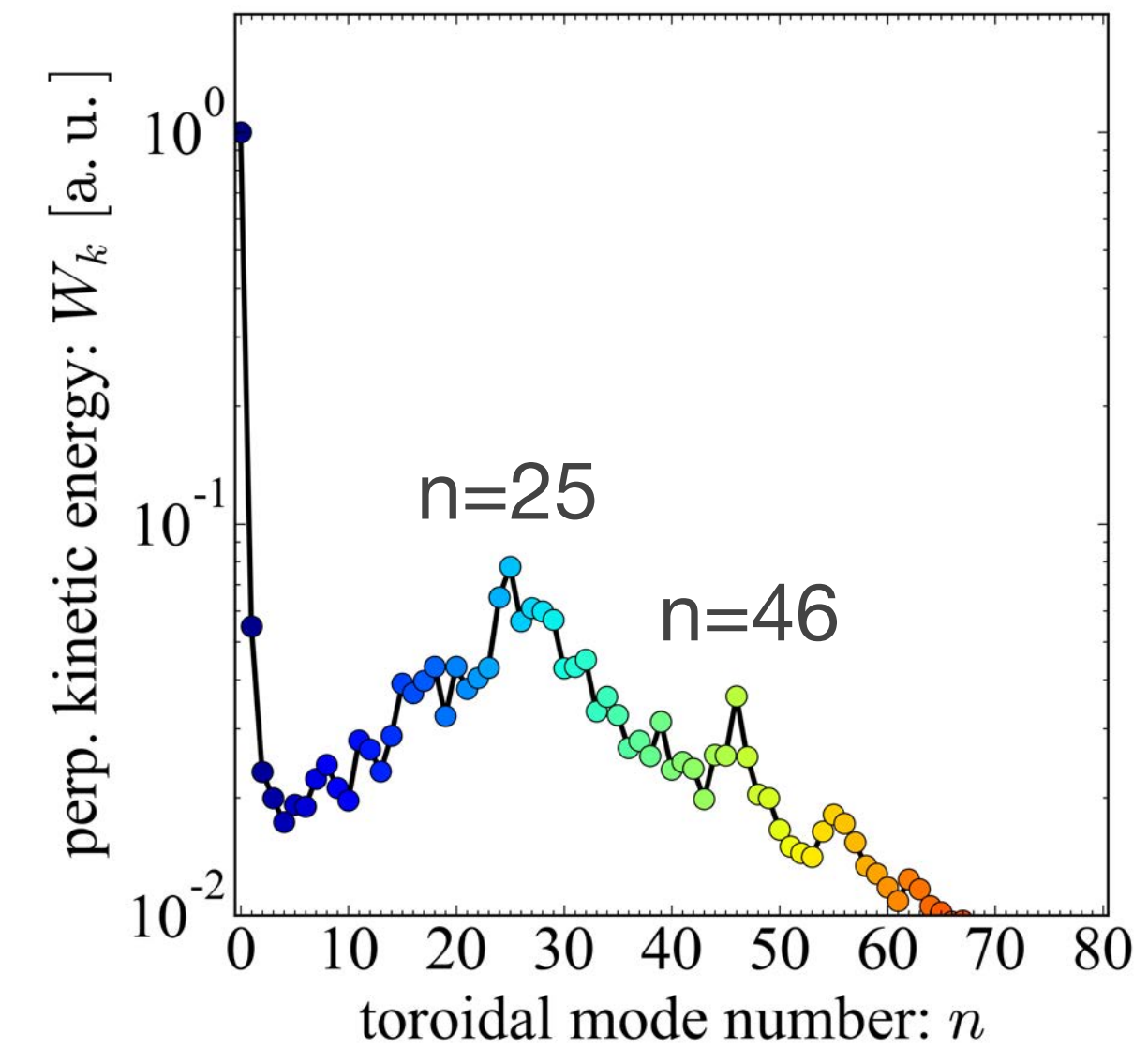
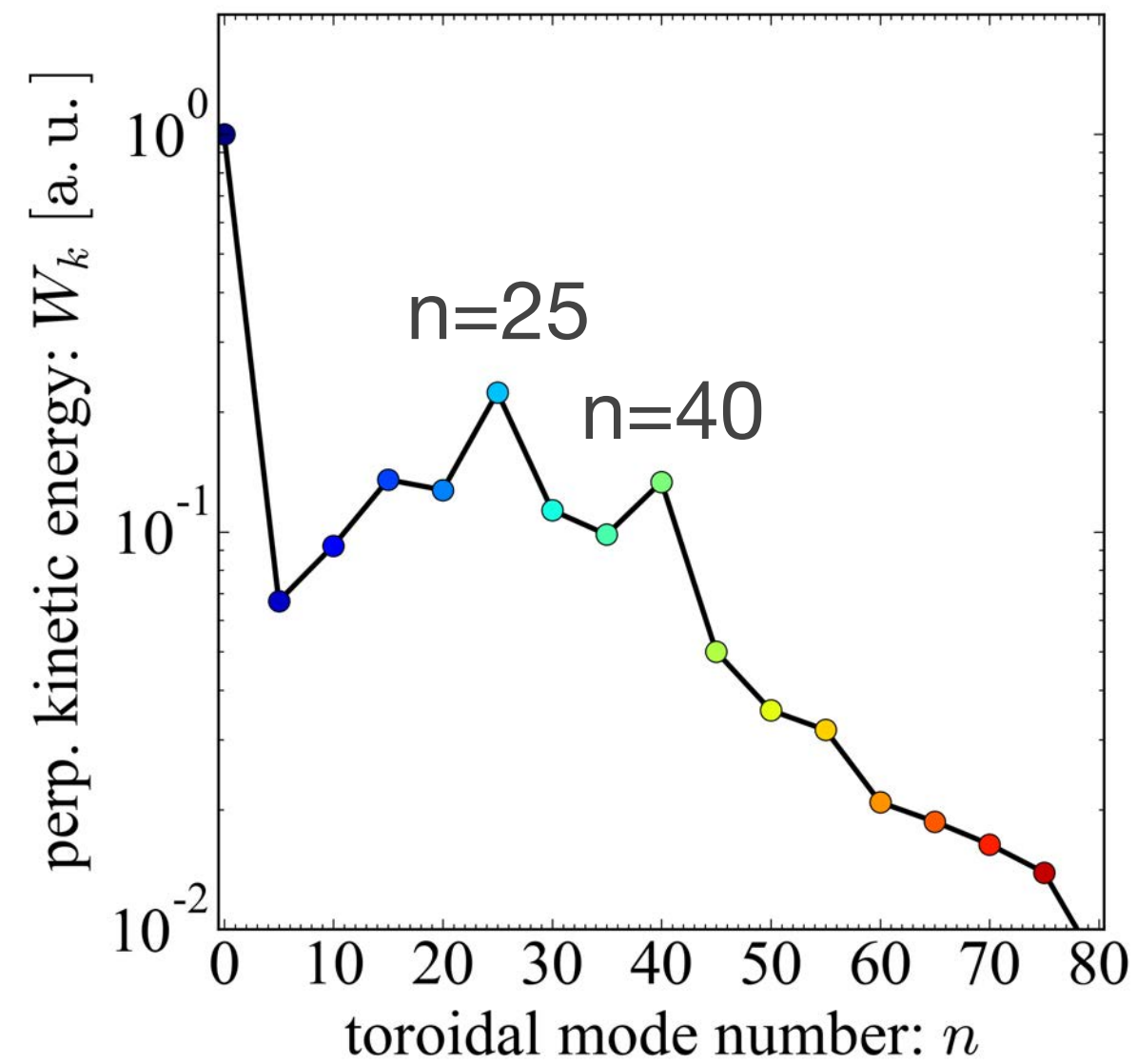
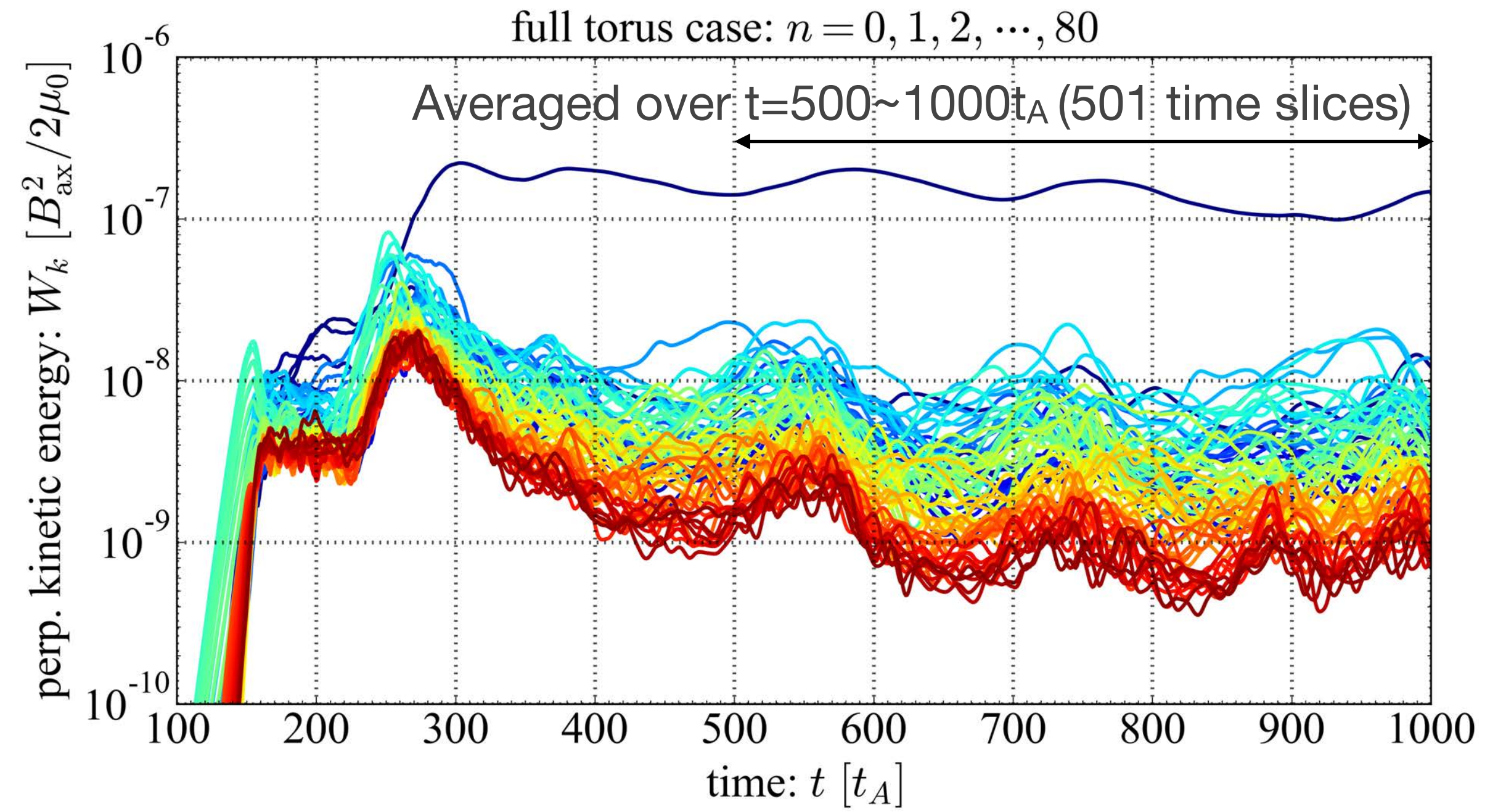
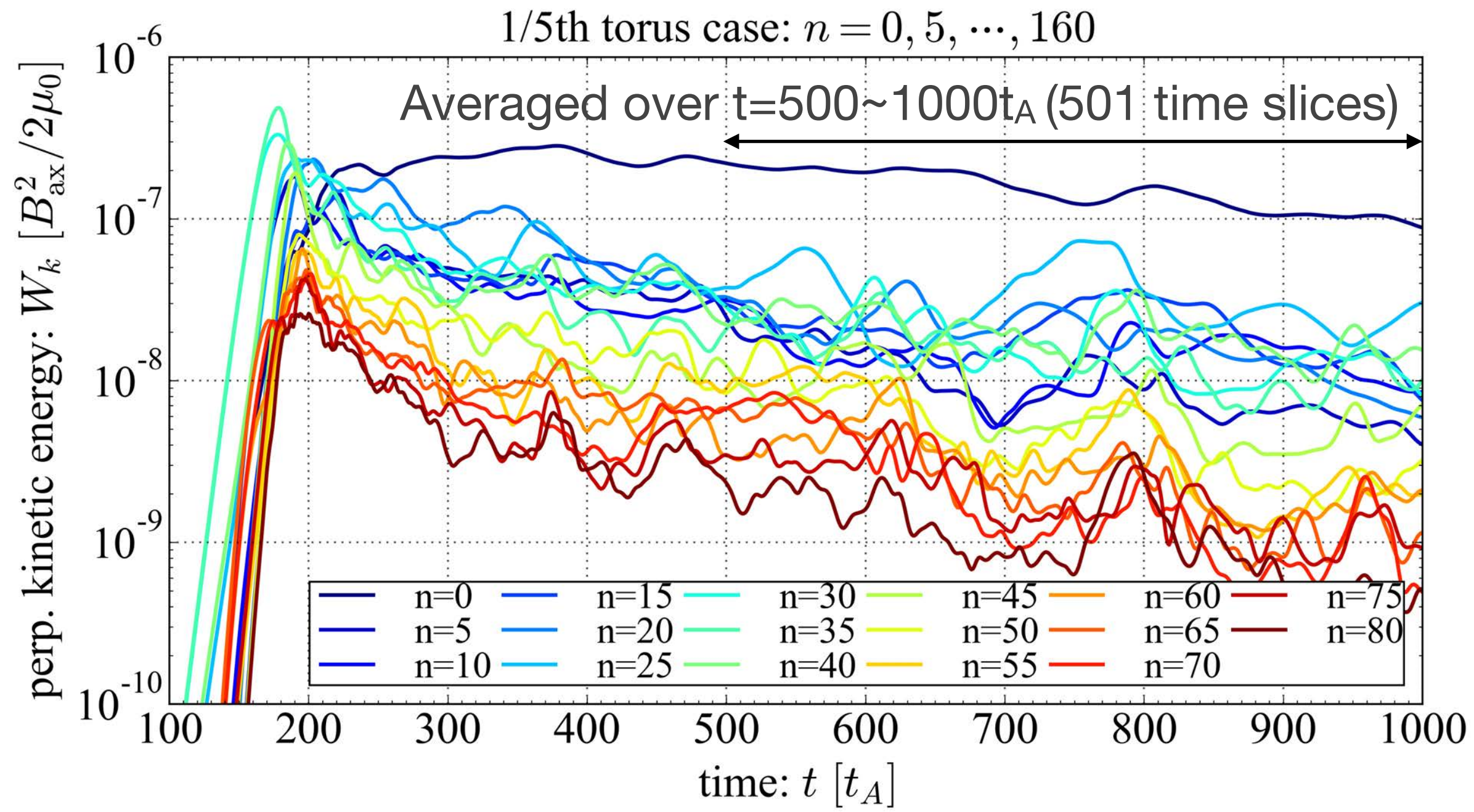
Between 1st and 2nd collapse $t=200t_A$

2nd collapse $t=250t_A$

After 2nd collapse: $t=300t_A$



perpendicular kinetic energy spectrums after crashes show similar trend



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- Preliminary pedestal collapse simulation in annular full torus domain in shifted circular geometry
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2D Poisson solver for low-n modes has been developed to extend BOUT++ for tokamak edge simulation solving interplay between $n=0$, low-n, middle-n and high-n modes in diverted geometries

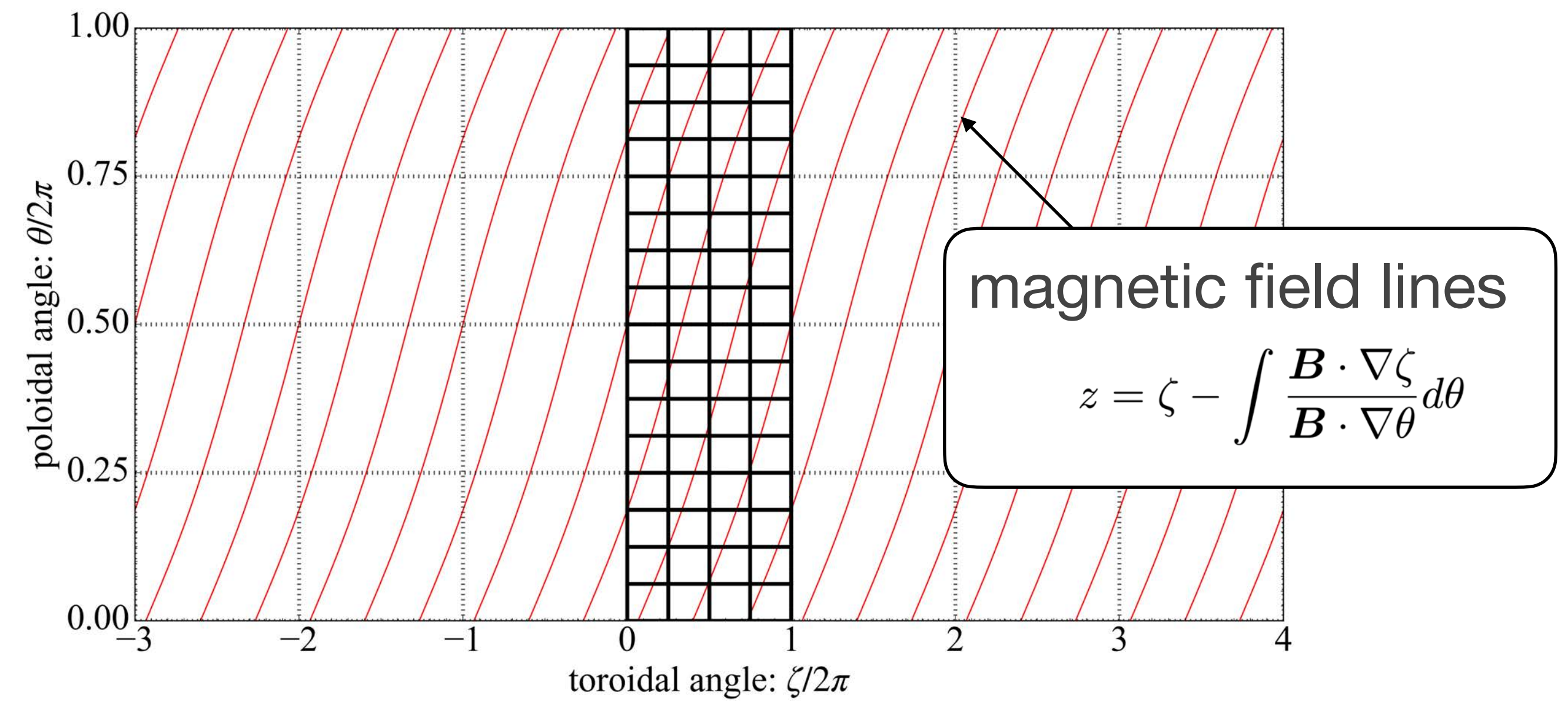
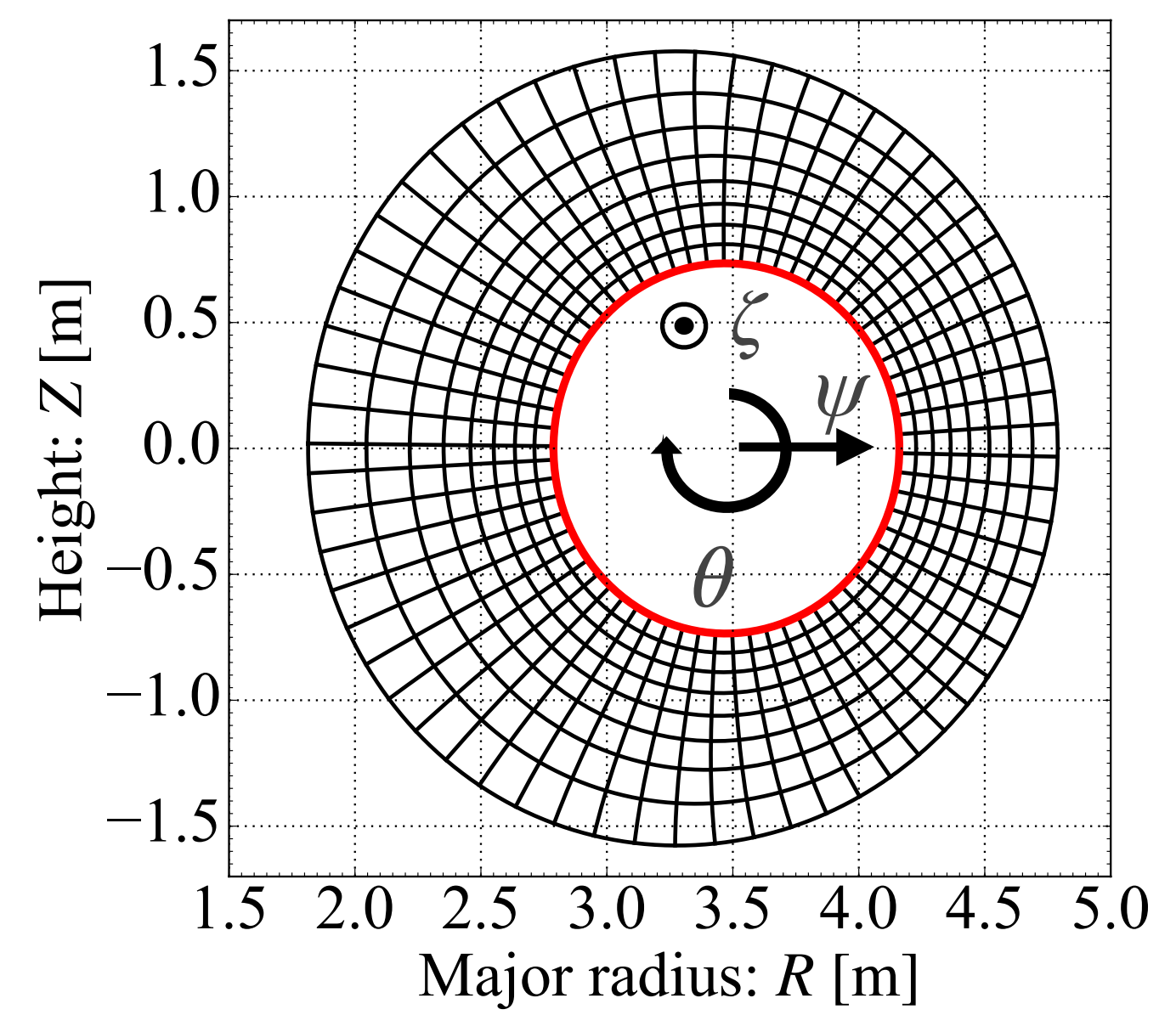
- Verification test of 2D Poisson solver by linear pressure-driven modes
 - Linear IBM growth rates in circular geometry show good agreement between 2D/1D Poisson solvers
 - Linear RBM growth rates in single-null geometry shows 6~8% difference
 - ➡ Further tests are required to clarify impact of flute-ordering in complex geometries
- Preliminary pedestal collapse simulation in annular full torus domain in shifted circular geometry
 - Pedestal collapse simulation in full-annular domain using low-n Poisson solver works with acceptable computational cost
 - Introducing low-n modes may change dynamics during pedestal collapse driven by high-n RBM instability but may not change turbulence property after pedestal collapse
 - ➡ Production run with high-resolution grid ($n_x=1024$, $n_y=128$, $n_z=512$) is required for further analysis

Verification test of 2D Poisson solver by linear problems

- Further ballooning type instability test with ion density profile in diverted geometries
- **2D Poisson solver test with current-driven instabilities (kink/peeling mode) for type-I ELMs**

Nonlinear ELM crash simulations

- Pedestal collapse simulation in full-annular diverted geometries
 - ✓ Some nonlinear runs have finished in single-null geometries but further code checks are required
- Simulation of transition from type-I to type-III ELM including resistive ballooning mode (RBM) turbulence in diverted geometry with full toroidal mode spectrum [research target in FY2021]
 - ✓ ELM crashes in a series of ITER like equilibria with different pedestal collisionality
 - ✓ The maximum simulated toroidal mode is scanned to investigate the impact of RBM turbulence on energy loss during pedestal collapses in type-I ELMs, type-III ELMs, and their intermediate regime
 - ➡ **Maybe useful for understanding dynamics of ELMs in ramp-up/-down phase**

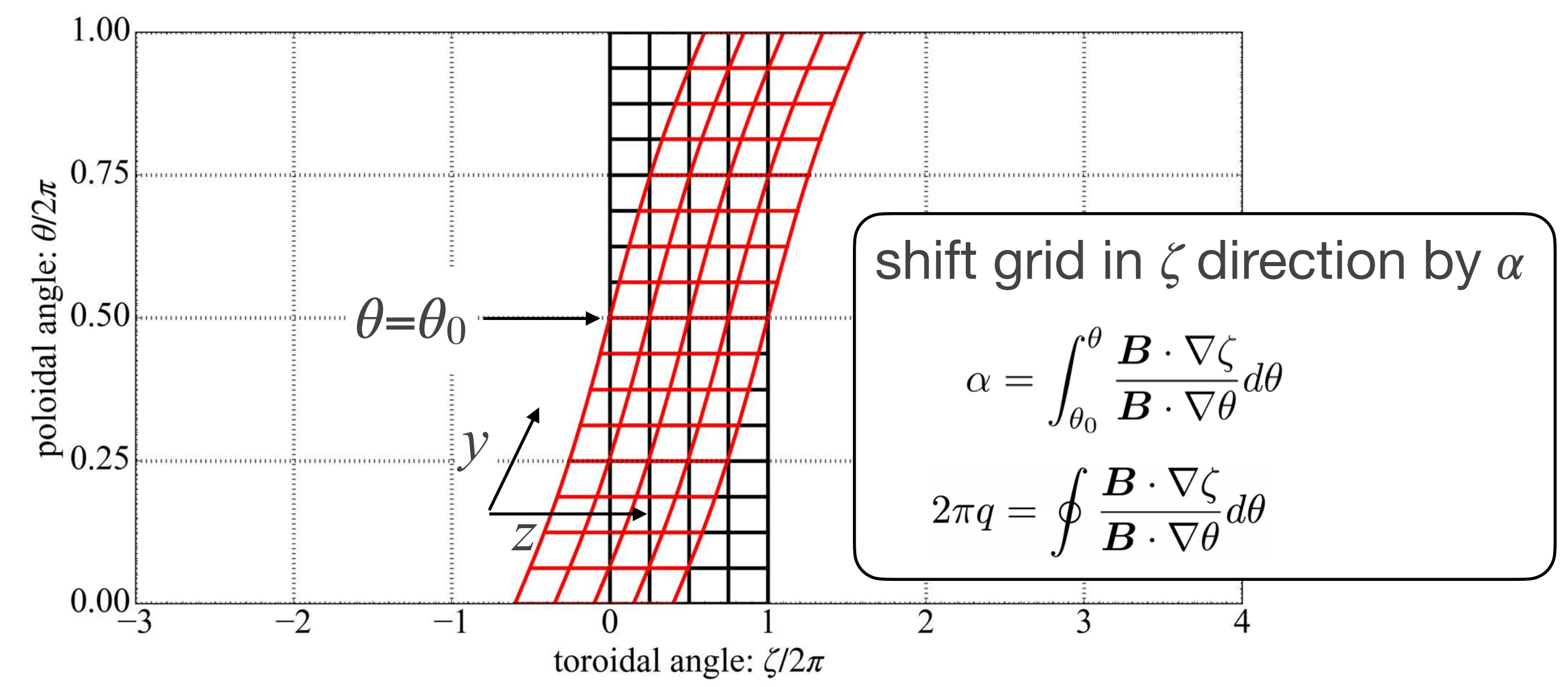
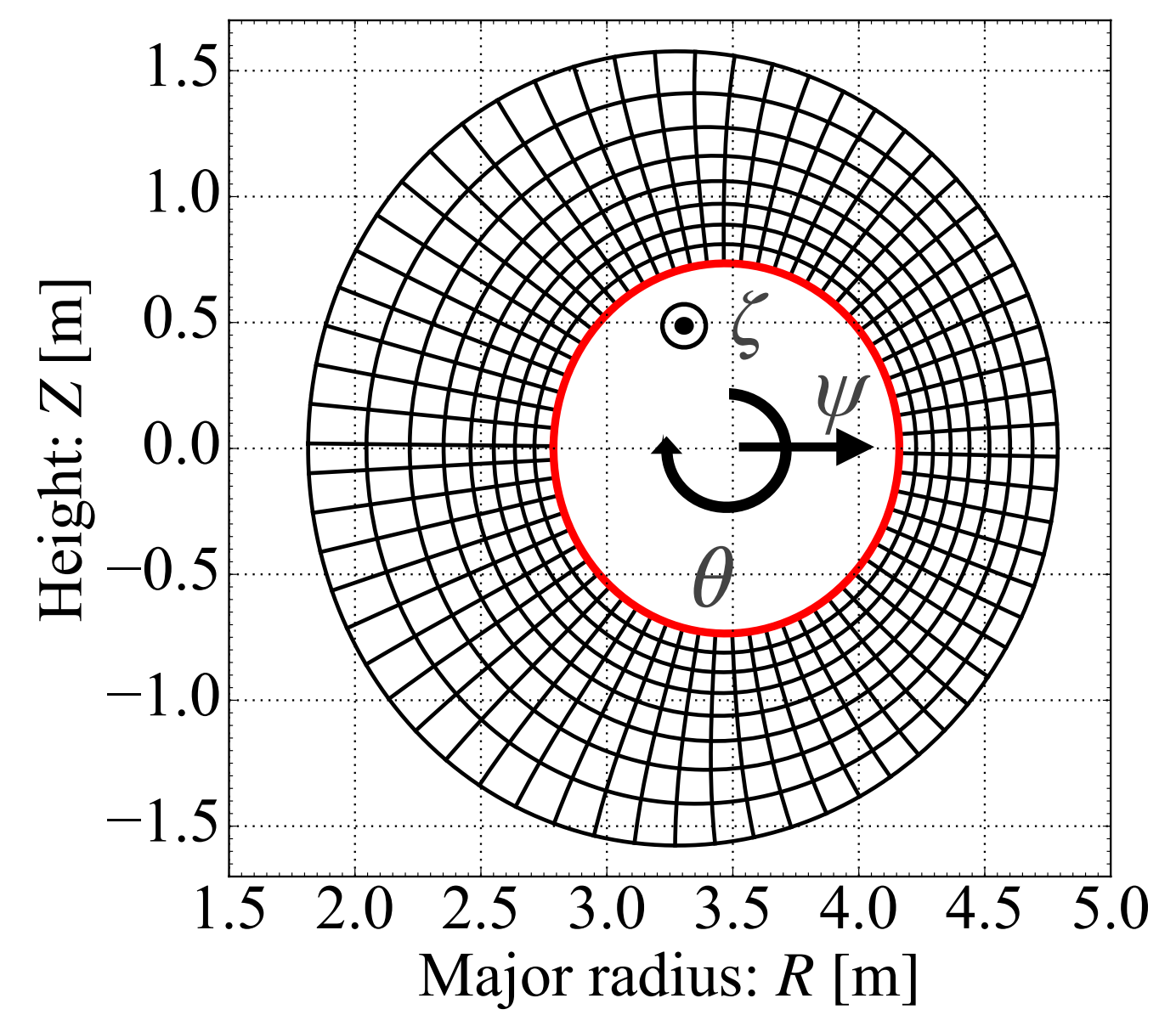


Flux-surface coordinates: (ψ, θ, ζ)

- ψ : poloidal flux function, $[\psi_{in}, \psi_{out}]$
- θ : orthogonal poloidal angle, $[0, 2\pi)$
- ζ : geometrical toroidal angle, $[0, 2\pi/N)$
- periodic boundary condition inside LCFS
 - toroidal: $f(\psi, \theta, \zeta + 2\pi/N) = f(\psi, \theta, \zeta)$
 - poloidal: $f(\psi, \theta + 2\pi, \zeta) = f(\psi, \theta, \zeta)$

Resonant modes have large structures along B but has fine structure perpendicular to B

➔ A number of poloidal grid is required for resonant poloidal mode $m \sim nq$ for high- n modes in high- q edge region



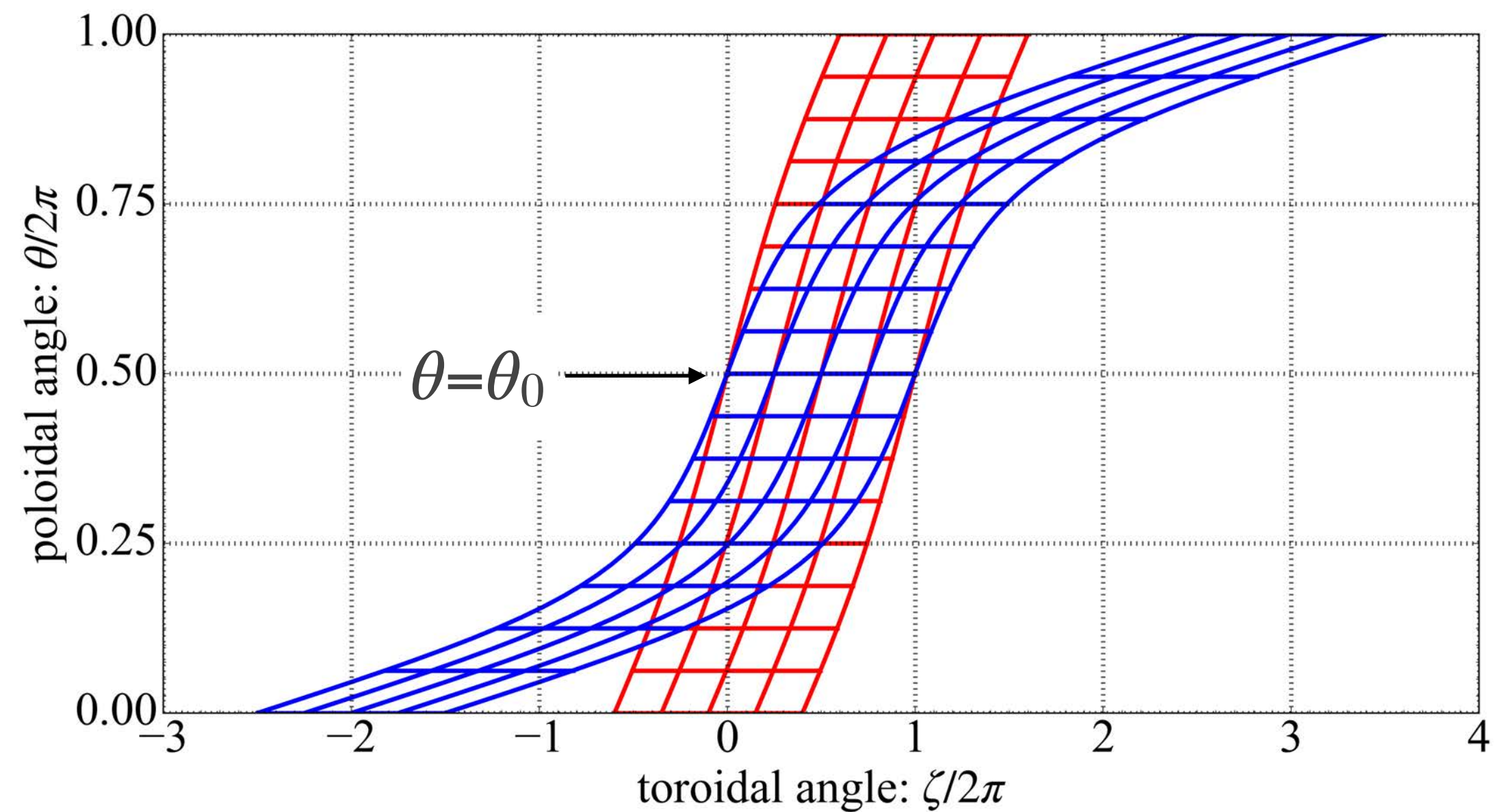
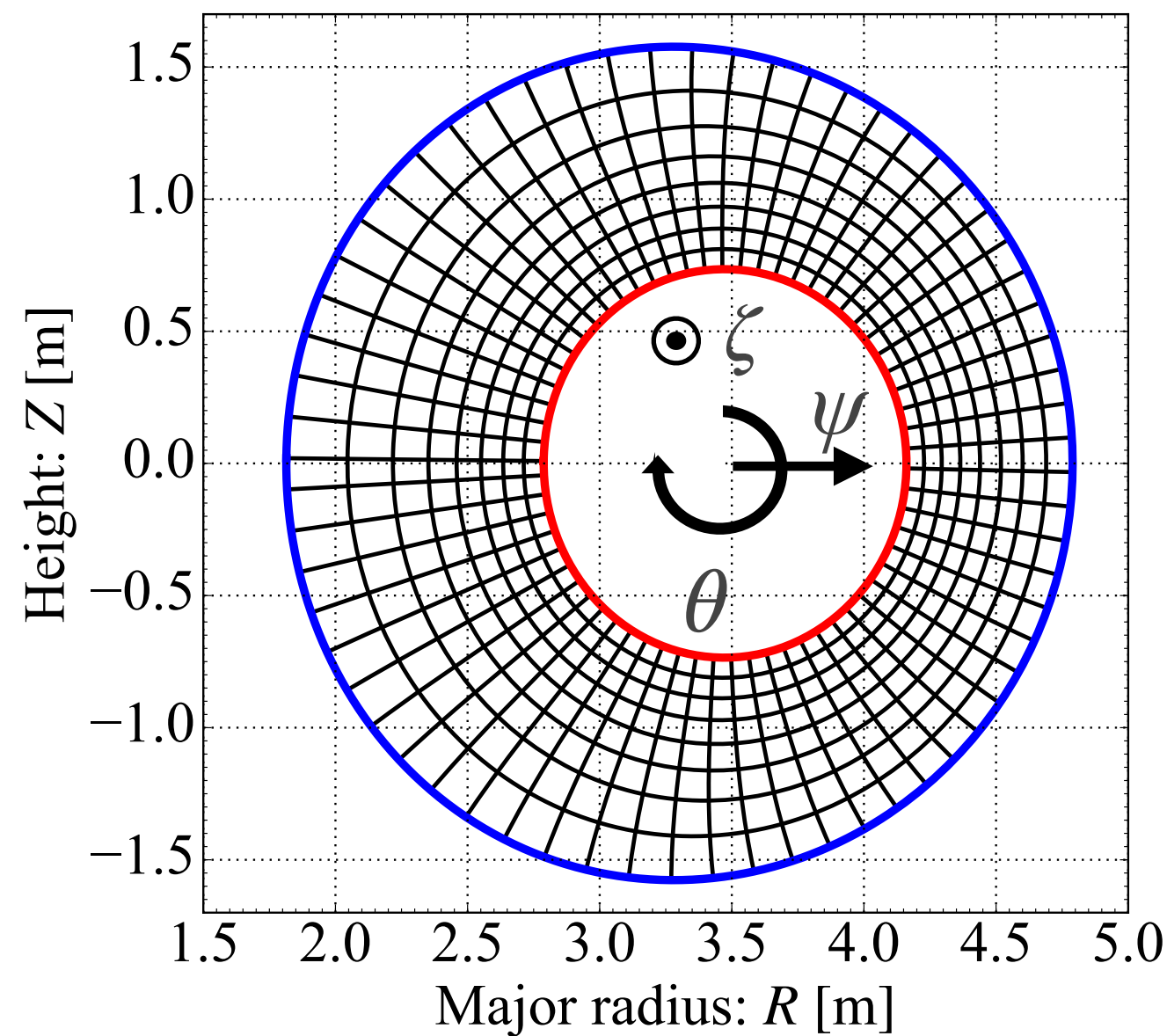
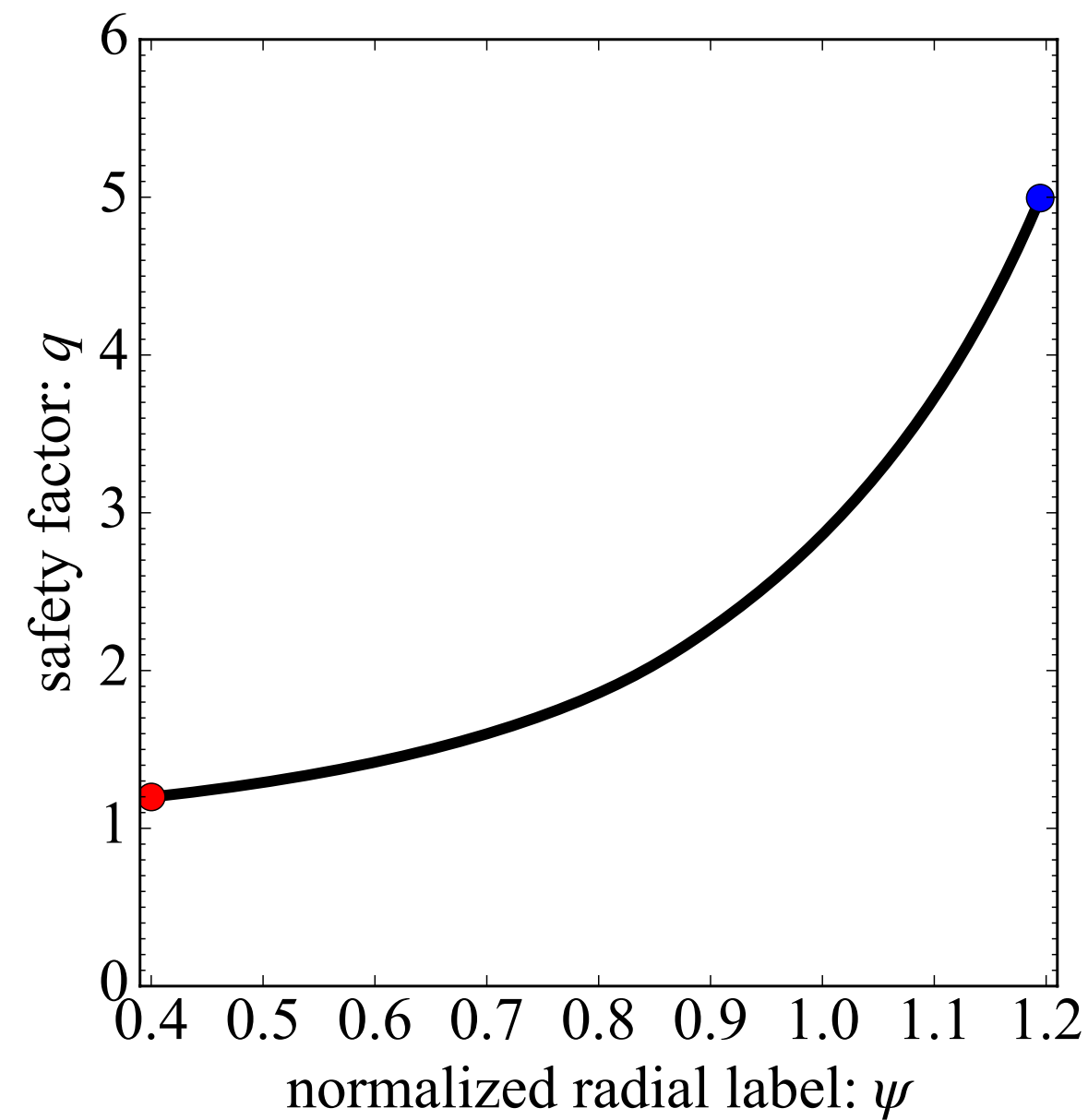
Field-aligned coordinates: (x, y, z)

- $x = \psi - \psi_0$: radial label, $[x_{in}, x_{out}]$
- $y = \theta$: parallel label, $[0, 2\pi)$
- $z = \zeta - \alpha$: binormal label, $[0, 2\pi/N)$
- periodic boundary condition inside LCFS
 - binormal: $f(x, y, z + 2\pi/N) = f(x, y, z)$
 - Parallel: $f(x, y + 2\pi, z - 2\pi q) = f(x, y, z)$

y-direction is aligned to magnetic field line

➔ Grid points in y-dir. can be reduced significantly

Radial shear of magnetic shear (safety factor) strongly deforms field-aligned grid



➔ Cell deformation strongly degrade accuracy of differencing in radial-direction

Example: cell deformation effect in 1st radial derivative in field-aligned coordinates

$$\frac{\partial}{\partial x} = \frac{\partial}{\partial \psi} + I \frac{\partial}{\partial \zeta}$$

Integrated magnetic shear $I = \int_{\theta_0} \frac{\partial \nu}{\partial \psi} d\theta$

Local magnetic shear $\nu = \frac{\mathbf{B} \cdot \nabla \zeta}{\mathbf{B} \cdot \nabla \theta}$

Example: divergence of vector A

$$\begin{aligned} \nabla \cdot \mathbf{A} &= \frac{1}{J} \frac{\partial}{\partial x} (J\mathbf{A} \cdot \nabla x) + \frac{1}{J} \frac{\partial}{\partial y} (J\mathbf{A} \cdot \nabla y) + \frac{1}{J} \frac{\partial}{\partial z} (J\mathbf{A} \cdot \nabla z) \\ &= \frac{1}{J} \left(\frac{\partial}{\partial \psi} + I \frac{\partial}{\partial z} \right) (JA^\psi) + \frac{1}{J} \frac{\partial}{\partial y} (JA^y) + \frac{1}{J} \frac{\partial}{\partial z} (JA^{z'} - IJA^\psi) \\ &= \frac{1}{J} \frac{\partial}{\partial \psi} (JA^\psi) + \frac{1}{J} \frac{\partial}{\partial y} (JA^y) + \frac{1}{J} \frac{\partial}{\partial z} (JA^{z'}) \end{aligned}$$

Integrated magnetic shear free form

Reciprocal basis vector of field-aligned coordinates

$$\begin{aligned} \nabla x &= \nabla \psi \\ \nabla y &= \nabla \theta \\ \nabla z &= \nabla \zeta - \nu \nabla \theta - I \nabla \psi \\ J^{-1} &= \nabla x \times \nabla y \cdot \nabla z \\ &= \nabla \psi \times \nabla \theta \cdot \nabla \zeta \end{aligned}$$

- All spatial differences are evaluated in (ψ, ζ) -plane or (y, z) -plane in integrated magnetic shear free form
 - No mix derivatives with ψ and y due to orthogonality of flux surface coordinates
 - FFT-base coordinate transform for differencing in (ψ, ζ) -plane

$$f(x, y, z) \xrightarrow{\text{Coord. transform}} f(\psi, \theta, \zeta) \xrightarrow{\text{Differencing}} \frac{\partial f}{\partial \psi}(\psi, \theta, \zeta) \xrightarrow{\text{Coord. transform}} \frac{\partial f}{\partial \psi}(x, y, z)$$